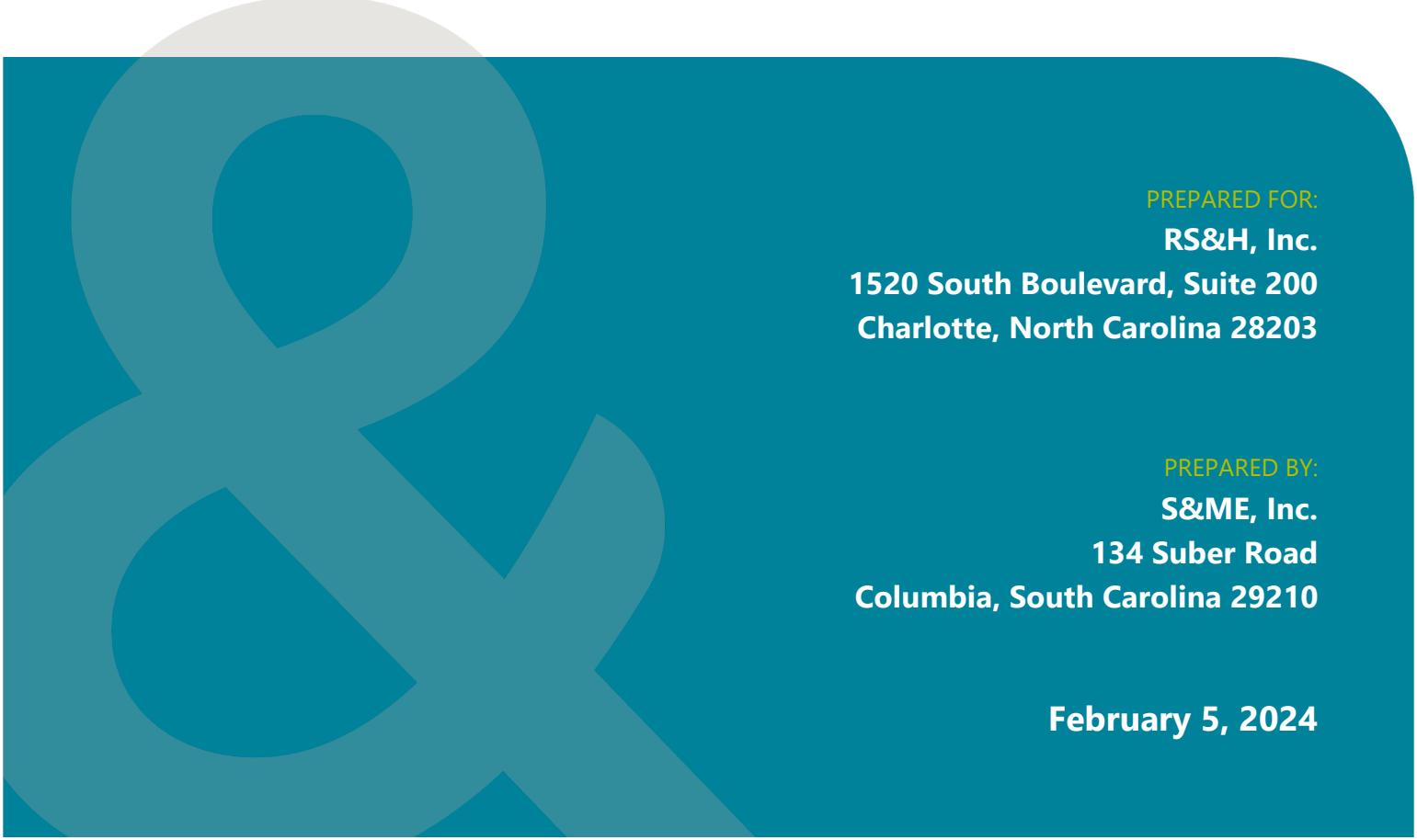




Geotechnical Baseline Report (GBR), Revision 1
Connector Road Bridge over Interstate 77 and Community Road
Interstate 77 Exit 26 – Scout Interchange
Blythewood, Richland County, South Carolina
SCDOT Project ID P042443
S&ME Project No. 23610178A



A large, semi-transparent teal ribbon graphic is positioned in the lower-left quadrant of the page. It features a thick, solid teal outer layer and a thinner, semi-transparent teal inner layer that overlaps it, creating a layered effect.

PREPARED FOR:
RS&H, Inc.
1520 South Boulevard, Suite 200
Charlotte, North Carolina 28203

PREPARED BY:
S&ME, Inc.
134 Suber Road
Columbia, South Carolina 29210

February 5, 2024



February 5, 2024

RS&H, Inc.
1520 South Boulevard, Suite 200
Charlotte, North Carolina 28203

Attention: Mrs. Jennifer Farino, P.E.

Reference: **Geotechnical Baseline Report (GBR), Revision 1**
Connector Road Bridge over Interstate 77 and Community Road
Interstate 77 Exit 26 – Scout Interchange
Blythewood, Richland County, South Carolina
SCDOT Project ID P042443
S&ME Project No. 23610178A

Dear Mrs. Farino:

The purpose of this Geotechnical Baseline Report (GBR) is to provide the design/build team information that may be used in preliminary design and bidding for construction of the bridge and roadway embankments associated with the proposed Connector Road bridge over Interstate 77 and Community Road portion of the overall Interstate 77 Exit 26 – Scout Interchange project, in Blythewood, Richland County, South Carolina. Our services were performed in general accordance with the *Subcontract for Professional Services* between RS&H and S&ME dated May 1, 2023, including the associated scope of services for geotechnical investigations in general accordance with the SCDOT *Geotechnical Design Manual* (GDM), dated January 2022.

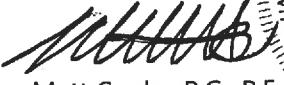
We look forward to continuing our geotechnical engineering services on this important project. Please contact us at (803) 561-9024 if you have questions or need additional information regarding this report.

Sincerely,

S&ME, Inc.



John P. Lewis, P.E.
Project Engineer



Matt Cooke, P.G., P.E.
Office Principal



Robert C. Bruorton, P.E.
Senior Engineer/Vice President





Table of Contents

1.0	Introduction	1
2.0	Project Description	1
3.0	Existing Conditions	2
4.0	Subsurface Exploration Procedures.....	2
4.1	Encroachment Permit.....	3
4.2	Traffic Control.....	3
4.3	Site Clearing	3
4.4	Standard Penetration Test (SPT) Borings.....	3
4.5	Undisturbed Samples (Shelby Tubes)	5
4.6	Shear Wave Velocity Test by Downhole Method	6
5.0	Classification of Recovered Soil Samples.....	6
6.0	Laboratory Physical Tests.....	7
7.0	Subsurface Conditions.....	8
7.1	Area Geology	8
7.2	Soil and Rock Stratification	9
7.2.1	<i>Surface Material</i>	10
7.2.2	<i>Existing Fill</i>	10
7.2.3	<i>Alluvium</i>	10
7.2.4	<i>Upper Cretaceous Coastal Plain Deposits</i>	10
7.2.5	<i>Piedmont Residuum</i>	10
7.2.6	<i>Partially Weathered Rock (PWR)</i>	11
7.2.7	<i>Ground Water</i>	11
7.3	Shear Wave Velocity Measurement	11
8.0	Seismic Design	11
8.1	Acceleration Design Response Spectrum (ADRS)	11
8.2	Preliminary Seismic Evaluation	12



9.0 Design and Construction Considerations.....	13
9.1 Drilled Deep Foundations.....	13
9.1.1 <i>Resistance Criteria</i>	14
9.2 Driven Deep Foundations	14
9.2.1 <i>Driving Considerations</i>	14
9.2.2 <i>Resistance Criteria</i>	14
9.3 Roadway Embankments.....	15
9.3.1 <i>Undercutting/Surface Stabilization</i>	15
9.3.2 <i>Imported Fill/Borrow</i>	15
9.3.3 <i>Slope Stability</i>	15
9.3.4 <i>Compression and Settlement</i>	15
9.4 Earth Retaining Structures	16
9.5 Vibration Monitoring Assessment	16
9.6 Corrosion Potential Results.....	16
10.0 Closing	17

List of Tables

Table 4-1 – Boring Summary	2
Table 4-2 – S&ME Drilling Equipment Summary	3
Table 4-3 – SPT Boring Summary	4
Table 6-1 – Laboratory Testing Table	7
Table 7-1 – Soil Stratification Table	9
Table 8-1 – Seismic Design Parameters.....	12
Table 9-1 – Summary of Corrosion Series Testing.....	16

Appendices

Appendix I – Figures

Appendix II – Tables

Appendix III – Soil Test Boring Records

Appendix IV – Downhole Shear Wave Velocity Test Results

Appendix V – SPT Hammer Energy Measurements



- Appendix VI – Laboratory Test Data Sheets – Split-Spoon Samples
- Appendix VII – Laboratory Test Data Sheets – Corrosion Series Testing
- Appendix VIII – Laboratory Test Data Sheets – Undisturbed Samples
- Appendix IX – 3-Point ADRS Curve
- Appendix X – Electronic Data Files



1.0 Introduction

This report summarizes the results of the geotechnical investigation conducted to date for the proposed Connector Road bridge over Interstate 77 and Community Road portion of the I-77 Exit 26 – Scout Interchange project. The general location of the interchange is shown on the *Site Location Plan*, attached as Figure 1 in Appendix I. Our scope of work relevant to the bridge and bridge embankment portions of the project included:

- Visits to the site by geotechnical personnel,
- Coordinating clearing activities for drill rig access,
- Coordinating coring and drilling activities,
- Performing geotechnical and geophysical subsurface investigations,
- Conducting laboratory testing,
- Reviewing available geologic and geotechnical-related data,
- Requesting ADRS curves provided by SCDOT,
- Preparing this report conforming to Section 21 of the GDM.

Project design parameters and computations generally follow those described in the relevant sections of the South Carolina Department of Transportation (SCDOT) *Geotechnical Design Manual (GDM)*, except where specifically described otherwise in the report text.

2.0 Project Description

Our understanding of the project is based on review of the following plans, provided by RS&H:

- ◆ Microstation file: P042443_DSN_LCS.dgn, dated June 12, 2023
- ◆ Google Earth kmz file: P042443_DSN_ALT03_LCS.kmz, dated September 11, 2023
- ◆ *Conceptual Roadway Plans Alternate 3*, prepared by RS&H, dated August 30, 2023
- ◆ *Conceptual I-77 Interchange and Connection Roads Construct Bridge on Connector Road over I-77 and Community Road, Conceptual Bridge Plans*, prepared by RS&H, dated December 11, 2023.

From our review of the provided information, we understand the Connector Road bridge over I-77 and Community Road will consist of an approximately 360-foot long, four-span structure supported on two end bents and three interior bents (spanning from Bent 1 through Bent 5), with an up to 100-foot wide extension to the south between Bent 1 and 3 to accommodate the on-ramp that will be supported by one additional interior bent and an additional end bent. Driven steel H-piles are planned for support of the end bents and drilled shafts are planned for support of the interior bents. Due to the roughly 20 to 30 feet of fill required to raise the roadway alignment above I-77 and Community Road, mechanically stabilized earth (MSE) retaining walls will support the bridge abutment embankments at end bents. The finished roadway configuration of the bridge will consist of three, 12-foot wide westbound lanes, two, 14-foot wide left turn lanes, two, 12-foot wide eastbound lanes, with one a dual-purpose right turn lane to on-ramp, a 12-foot wide eastbound right turn lane to on-ramp and two, 12-foot wide southbound lanes associated with the on-ramp, with appropriate shoulders and barrier walls.



3.0 Existing Conditions

The proposed Connector Road bridge will cross over I-77 and re-aligned Community Road near mile marker 25.7, roughly 1.5 miles north of the existing interchange of I-77 with US Highway 21 (Wilson Boulevard) and roughly 1.6 miles south of the existing interchange of I-77 with Blythewood Road. The approximate location of the proposed bridge crossing is shown on the *Site Location Plan*, Figure 1 in Appendix I.

At the time of our exploration, the planned alignment, from west to east, was observed to consist of portions of Community Road and I-77, including grassed shoulders and medians, as well as undeveloped woodlands.

The existing Community Road right-of-way in this area consisted of a two-lane, asphalt-paved road with grassed shoulders. Beyond the shoulder to the west and east was a grassed drainage ditch and varying woodlands. The existing I-77 right-of-way in this area consisted of a four-lane, separated asphalt-paved highway with asphalt paved shoulders. The median area is grassed and a drainage ditch was observed near the center of the median. Beyond the shoulders to the west and east was a grassed drainage ditch followed by varying woodlands.

The topographic survey map published by the United States Geological Survey (USGS) was reviewed for ground surface features at the project location. From our review of the Blythewood, South Carolina historical topographic quadrangle map, the site is generally situated along the crest of a ridge. Two unnamed tributaries of Beasley Creek are shown to cross beneath Interstate 77 roughly 2,100 feet south and 3,200 feet north of the bridge site.

4.0 Subsurface Exploration Procedures

As requested, representatives of S&ME were present at the above-referenced site between September 28 and November 16, 2023, to conduct field activities for the project. The exploration included the following:

- Twenty-seven (27) Standard Penetration Test (SPT) borings – EB-1C through EB-6C, IB-1C through IB-11C, W-1 through W-8, EM-1, and EM-2,
- Two (2) undisturbed samples – conducted at offset Boring W-2UD, and,
- One (1) Down-Hole Shear Wave Velocity Test – conducted in Boring EB-1C.

Boring designations reflect the purpose of the borings, as follows:

Table 4-1 – Boring Summary

Purpose	Boring No.
End Bents	EB-1C through EB-6C
Interior Bents	IB-1C through IB-11C
Bridge Embankments	EM-1 and EM-2
Retaining Walls	W-1 through W-8

The boring locations were initially established in the field by representatives of S&ME at the locations submitted to and approved by SCDDOT using our hand-held sub-meter GPS unit. Borings were performed in reasonable



proximity to marked location stakes unless they are offset because of slopes, ditches, overhead power, or other obstructions. Subsequent to drilling and abandonment, boring coordinates and elevations were surveyed by CES Group Engineers, LLC (CES) under subcontract to RS&H. A summary of testing locations, including coordinates, elevation, alignment, station and offset are presented in Table 1, *Test Location Summary*, in Appendix II. Surveyed coordinates are tabulated in decimal degree latitude and longitude as well as South Carolina State Plan northing and easting. The coordinates and elevations of the borings tabulated in this report and indicated on the boring records may be considered accurate to the degree of surveying accuracy used by the surveyor.

The following sections summarize the general outline of each test. The field testing data are organized into appendices of this report as follows:

- ◆ Appendix III – Soil Test Boring Records
- ◆ Appendix IV – Down-Hole Shear Wave Velocity Test Results
- ◆ Appendix V – SPT Hammer Energy Reports

4.1 Encroachment Permit

S&ME applied for encroachment along the SCOT right-of-way along Interstate 77 on June 27, 2023, and received the approved encroachment permit No. 269263 on July 25, 2023. S&ME applied for encroachment along the SCOT right-of-way along Community Road on June 27, 2023, and received the approved encroachment permit No. 269262 on July 25, 2023.

4.2 Traffic Control

Traffic control for the project was provided by Area Wide Protective (AWP), under subcontract to S&ME, for borings within the existing shoulders of Community Road and along the existing shoulders and median of I-77. Traffic control was performed in accordance with applicable SCOT Standard Drawings.

4.3 Site Clearing

Clearing was performed by Palmetto State Land Management, under subcontract to S&ME, using a skid steer-mounted forestry grinder to create drill rig access pathways to several of the boring locations located in wooded areas. Trails of approximately 12 to 15 feet wide were cleared with trees chipped in-place. No attempt was made to stack or remove downed trees from the site. Care was taken to limit site disturbance during this process.

4.4 Standard Penetration Test (SPT) Borings

Twenty-seven (27) soil test borings with SPT sampling were performed for the project using four (4) drill rigs during the exploration, as follows.

Table 4-2 – S&ME Drilling Equipment Summary

Rig Make/Model	Serial No.	Carrier Type	Average SPT Energy
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			Transfer Ratio (ETR), %
CME-550X	290593	ATV	91.6%
CME-550X	299403	ATV	91.0%
Diedrich D-50	316	Track	96.8%
CME-550X	293193	ATV	87.6%

SPT hammer energy measurements with a Pile Driving Analyzer (PDA) were performed by S&ME at off-site locations for the drill rigs used on the project in general accordance with ASTM D4633 *Standard Test Method for Energy Measurement for Dynamic Penetrometers*. The SPT Energy test results are provided in Appendix V. The N-values indicated on the logs are field values and were not corrected for overburden stress, rod length, borehole diameter or hammer efficiency. Hammer energy ratios are provided on the individual soil test boring records in Appendix III.

Soil test borings with SPT sampling were performed using mud rotary drilling techniques. The borings were extended to termination or drill bit refusal depths ranging from 39.4 to 100 feet below the existing ground surface.

Table 4-3 – SPT Boring Summary

Boring No.	Purpose
EB-1C	End Bent 1 Westbound
EB-2C	End Bent 1 Eastbound
EB-3C	End Bent 5 Westbound
EB-4C	End Bent 5 Eastbound
EB-5C	End Bent 6 Southbound (On-Ramp)
EB-6C	End Bent 6 Southbound (On-Ramp)
EM-1	Western Roadway Embankment Eastbound
EM-2	Eastern Roadway Embankment Westbound
IB-1C	Interior Bent 4 Westbound
IB-2C	Interior Bent 4 Eastbound
IB-3C	Interior Bent 4 Eastbound
IB-4C	Interior Bent 3 Westbound
IB-5C	Interior Bent 3 Westbound
IB-6C	Interior Bent 3 Eastbound
IB-7C	Interior Bent 2 Westbound
IB-8C	Interior Bent 2 Westbound
IB-9C	Interior Bent 2 Eastbound (On-Ramp)



Boring No.	Purpose
IB-10C	Interior Bent 7 Southbound (On-Ramp)
IB-11C	Interior Bent 7 Southbound (On-Ramp)
W-1	MSE Abutment Retaining Wall No. 2 North
W-2	MSE Abutment Retaining Wall No. 2 North
W-3	MSE Abutment Retaining Wall No. 2 South
W-4	MSE Abutment Retaining Wall No. 2 South
W-5	MSE Abutment Retaining Wall No. 1 North
W-6	MSE Abutment Retaining Wall No. 1 North
W-7	MSE Abutment Retaining Wall No. 1 South
W-8	MSE Abutment Retaining Wall No. 1 South

Soil sampling and penetration testing were performed in general accordance with ASTM D1586 *Standard Test Method for Penetration Test and Split Barrel Sampling of Soils*. SPT was performed in each boring continuously in the upper 10 feet in each end bent, interior bent, abutment wall and embankment boring, followed by approximate 5-foot centers, thereafter. The split-barrel sampler was opened at the drill site and sloughed material was identified and separated from the recovered sample. The recovered sample was visually described and classified by S&ME's rig geologist or engineer. A selected portion of the sample was placed in a sealed moisture-proof container. Where materials changed over the sample drive length, a sample of each material was retained. The containers were labeled and transported to the S&ME Columbia Office at the end of each workday.

Water level measurements were attempted immediately after completion of drilling and, where feasible, were repeated after a period of roughly 24 hours. We note that due to the use of drilling fluid additives in mud rotary borings, the water level readings recorded in the soil borings may not accurately reflect the ground water conditions at the site. Ground water readings were conducted in general accordance with ASTM D4750 *Standard Test Method for Determining Subsurface Liquid Levels in a Borehole or Monitoring Well (Observation Well)*.

After ground water measurements were complete, the borings were backfilled with bentonite chips, auger cuttings or clean fill to within 20 feet of the existing ground surface then abandoned with Portland cement/bentonite grout to the existing ground surface. Grout quantities were recorded, and grout logs are available upon request.

4.5 Undisturbed Samples (Shelby Tubes)

Two (2) relatively undisturbed (UD) samples, or Shelby Tubes, were attempted and recovered at boring location W-2UD located along the northern portion of the MSE Abutment retaining wall No. 2. Sampling was performed in general accordance with ASTM D1587 *Standard Practice for Thin-Walled Tube Sampling of Fine Grained Soils for Geotechnical Purposes*. Shelby tube sample depths were selected by S&ME upon review of the companion SPT log and assigned accordingly.



Shelby Tubes provide sufficiently intact samples for quantitative laboratory testing. Samples were obtained by pushing a 3-inch outer diameter, 16-gauge, steel tube into the soil at the desired sampling intervals in a borehole adjacent to the original SPT location. The tube, together with the encased soil, was carefully removed from the ground and length of the recovered soil measured. The ends of the tube were sealed with microcrystalline wax and labeled with applicable project information before being transported to our laboratory. Shelby tube samples were transported and stored in general accordance with ASTM D4220 for Group C samples.

4.6 Shear Wave Velocity Test by Downhole Method

Upon completion of drilling activities for bridge boring EB-1C, flush-threaded schedule 40 PVC casing was installed, and the annulus grouted in place using a cement/bentonite grout mixture to support shear wave velocity testing.

On October 30, 2023, we performed a downhole seismic survey within boring EB-1C in general accordance with ASTM D7400 *Standard Test Methods for Downhole Seismic Testing*, using a Geometrics seismograph and 14 Hz downhole triaxial geophone. Energy for the seismic survey was generated by a 16-pound sledgehammer striking the end of a wooden plank. Seismic velocities were obtained to a depth of about 97 feet using recorded depth intervals of 3 feet. Data analysis was conducted using the OYO Corporation's SeisImagerTM/SW software (PickwinTM) and the resulting shear wave velocity profile for EB-1C is presented in Appendix IV. After completion of downhole shear wave velocity testing, the top of the PVC casing was cut flush with the ground surface and tremie grouted to the ground surface.

Geophysical Limitations

Regardless of the thoroughness of a geophysical survey, there is always a possibility that actual conditions may not match the interpretations. The results should be considered accurate only to the degree implied by the method used and the method's limitations and data coverage. In addition, site activity (e.g., heavy traffic, etc.) and overhead powerlines can cause noise/interference in downhole seismic data sets.

5.0 Classification of Recovered Soil Samples

Recovered split-spoon samples were initially classified in general accordance with ASTM D2488 *Standard Practice for Description and Identification of Soils (Visual-Manual Method)*. After laboratory testing was completed, provisional field classifications were revised as necessary to provide a soil description that generally follows the terminology given by ASTM D2487 *Standard Practice for Classification of Soils for Engineering Purposes (Unified Soil Classification System)* and AASHTO M145 *Recommended Practice for Classification of Soils and Soil-Aggregate Mixtures for Highway Construction Purposes*.

Interpreted subsurface conditions encountered by the SPT borings are shown on the boring records in Appendix III. These records were compiled in gINT using standard SCOT template. Interpreted subsurface profiles are provided for the bridge alignment (Figure 3), MSE wall No.1 alignment (Figure 4) and MSE wall No. 2 alignment (Figure 5) in Appendix I. These records represent our interpretation of the subsurface conditions based on the test data. Stratification lines on the boring records represent approximate boundaries between soil types; however, the actual transition may be gradual, and the thicknesses of the strata will vary across the site. The soil samples



will be retained at our laboratory for a period of seven years, or until completion of substructure installation, whichever is earlier.

6.0 Laboratory Physical Tests

Index property testing consisting of Atterberg limits, particle-size distribution, percent finer #200 sieve, and natural moisture content tests were performed on split-spoon samples and undisturbed samples to assist in classifying the soils. Additionally, corrosion series (pH, chloride, sulfate, and resistivity) testing was performed on selected split-spoon samples. Finally, unit weight and consolidated undrained triaxial shear testing were performed on undisturbed samples.

Table 6-1 – Laboratory Testing Table

Test Type	Quantity
Atterberg limits	52
Particle-size distribution	25
Percent-finer 200 sieve	51
Natural moisture content	76
Corrosion Series	6
Unit Weight	1
Consolidated undrained triaxial shear	1

Testing was performed in general accordance with ASTM, AASHTO, or SC state test procedures as follows:

- Atterberg limits – ASTM D4318
- Particle-size distribution – ASTM D6913
- Percent-finer 200 sieve – ASTM D1140
- Natural moisture content – ASTM D2216
- Corrosion Series:
 - pH – AASHTO T289
 - Chloride – AASHTO T291
 - Sulfate – AASHTO T290
 - Resistivity – AASHTO T288
- Unit Weight – ASTM D2166
- Consolidated undrained triaxial shear – ASTM D4767

Tables summarizing the laboratory test results are provided after this report as follows:

- gINT Summary of Laboratory Test Results,
- Table 2: Undisturbed Samples – Laboratory Classification & Shear Strength Testing Summary

The laboratory test data sheets are organized into appendices of this report as summarized below:



- Appendix VI – Laboratory Test Data Sheets – Split Spoon Samples (includes gINT Index Properties vs. Depth, Grain Size Distribution, and Atterberg Limits Results)
- Appendix VII – Laboratory Test Data Sheets – Corrosion Series Testing
- Appendix VIII – Laboratory Test Data Sheets – Undisturbed Samples

Electronic data files, including gINT project files are included as Appendix X.

7.0 Subsurface Conditions

Assessment of the geotechnical conditions included review of available topographic, geologic and soils maps for relevant information.

7.1 Area Geology

From our review of the *Geologic Map of the Blythewood Quadrangle, Richland and Fairfield Counties, South Carolina 1962*, prepared by the South Carolina Geological Survey, the site maps as being location along the fall-line separating the Coastal Plain and Piedmont physiographic providences of South Carolina.

The site maps as lying within the White Sand Hills Physiographic Region of the Upper Coastal Plain of South Carolina. The White Sand Hills form the most inland portion of the Coastal Plain and are underlain by mostly sandy Upper Cretaceous age sediments of the Cape Fear and Eutaw formations. These soils were eroded from a range of mountains in the northwest portion of the state approximately 65,000,000 years ago and laid down in their present positions as fan deposits, where they have weathered in place. In the Columbia metropolitan area these sediments rest unconformably on top of the underlying late-Proterozoic age Piedmont rocks of the Persimmon Fork formation at depths of between 20 and 120 feet. Massive, buff, or tan kaolin beds are prevalent throughout the sequence, alternating with coarse-grained water-bearing sands and gravels which become increasingly prevalent near the base of the formation. Soil layers exhibit considerable lateral and vertical discontinuity. In many areas groundwater is relatively shallow and supports heavy forest cover. Fresh soil exposures are typically white, but become pink, purple, or rusty orange with weathering. Iron-oxide cemented sandstone beds are common. In the local area, Coastal Plain sediments have been deeply eroded, exposing underlying Piedmont residuum and weathered rock in some of the deeper swales and depressions.

The underlying Piedmont residuum consists of soils weathered in place from the parent crystalline bedrock material. Residual soils of the Carolina Piedmont consist of stiff or very stiff micaceous silts and clays, grading to firm sands with depth. These soils have been completely weathered in place from the parent bedrock material, and consist, mostly of fine grained schists and phyllites of the Carolina Slate Belt. There are a number of volcanic intrusive sill or dikes comprised of diabase, where hard rock lies within a few feet of the surface. Elsewhere the soil residuum retains nearly all of the relict rock foliation or bedding structure below a depth of a few feet. Soil strength derives largely from relict intermolecular bonding and remolded materials generally exhibit lower shear strength than do undisturbed samples. Piedmont soils are normally consolidated to slightly over-consolidated.

The term *partially weathered rock (PWR)* is applied to very dense micaceous sands or silty sands of the Carolina Piedmont, which register SPT N-values in excess of 100 blows per foot. PWR generally varies widely within even small areas owing to minute differences in the chemical properties of the parent bedrock, which results in widely



varying rates of weathering. Isolated lenses or seams of PWR often are present within Piedmont Residuum well above the overall PWR level within a given area. PWR is considered excellent bearing material for foundations and is relatively incompressible except in highly stressed deep foundations.

Subsequent geologic processes may mask the contact between the Piedmont and Coastal Plain over localized areas. Over geologic time erosion of the Coastal Plain and Piedmont sediments has occurred from higher elevations, with the eroded materials deposited as Quaternary-aged alluvial sediments along streams, rivers, and their associated floodplains. In most cases the recent alluvial sediments are soft and compressible since they have never been consolidated under loads in excess of their own weight.

It appears that portions of the natural geological profile of the site have been modified by past grading activities that appear to have resulted in the placement of fill and the disturbance of the near surface soils. Please keep in mind that fill and disturbed soils can vary in composition and consistency, and the engineering characteristics of these soils can be difficult to predict. There is no specific correlation between the degree of compaction of the existing fill or the amount of disturbance of the near surface soils from the results of standard penetration testing. However, a qualitative assessment of existing fill and the disturbed soils can often be made based on visual observation of these materials sampled in the borings/test pits and the general magnitude of the standard penetration test values and difficulty of excavation.

7.2 Soil and Rock Stratification

The generalized subsurface conditions at the site are described below. Interpreted subsurface cross-sectional profiles are attached as Figures 3 through 5 in Appendix I. The discussed subsurface description is of a generalized nature to highlight the major subsurface stratification features and material characteristics. The boring records included in Appendix III should be reviewed for specific information at each boring location. The depth and thickness of the subsurface strata indicated on the boring records was estimated based on the drill cuttings and the samples recovered. The transition between materials may be more gradual than indicated on the boring records. Information on actual subsurface conditions exists only at the specific boring locations and is relevant to the time the exploration was performed. Variations may occur and should be expected at locations remote from the boring. The stratification lines were used for our analytical purposes and, unless specifically stated otherwise, should not be used as the basis for design or construction cost estimates.

A summary of the stratification across the project area is provided below.

Table 7-1 – Soil Stratification Table

Geotechnical Strata Designation	USCS Soil Class	Average Depth Interval Range (ft)	Elevation Interval Range (ft MSL)	Range of Raw SPT N-values (bpf)
Existing Fill	SM, SC, CL	0 to 6	466.3 to 447.8	3 to 32
Alluvium (boring W-2 only)	SC	4 to 10	447.8 to 441.8	3
Upper Cretaceous Coastal Plain	SP-SM, SM, SC, ML, CL, CH	0 to 28	462.0 to 435.1	4 to 50/2"



Piedmont Residuum	GM, ML, CL, MH	23 to 98	445.6 to 416.8	17 to 85
Partially Weathered Rock	ML	13 to 100	440.6 to 354.8	50/5" to 50/1"

7.2.1 Surface Material

Surface material, in the form of topsoil, was encountered at the existing ground surface at most soil boring locations. Existing topsoil thicknesses typically ranged from roughly ½ to 6 inches.

7.2.2 Existing Fill

Existing fill was encountered along the alignment in the vicinity of existing Community Road and I-77 Southbound (interior bents 2, 3 and 7, end bent 6, and MSE wall No. 2) to depths ranging from less than 1 foot to about 6 feet. Existing fill consisted of silty sands (SM), clayey sands (SC), and sandy lean clays (CL).

Recovered samples were dry to moist to the touch and were varying hues of brown, red, yellow, gray, and white. SPT N-values ranged from 3 to 32 blows per foot (bpf), indicating very loose to dense relative densities in sandy soils and very stiff consistency in clayey soils.

7.2.3 Alluvium

Alluvium was encountered at boring W-2 to a depth of roughly 10 feet below the existing ground surface. The alluvial deposits consisted of clayey sands (SC) and contained organics and fine gravels.

Recovered samples were dry to wet to the touch and were varying hues of gray. SPT N-values ranged of 3 bpf, indicating very loose relative densities.

7.2.4 Upper Cretaceous Coastal Plain Deposits

Coastal Plain deposits were encountered across the project area to depths ranging from roughly 9½ feet to 28½ feet below the existing ground surface. Coastal Plain deposits consisted of sands with varying amounts of fines (SP-SM, SM and SC) and low to high plasticity fines with varying amounts of sands (ML, CL and CH).

Recovered samples were dry to moist to the touch and were varying hues of olive, brown, red, yellow, gray, and white, pink, and black. SPT N-values ranged from 4 to 50/2" bpf, indicating very loose to very dense relative densities in sandy soils and soft to very hard consistencies in clayey and silty soils. Higher penetration resistances within the Coastal Plain deposits are likely due to the presence of gravels and/or cemented layers.

7.2.5 Piedmont Residuum

Beneath the native Coastal Plain deposits, the borings across the project area encountered Piedmont residual soils to depths ranging from roughly 13½ to 100 feet below the existing ground surface. Piedmont residuum consisted of low to high plasticity fines with varying amounts of sands (ML, CL and MH) with isolated silty gravel with some low plasticity fines (GM).



Recovered samples were dry to moist to the touch and were white, red, yellow, pink, brown, green, gray, and olive in color. SPT N-values ranged from 17 to 85 bpf, indicating medium dense to very dense relative densities in sandy soils and very stiff to very hard consistencies in silty and clayey soils.

7.2.6 *Partially Weathered Rock (PWR)*

Partially weathered rock (PWR) was predominately encountered lowermost beneath the Piedmont residuum soils to the termination depths of our borings. Intermittent seams of residuum soils also were encountered within the PWR layer. PWR is defined as a very dense or very hard residual material exhibiting SPT N-values in excess of 100 bpf.

Recovered samples of PWR consisted mostly of silts with varying amounts of sands (ML). Split-spoon samples were dry to wet to the touch and were yellow, pink, white, brown, black, olive, red, green, gray, and blue in color.

7.2.7 *Ground Water*

Observation of ground water in the borings was not possible at time of drilling due to the mud rotary drilling techniques used to advance the boreholes. Depth to ground water was measured in most boreholes at least 24 hours after completion of drilling. These measured ground water depths ranged from about 9 to 30 feet below the existing ground surface (approximate elevation +436 feet to +451 feet). Depth to ground water was not reported at 24 hours in borings EB-1C and EB-6C.

7.3 Shear Wave Velocity Measurement

Shear wave velocity measurements were made using DHSW methods within the cased borehole of EB-1C. The shear wave velocity profile depicted resolves into vertical intervals of roughly 3 feet. Velocity measurements were obtained to a depth of about 97 feet below the existing ground surface. A best-fit profile determined from the scatter of the data may be expressed as a shear wave velocity ranging from about 1,000 feet per second (fps) within the upper 5 feet, then increasing to about 2,750 fps around roughly 17 feet to 20 feet, then decreasing to values ranging between 2,100 and 2,600 fps to a depth of roughly 40 feet, then increasing to values ranging between about 3,000 fps to about 3,600 fps to a depth of roughly 65 feet and then between 2,740 fps to about 3,200 fps to near termination.

8.0 Seismic Design

8.1 Acceleration Design Response Spectrum (ADRS)

The results of the DHSW testing at this bridge, as well as testing conducted at the Ramp BA bridge over I-77, and US-21 bridge over Norfolk Southern Railroad were provided to the SCDOT Design/Build RPG for the purposes of establishing seismic design parameters for the overall project. The 3-Point Acceleration Design Response Spectrum (ADRS) provided by the SCDOT for the I-77 Exit 26 Project is included in Appendix IX. The overpass bridge was provided to have a bridge Operational Classification (OC) of "II" (OC II). The bridge embankment, defined as the portion of the approach embankment including the front slope plus 3.25 times the backwall height measured from the end of the approach slab, would extend approximately 33 feet beyond the end of approach



slab, or roughly 53 feet beyond the end bents on each abutment based on the Conceptual Bridge Plans. Roadway embankments beyond the bridge embankment do not require seismic hazard analyses.

The SCDOT Geotechnical Design Section provided pseudo spectral accelerations (PSA) for the Safety Evaluation Earthquake (SEE) (3% probability of exceedance in 75 years) and the Functional Evaluation Earthquake (FEE) (15% probability of exceedance in 75 years). These values were provided for the geologically realistic condition, 5% critical damping, and the peak ground acceleration (PGA) at the B-C boundary. The 3-point method was utilized to generate the ADRS curves provided in Appendix IX. The design parameters derived from these curves are detailed in the table below.

Table 8-1 – Seismic Design Parameters

Seismic Design Parameter	Acceleration (g)
PGA-FEE	0.20
SDS-FEE	0.32
SD1-FEE	0.06
PGA-SEE	0.41
SDS-SEE	0.77
SD1-SEE	0.16

Seismic Design Category (SDC) designation of a structure from A to D determines the level of analysis and detailing required. SDC is determined by the bridge operational classification (OC) and the design spectral response acceleration for the SEE event at the one-second period. The long period acceleration SD1-SEE is < 0.30 g. Per Table 3.5 of the *SCDOT Seismic Design Specifications for Highway Bridges (2008)*, Seismic Design Category (SDC) based on these parameters for an OC Level II structure is A.

8.2 Preliminary Seismic Evaluation

In order to evaluate the need for ground improvement, the potential for soil liquefaction and soil strength loss (SSL) were examined for sand-like cyclic liquefaction potential and clay-like cyclic softening utilizing screening procedures outlined in GDM Chapter 13. This methodology was used to determine lateral displacement and one-dimensional reconsolidation settlement of liquefied soils due to seismic loads. Soils above the water table, which includes portions of the existing fill, alluvium, Coastal Plain deposits and Piedmont, were considered as unsaturated and non-susceptible. Due to the geologic age, density and consistency of the Coastal Plain deposits, Piedmont residual soils and partially weathered rock (PWR), these soils were also considered non-susceptible.

Very loose alluvial clayey sands located below the water table were encountered in boring W-2 only. This boring was located in the vicinity of the northern portion of the planned abutment retaining wall at End Bent 5, offset approximately 40 feet east from the face of the wall. These alluvial soils due to their relatively young geologic age and relative density will likely be susceptible to sand-like liquefaction and resulting volumetric compaction. As the boring was offset somewhat from the planned wall, additional subsurface data may be necessary in this area to further explore the vertical and lateral extent of the alluvial deposits. With the exception of the isolated retaining wall area above, SSL does not appear to be a credible hazard with respect to the proposed bridge construction.



9.0 Design and Construction Considerations

Chapter 21 of the SCDOT GDM provides that the GBR should provide limited (preliminary) geotechnical information on a D/B project, thus permitting the contractor to bid on the project with a certain degree of knowledge and acceptable risk. The preliminary design and construction considerations submitted herein are based, in part, upon data obtained from our field exploration and laboratory testing program. Subsurface conditions across the site will vary, as will grading and construction details. Additional geotechnical exploration and analysis may be required to provide detailed analysis and recommendations for the project.

9.1 Drilled Deep Foundations

Drilled shaft foundations are possible for support of the bridge interior bents. We anticipate that drilled shafts for the bridge could range from 36 to 60 inches in diameter. Due to the subsurface conditions encountered, we anticipate that the drilled shafts will be socketed into the underlying PWR to provide the required axial and lateral resistance.

Bedrock was not encountered at the boring locations for this portion of the project. Therefore, difficult drilling and deeper penetration into the PWR may be required to achieve proper bearing and lateral stability for the bridge foundations. Individual shafts may encounter ledges, boulders or seams of relatively hard rock within the PWR zone overlying competent bedrock, which may require special measures to permit advancement to the required bearing.

Due to the ground water conditions encountered in our borings, we anticipate drilled shafts will be installed using the wet method of construction with casing described in SCDOT Standard Specification Section 712.4.5. Steel casing should be advanced and seated into the top of PWR or rock to provide an effective seal. If an effective seal is established, the drilled shaft contractor may be able to effectively dewater the hole and maintain the stable bottom until concrete is placed. However, if the casing penetrates to less competent material and an effective seal is not obtained, or if the competent material does not extend over the entire base of the drilled shaft, it is likely that the water head in the deeper shafts will cause severe softening and necessitate additional depth of drilling to reach a stable bottom. In this case, wet construction installation methods using a drilling slurry as described in SCDOT Standard Specification Section 712.4.5 may be required to stabilize the hole and allow placement of concrete.

The overburden soil materials consisting of the existing fill, Coastal Plain deposits and Piedmont residual soils can typically be excavated with a conventional earth auger. PWR or very poor to poor quality rock will necessitate use of a rock auger advanced by a large foundation drilling rig. Contractor should be required to provide augering equipment with adequate torque and power to install drilled shafts through very dense PWR and very poor to poor quality rock using augers with hardened tungsten carbide bits. The speed of excavation depends upon the type of material being penetrated, size of foundation element and size of the drilling rig. Individual shafts may encounter ledges, boulders or seams of relatively hard rock within the partially weathered rock zone overlying competent bedrock. Specialized drilling equipment may be required due to the observed PWR consistencies, depending on required penetration depths. This may include, but not be limited to rock augers, core barrels, or rotary percussion drilling equipment.



Ground water control is important during construction of drilled shafts. Due to the observed ground water along the bridge alignment, ranging from roughly 9 to 30 feet below the existing ground surface, it may be necessary to use telescoping casing installation methods to achieve the planned casing tip elevations.

9.1.1 *Resistance Criteria*

Axial resistance will likely govern the geotechnical foundation design and be developed in end bearing in the underlying PWR, as well as side resistance in the uncased portion of the shaft. Development of lateral resistance of the drilled shafts should be achievable in the Piedmont residuum and underlying PWR.

9.2 Driven Deep Foundations

Driven steel H-pile foundations are typically preferred for end bent support by SCDOT. Piles are anticipated to bear on/within very dense/very hard PWR. Driven steel H-piles are advantageous due primarily to their relative cost and ease for pile splicing and cutting. Piles are commonly paid for on an "in-place" basis and no charge is made for the length of steel cut off. The principal disadvantage associated with steel H-piles are their relatively small tip areas, which can result in very small end bearing resistance in residual soils since formation of a soil plug cannot be counted on in all cases to help with end bearing capacity development, hence piles will need to extend to sufficient depth to bear on/within PWR or rock. Nominal pile resistance will be essentially the allowable stress of the steel pile cross sectional area in this case.

9.2.1 *Driving Considerations*

The contractor should take care not to overdrive or overstress the piles during driving. Prior to installing piles, a wave equation analysis should be performed to evaluate whether the Contractor's proposed driving system (i.e., hammer type and size) is capable of efficiently driving the piles to the desired depths without damaging the piles, and to establish driving criteria. Per the GDM, practical refusal is defined as 5 blows per quarter ($\frac{1}{4}$) inch or 20 blows per inch. Steel pile compressive stresses during driving should not exceed 0.9 times the yield strength of the steel section during driving. Because the PWR and argillite bedrock is anticipated to be very hard, we recommend that the piles be equipped with driving points or shoes to protect the pile from damage during driving. Due to the presence of very dense gravelly or cemented layers within the Coastal Plain deposits on both the east and west sides of the bridge, pre-drilling and/or penetration aids may be needed to facilitate pile installation.

9.2.2 *Resistance Criteria*

Axial resistance will likely govern the geotechnical foundation design and be developed in end bearing on the underlying PWR with some contribution from skin friction in the soils above the pile tip elevation. Development of lateral resistance of the pile foundations should be achievable in the Coastal Plain soils, Piedmont residuum and underlying PWR, however, adequate depth for lateral resistance may require pre-drilling and/or penetration aids as previously discussed.



9.3 Roadway Embankments

Fill embankments of up to approximately 29 feet in height supported by MSE walls at the abutments will be required to achieve planned grades. Fill slope areas should be prepared, and fill materials placed, in accordance with the SCDOT *Standard Specifications for Highway Construction*.

9.3.1 *Undercutting/Surface Stabilization*

The majority of the split-spoon samples obtained just below the ground surface were typically classified as silty and clayey soils ranging from A-2-4 to A-6 using the AASHTO classification system which typically provide a suitable subgrade for fill placement. Select penetration resistances in the upper 2 to 4 feet indicated very loose to loose conditions in the sandy soils. Therefore, some stabilization of the near surface sandy soils may be required prior to fill placement. This can typically be accomplished with a vibratory roller and is standard practice under the SCDOT *Standard Specifications for Highway Construction*.

9.3.2 *Imported Fill/Borrow*

As the site is located in Blythewood, Richland County, South Carolina, Group B, per Section 203.2.1.8 of the SCDOT *Standard Specifications for Highway Construction*, would apply to borrow soils allowed for use as fill.

9.3.3 *Slope Stability*

Although planned slopes are typically shown at 2H:1V to 3H:1V on the conceptual plans, global stability of both cut and fill slopes will need to be evaluated as part of design development by the successful team due to the height of the slopes. Per SCDOT GDM, embankments constructed within the limits of the bridge embankment must be designed and evaluated under both service and extreme event limit states, while the remaining roadway embankments will only require service limit state evaluation.

9.3.4 *Compression and Settlement*

Since portions of the alignment will have fill heights in excess of 29 feet, long term differential settlements resulting from even minor volume changes in the fill (measured in percent of fill height) could be substantial and must be accounted for in design. Therefore, the performance objectives of the GDM and project team should consider the potential for these settlements in evaluation efforts.

Immediate settlements include self-weight compression of the fill mass during and immediately following fill placement. Typically, in sandy alluvial soils, Upper Cretaceous Coastal Plain deposits and Piedmont residuum, these settlements are built out during placement of successive lifts and do not contribute substantially to post construction settlement. However, depending on sequence of construction of end bent piles, MSE walls or other ERS structures self-weight compression may be applicable to downdrag calculations or to wall settlements. Contractor design submittals will need to address how initial compression of soils placed around structures will be accommodated.

In most areas explored, a majority of settlements are anticipated to occur during construction, prior to paving operations, because soils providing support for the new fill consist of mostly existing sandy alluvial and Coastal



Plain deposits with layers of very stiff to hard silts and clays. Compression due to consolidation under these conditions is anticipated to be rapid and indistinguishable from immediate settlement. Therefore, it is not expected that post construction settlements will exceed performance objectives. Compression/consolidation testing was not performed at this time, therefore, depending on the performance objectives, additional testing consisting of, but not necessarily limited to, laboratory consolidation testing or in-situ testing by cone penetration or flat-blade dilatometer soundings may be required by the D/B Contractor.

9.4 Earth Retaining Structures

As discussed, MSE retaining walls are planned at the following locations:

- MSE Wall No. 1 – Connector Road Bridge western embankment along Community Road at roughly Station 146+34,
- MSE Wall No. 2 – Connector Road Bridges eastern embankment along I-77 Northbound at roughly Station 149+69, and
- MSE Wall No. 3 – CONRPC Entrance Ramp embankment at roughly Station 1730+34.

Per the GDM, earth retaining structures must be designed and evaluated for internal and external stability. Abutment walls at the end bents of the overpass must be designed for internal stability and external stability, including bearing capacity, overturning, sliding and global stability, under service and extreme event limit states. MSE walls at the bridge abutments will have end bent deep foundations within the reinforced zone, therefore, construction sequencing and protection of the reinforcement around the piles should be considered. Deep foundations installed prior to MSE wall fill placement may be subjected to downdrag forces caused by immediate and consolidation settlements.

9.5 Vibration Monitoring Assessment

Per the requirements of Table 24-6 of the GDM, it does not appear that vibration monitoring will be required. The planned bridge, retaining wall, and bridge embankment construction does not appear to be located within the distances from potential receptors that would require monitoring.

9.6 Corrosion Potential Results

Corrosion series testing was performed to determine the potential for material deterioration of the proposed foundations. Six (6) composite samples were taken from selected recovered samples of Borings EB-2C, EB-3C, EB-5C, IB-1C, IB-7C, and IB-11C to perform pH, resistivity, sulfate, and chloride geochemical tests. These borings are representative of end and interior bents along the alignment. The samples were selected based on their proximity to the estimated soil/pile/ground water interface elevation.

Table 9-1 – Summary of Corrosion Series Testing

Sample	Depth (feet)	Minimum Resistivity (ohm-cm)	Sulfate Content (ppm)	Chloride Content (ppm)	pH
EB-2C (SS-8)	23.5-25	56,950	21.7	49.3	6.9



EB-3C (SS-6)	13.5-15	34,840	30.6	77.1	6.0
EB-5C (SS-10)	33.5-35	67,000	27.2	62.9	7.0
IB-1C (SS-6)	13.5-15	40,200	43.1	105.7	5.7
IB-7C (SS-7)	18.5-20	67,000	25.4	75.7	5.6
IB-11C (SS-7)	18.5-20	58,290	26.5	59.9	6.8

The complete laboratory testing results of the corrosion series testing are provided in Appendix VII.

Section 7.18 of the GDM provides guidance on determining corrosion potential or aggressiveness. The following soil conditions from GDM Table 7-34 suggest aggressive conditions:

- pH less than 5.5;
- Sulfate concentrations greater than 1,000 ppm (mg/kg); and
- Resistivity less than 2,000 ohm-cm.

Therefore, the site appears to be non-aggressive for foundations. However, interpretation of the data and corrosion protection of structural components shall be reviewed and provided by the structural engineer during the design phase of the project.

10.0 Closing

This report has been prepared in accordance with generally accepted geotechnical engineering practice for specific application to this project. The conclusions and recommendations contained in this report are based upon applicable standards of our practice in this geographic area at the time this report was prepared. No other warranty, express or implied, is made.

We relied on project information given to us to develop our conclusions and recommendations. If project information described in this report is not accurate, or if it changes during project development, we should be notified of the changes so that we can modify our recommendations based on this additional information if necessary.

Our conclusions and recommendations are based on limited data from a field exploration program. Subsurface conditions can vary widely between explored areas. Some variations may not become evident until construction. If conditions are encountered which appear different than those described in our report, we should be notified. This report should not be construed to represent subsurface conditions for the entire site.

Unless specifically noted otherwise, our field exploration program did not include an assessment of regulatory compliance, environmental conditions or pollutants or presence of any biological materials (mold, fungi, bacteria). If there is a concern about these items, other studies should be performed. S&ME can provide a proposal and perform these services if requested.

S&ME should be retained to review the final plans and specifications to confirm that earthwork, foundation, and other recommendations are properly interpreted and implemented. The recommendations in this report are



contingent on S&ME's review of final plans and specifications followed by our observation and monitoring of earthwork and foundation construction activities.

Appendices

Appendix I – Figures



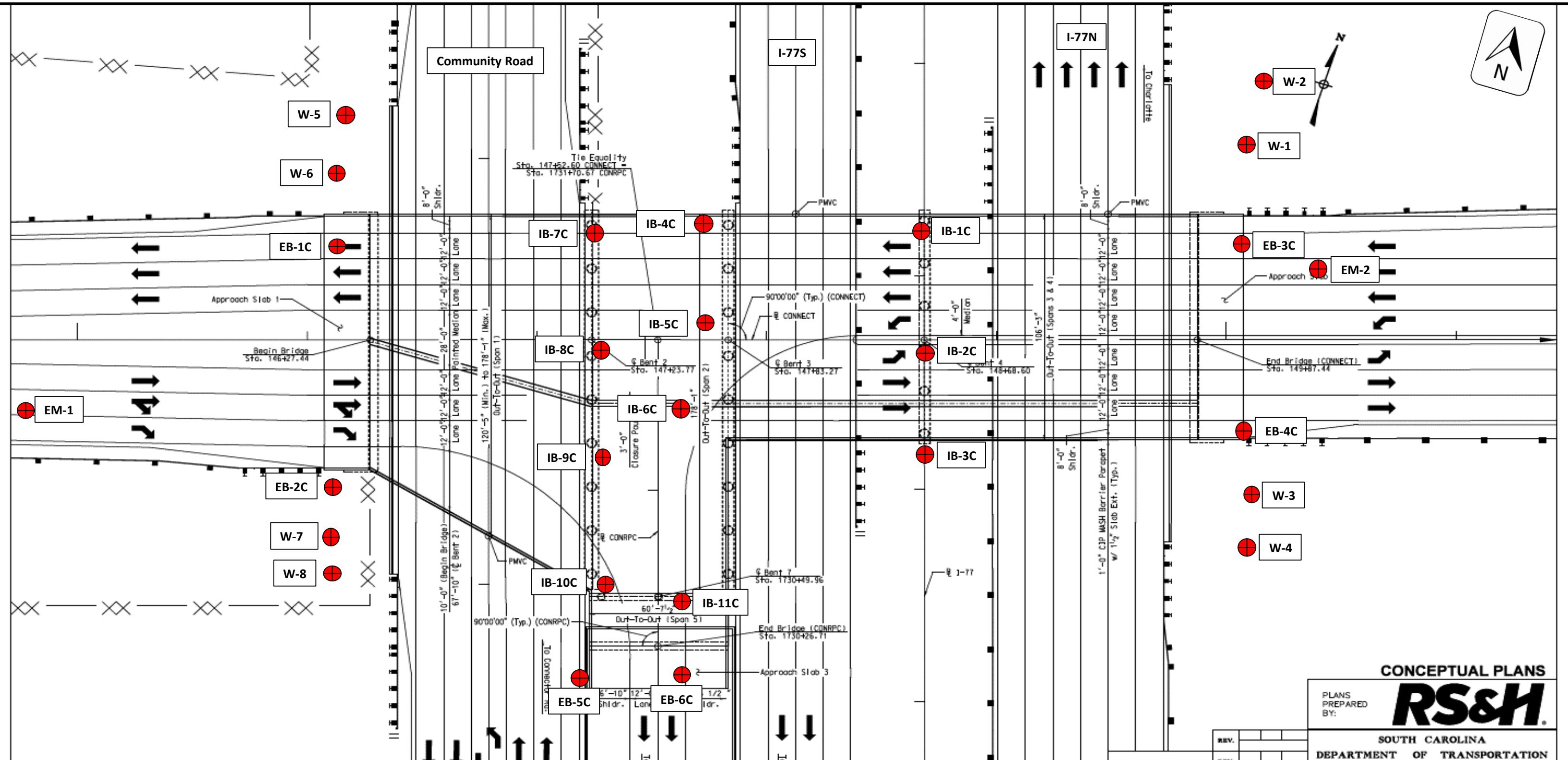
SOURCE: USGS National Map



SITE LOCATION PLAN

JOB NAME:	Connector Road Bridge over I-77 I-77 Exit 26 Interchange	FIGURE NO.
CITY, STATE:	Blythewood, Richland County, South Carolina	
S&ME PROJECT NO.:	23610178A	
SCALE:	NTS	CHECKED BY: JPL
DATE:	1/12/2024	DRAWN BY: HMS

1



SPT Soil Test Boring - Approximate Location



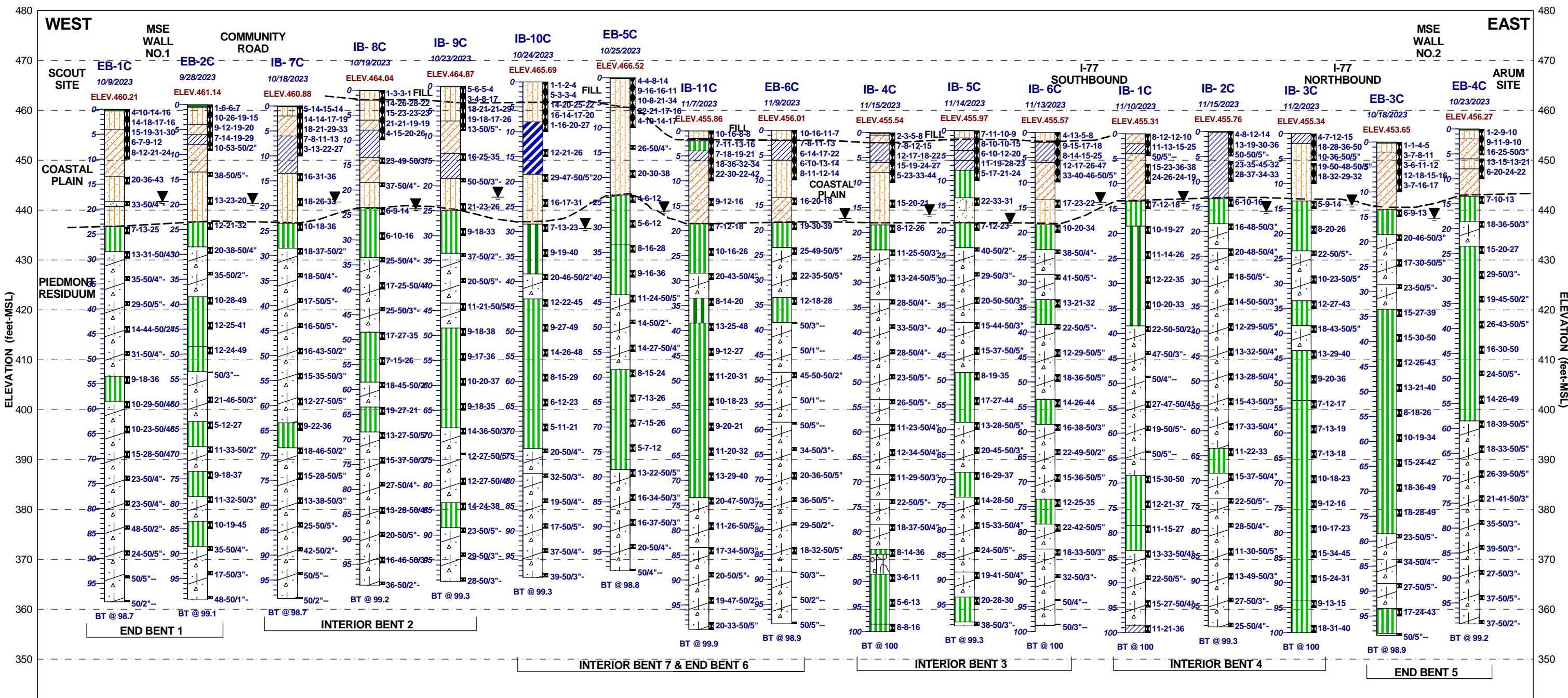
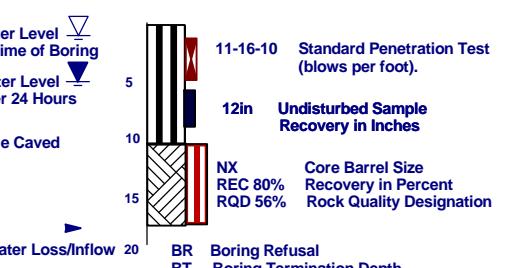
Test Location Plan

JOB NAME:	Connector Road Bridge over I-77 I-77 Exit 26 Interchange	
CITY, STATE:	Blythewood, Richland County, South Carolina	
S&ME JOB NO.:	23610178A	
SCALE:	NTS	CHECKED BY: JPL
DATE:	1/12/2024	DRAWN BY: HMS

BENT 1 F.G. = 485.7

CONNECTOR ROAD

BENT 5 F.G. = 483.5

SOIL TEST BORINGS
B-3 Boring Number
123.0 Elevation at GS

LEGEND OF MATERIAL GRAPHICS FOR SOIL TEST BORINGS

Topsoil	SM, Silty Sand	SC, Clayey Sand	Poorly-graded Sand with Silt
ML, Low Plasticity Silt	SC DOT: Saprolite	CL, Low Plasticity Clay	CH, High Plasticity Clay
GM, Silty Gravel			

SUBSURFACE PROFILE

PROJECT: Connector Road Bridge over I-77
LOCATION: Blythewood, Richland County, SC
FIGURE: 3

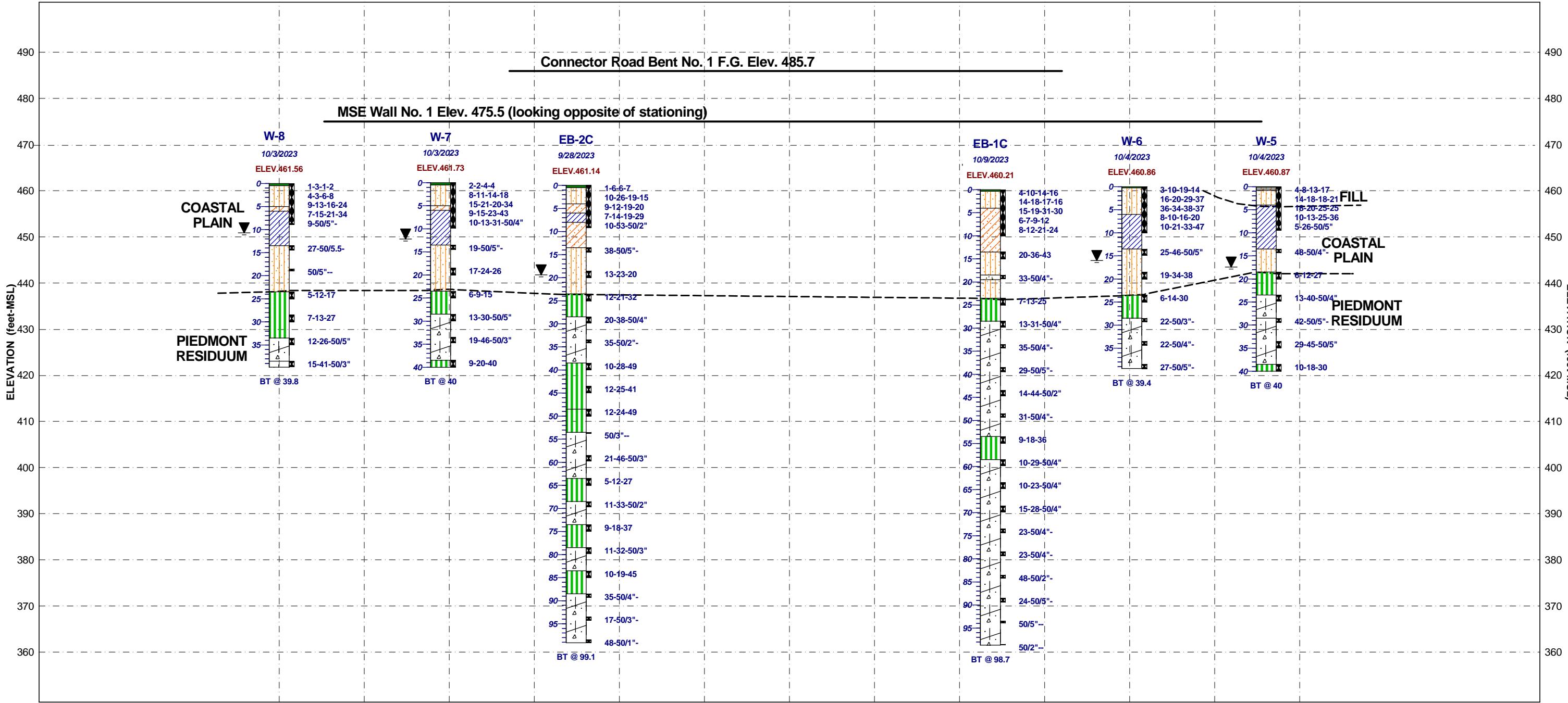
JOB NO: P042443-B01
S&ME 23610178A
DATE:
January 2024



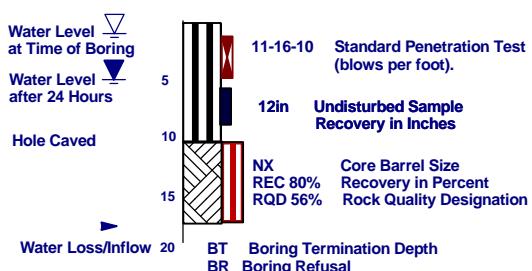
The depicted stratigraphy is shown for illustrative purposes only and is not warranted. Separations between different strata may be gradual and likely vary considerably from those shown. Profiles between nearby borings have been estimated using reasonable engineering care and judgment. The actual subsurface conditions will vary between boring locations.

SOUTH

NORTH



SOIL TEST BORINGS
B-3 Boring Number
123.0 Elevation at GS

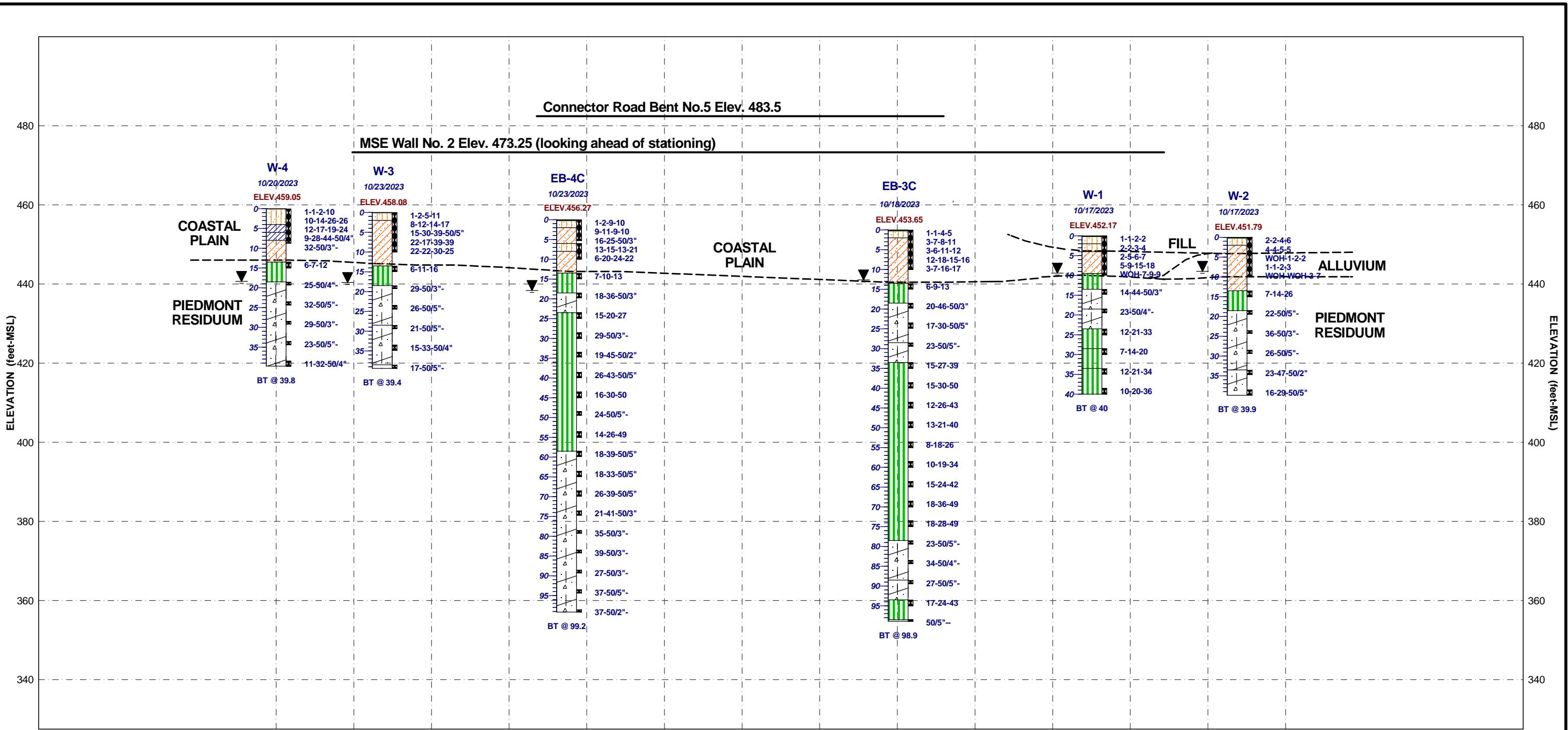


LEGEND OF MATERIAL GRAPHICS FOR SOIL TEST BORINGS

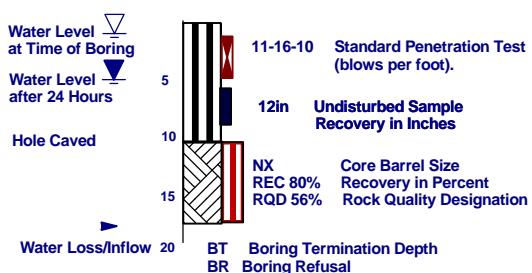
SUBSURFACE PROFILE		JOB NO: P042443
PROJECT: Connector Road Bridge over I-77 - MSE Wall No.1		S&ME 23610178A
LOCATION: Blythewood, Richland County, SC		DATE:
FIGURE: 4		January 2024



The depicted stratigraphy is shown for illustrative purposes only and is not warranted. Separations between different strata may be gradual and likely vary considerably from those shown. Profiles between nearby borings have been estimated using reasonable engineering care and judgment. The actual subsurface conditions will vary between boring locations.



SOIL TEST BORINGS
B-3 Boring Number
123.0 Elevation at GS



LEGEND OF MATERIAL GRAPHICS FOR SOIL TEST BORINGS

Topsoil	SM, Silty Sand	SC, Clayey Sand	ML, Low Plasticity Silt
CL, Low Plasticity Clay			

SUBSURFACE PROFILE

PROJECT: Connector Road Bridge over I-77 - MSE Wall No. 2

LOCATION: Blythewood, Richland County, SC

FIGURE: 5

JOB NO:P042443

S&ME 23610178A

DATE:

January 2024

The depicted stratigraphy is shown for illustrative purposes only and is not warranted. Separations between different strata may be gradual and likely vary considerably from those shown. Profiles between nearby borings have been estimated using reasonable engineering care and judgment. The actual subsurface conditions will vary between boring locations.



Appendix II – Tables



Table 1: Boring Location Summary

Test ID	SC State Plane Northing (ft.)	SC State Plane Easting (ft.)	Latitude (degrees)	Longitude (degrees)	Elevation (ft-NAVD88)	Alignment	Station	Offset (ft)
EB-1C	857824.4801	2004705.038	34.19106	-80.98444	460.2	Connector Rd	146+03.10	-41.8
EB-2C	857707.6487	2004740.711	34.19074	-80.98432	461.1	Connector Rd	146+01.12	80.3
EB-3C	857947.6434	2005087.268	34.19140	-80.98318	453.7	Connector Rd	150+04.68	-41.5
EB-4C	857866.9345	2005115.233	34.19118	-80.98308	456.3	Connector Rd	150+06.47	43.9
EB-5C	857679.1745	2004878.973	34.19067	-80.98387	466.5	Connector Rd	147+23.93	149.9
EB-6C	857693.9224	2004919.687	34.19071	-80.98373	456.0	Connector Rd	147+67.20	148.4
EM- 1	857728.4249	2004659.089	34.19080	-80.98459	458.6	Connector Rd	145+29.84	35.5
EM- 2	857955.704	2005144.865	34.19143	-80.98299	452.4	Connector Rd	150+61.97	-31.4
IB- 1C	857902.4187	2004958.401	34.19128	-80.98360	455.3	Connector Rd	148+68.15	-38.1
IB- 2C	857857.2285	2004973.005	34.19115	-80.98355	455.8	Connector Rd	148+68.15	9.4
IB- 3C	857810.7103	2004988.218	34.19103	-80.98350	455.3	Connector Rd	148+68.32	58.4
IB- 4C	857887.3402	2004858.218	34.19124	-80.98393	455.5	Connector Rd	147+68.19	-54.5
IB- 5C	857842.3156	2004872.049	34.19111	-80.98389	456.0	Connector Rd	147+67.50	-7.4
IB- 6C	857801.726	2004886.164	34.19100	-80.98384	455.6	Connector Rd	147+68.45	35.5
IB- 7C	857865.5314	2004809.165	34.19118	-80.98410	460.9	Connector Rd	147+14.80	-48.9
IB- 8C	857812.477	2004828.854	34.19103	-80.98403	464.0	Connector Rd	147+17.23	7.7
IB- 9C	857765.6801	2004846.023	34.19090	-80.98397	464.9	Connector Rd	147+19.17	57.5
IB-10C	857722.9571	2004860.803	34.19079	-80.98393	465.7	Connector Rd	147+20.10	102.7
IB-11C	857727.5795	2004909.586	34.19080	-80.98376	455.9	Connector Rd	147+67.94	113.3
W- 1	857995.7737	2005073.872	34.19154	-80.98322	452.2	Connector Rd	150+06.74	-91.4
W- 2	858033.7625	2005069.856	34.19164	-80.98323	451.8	Connector Rd	150+14.60	-128.8
W- 3	857823.3911	2005134.903	34.19106	-80.98302	458.1	Connector Rd	150+11.80	91.4
W- 4	857796.1012	2005139.3	34.19099	-80.98300	459.1	Connector Rd	150+07.59	118.7
W- 5	857888.4762	2004685.494	34.19124	-80.98450	460.9	Connector Rd	146+04.18	-108.7
W- 6	857856.3829	2004693.853	34.19115	-80.98448	460.9	Connector Rd	146+02.27	-75.6
W- 7	857686.7333	2004746.157	34.19069	-80.98430	461.7	Connector Rd	145+99.87	101.9
W- 8	857670.9937	2004751.725	34.19064	-80.98429	461.6	Connector Rd	146+00.33	118.6

Notes: As-built coordinates and elevation provided by CES.

NA = NOT AVAILABLE



Table 2: Undisturbed Samples - Laboratory Classification, Unit Weight, & Shear Strength Testing Summary

Boring Number	Sample Number	Sample Depth (ft)	Test Type	Atterberg Limits		Percent Finer #200 (%)	Organic Matter Content (%)	USCS	AASHTO	Specific Gravity	Test Specimen Number	Initial Dry Unit Weight (pcf)	Initial Moisture Content (%)	Shear Strength Parameters											
																Total	Effective								
W-2	UD-1	5-7	ASTM D4767	25	12	29.2	TNP	SC	A-2-6(0)	2.65	1	113.7	5.1	0.297	21	0	34								
W-2	UD-2	7-9	ASTM D7263	18	4	42.6	TNP	SC-SM	A-4(0)	TNP	N/A	115.3	14.0	TNP	TNP	TNP	TNP								

NP = Non-plastic

TNP = Test Not Performed



SUMMARY OF LABORATORY RESULTS

PAGE 1 OF 3

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

Borehole	Depth	Liquid Limit	Plastic Limit	Plasticity Index	Maximum Size (mm)	%<#200 Sieve	Classification	Water Content (%)	Dry Density (pcf)	Saturation (%)	Void Ratio
EB-1C	0.0				4.75	27		2.0			
EB-1C	4.0				0.075	34		11.4			
EB-1C	23.5	44	33	11	0.075	87	ML	25.0			
EB-2C	0.0				4.75	20		4.1			
EB-2C	4.0	40	22	18	0.075	34	SC	12.9			
EB-2C	6.0	40	22	18	0.075	79	CL	23.2			
EB-2C	18.5	NP	NP	NP	0.075	20	SM	12.0			
EB-3C	0.0				4.75	36		8.1			
EB-3C	4.0	31	13	18	0.075	40	SC	13.2			
EB-3C	8.0	27	13	14	0.075	21	SC	13.5			
EB-3C	33.5	35	29	6	0.075	81	ML	26.4			
EB-3C	78.5	35	31	4	0.075	67	ML	23.9			
EB-3C	93.5	38	28	10	0.075	70	ML	23.3			
EB-4C	0.0				9.5	32		2.8			
EB-4C	6.0	37	26	11	0.075	44	SM	14.6			
EB-4C	8.0				0.075	29		15.3			
EB-4C	13.5	41	37	4	0.075	89	ML	28.7			
EB-5C	0.0				4.75	29		2.2			
EB-5C	6.0	NP	NP	NP	9.5	27	SM	10.0			
EB-5C	8.0	NP	NP	NP	9.5	39	SM	14.2			
EB-5C	23.5	49	41	8	0.075	93	ML	30.4			
EB-6C	0.0	NP	NP	NP	0.075	19	SM	4.5			
EB-6C	4.0	42	23	19	0.075	84	CL	19.1			
EB-6C	13.5	24	18	6	0.075	20	SC-SM	11.9			
EM- 1	0.0				4.75	18		1.5			
EM- 1	4.0				0.075	31		7.2			
EM- 1	8.0	36	25	11	0.075	88	ML	13.6			
EM- 2	0.0	NP	NP	NP	0.075	39	SM	9.5			
EM- 2	6.0	28	18	10	0.075	24	SC	13.3			
EM- 2	13.5	44	33	11	0.075	86	ML	26.4			
IB- 1C	0.0	34	16	18	0.075	45	SC	9.5			
IB- 1C	6.0	36	18	18	0.075	20	SC	10.2			
IB- 1C	18.5	58	38	20	0.075	59	MH	26.2			
IB- 2C	2.0	38	18	20	0.075	56	CL	13.5			
IB- 2C	13.5	46	30	16	0.075	83	ML	32.2			
IB- 3C	0.0	32	18	14	0.075	63	CL	10.9			
IB- 3C	8.0	NP	NP	NP	0.075	24	SM	14.7			
IB- 3C	13.5	46	36	10	0.075	81	ML	36.8			
IB- 4C	2.0	37	19	18	0.075	64	CL	13.5			
IB- 4C	8.0	NP	NP	NP	0.075	22	SM	9.9			
IB- 4C	18.5	44	32	12	0.075	66	ML	24.5			
IB- 4C	88.5	45	35	10	0.075	76	ML	31.2			
IB- 5C	2.0	41	19	22	0.075	65	CL	14.1			



SUMMARY OF LABORATORY RESULTS

PAGE 2 OF 3

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

Borehole	Depth	Liquid Limit	Plastic Limit	Plasticity Index	Maximum Size (mm)	%<#200 Sieve	Classification	Water Content (%)	Dry Density (pcf)	Saturation (%)	Void Ratio
IB- 5C	4.0	35	19	16	0.075	79	CL	16.6			
IB- 5C	13.5				0.075	11		12.3			
IB- 6C	0.0	NP	NP	NP	0.075	12		5.7			
IB- 6C	2.0	30	16	14	0.075	65	CL	8.8			
IB- 6C	6.0	37	17	20	0.075	41	SC	13.2			
IB- 7C	0.0				4.75	29		3.3			
IB- 7C	4.0	46	26	20	0.075	36	SC	13.0			
IB- 7C	8.0	37	18	19	0.075	79	CL	14.0			
IB- 7C	13.5				4.75	27		11.5			
IB- 7C	28.5	44	33	11	0.075	73	ML	25.3			
IB- 7C	63.5	39	33	6	0.075	79	ML	27.6			
IB- 8C	0.0				9.5	18		2.5			
IB- 8C	6.0	36	18	18	0.075	47	SC	13.8			
IB- 8C	8.0	37	16	21	0.075	76	CL	13.6			
IB- 8C	13.5	26	15	11	0.075	48	SC	12.1			
IB- 8C	23.5	42	32	10	0.075	80	ML	27.5			
IB- 8C	48.5	49	32	17	0.075	69	ML	29.0			
IB- 9C	0.0	NP	NP	NP	9.5	18	SM	2.0			
IB- 9C	8.0				0.075	27		12.6			
IB- 9C	13.5	30	17	13	0.075	67	CL	11.1			
IB-10C	0.0	NP	NP	NP	9.5	20	SM	2.6			
IB-10C	2.0				0.075	18		2.9			
IB-10C	8.0	50	27	23	0.075	52	CH	16.1			
IB-10C	18.5				0.075	22		10.1			
IB-10C	28.5	62	45	17	0.075	90	MH	28.6			
IB-11C	0.0	NP	NP	NP	9.5	19	SM	4.1			
IB-11C	2.0	42	28	14	0.075	69	ML	15.2			
IB-11C	6.0	29	18	11	0.075	38	SC	10.6			
IB-11C	33.5	67	46	21	0.075	71	MH	35.7			
W- 1	0.0				9.5	36		11.9			
W- 1	4.0	31	15	16	0.075	34	SC	13.8			
W- 1	23.5	38	28	10	0.075	63	ML	22.8			
W- 2	0.0				9.5	35		12.5			
W- 2	4.0	32	16	16	0.075	32	SC	16.9			
W- 2	8.0	32	14	18	0.075	18	SC	17.5			
W- 3	0.0				9.5	30		2.6			
W- 3	4.0	33	18	15	0.075	41	SC	14.1			
W- 3	8.0	29	17	12	0.075	32	SC	14.4			
W- 4	0.0				9.5	30		2.3			
W- 4	4.0	42	21	21	0.075	58	CL	15.7			
W- 4	8.0	33	17	16	0.075	35	SC	11.7			
W- 5	2.0				4.75	39		3.2			
W- 5	4.0	44	23	21	0.075	51	CL	10.5			



SUMMARY OF LABORATORY RESULTS

PAGE 3 OF 3

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

Borehole	Depth	Liquid Limit	Plastic Limit	Plasticity Index	Maximum Size (mm)	%<#200 Sieve	Classification	Water Content (%)	Dry Density (pcf)	Saturation (%)	Void Ratio
W- 5	13.5	NP	NP	NP	4.75	22	SM	10.1			
W- 6	0.0	NP	NP	NP	4.75	29	SM	2.1			
W- 6	6.0	34	18	16	0.075	85	CL	13.7			
W- 6	8.0	29	18	11	0.075	83	CL	11.9			
W- 6	13.5				9.5	22		8.9			
W- 7	0.0				4.75	19		2.0			
W- 7	6.0	34	18	16	0.075	84	CL	16.1			
W- 7	13.5				4.75	33		10.1			
W- 8	0.0				9.5	28		4.9			
W- 8	5.0	45	22	23	0.075	35	SC	16.7			
W- 8	6.0	33	19	14	0.075	81	CL	9.7			



Rock Coring Summary

PAGE 1 OF 1

PROJECT ID 23610178A

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

Borehole	Core Run Number	Core Run Top Depth	REC (%)	RQD (%)	q_u (psi)	Poisson's Ratio	Secant Modulus (ksi)	Unit Weight (pcf)	RMR	GSI
EB-1RB1	RC-1	52.5	47	0						
EB-1RB1	RC-2	57.0	88	65						
EB-1RB1	RC-3	62.0	100	25	2738	0.94	1080	151	23	15
IB-1RB1	RC-1	49.9	75	30	2786	0.82	770	153	23	5
IB-1RB1	RC-2	54.2	68	8						
IB-1RB1	RC-3	59.2	88	26						
IB-1RB1	RC-4	64.2	86	52	5644	0.21	6180	169	36	25
IB-1RB1	RC-5	69.2	83	8						

Appendix III – Soil Test Boring Records

LEGEND TO SOIL CLASSIFICATION AND SYMBOLS

SOIL TYPES

(Shown in Graphic Log)



Fill



Asphalt



Concrete



Topsoil



Gravel



Sand



Silt



Clay



Organic



Silty Sand



Clayey Sand



Sandy Silt



Clayey Silt



Sandy Clay



Silty Clay



Partially Weathered Rock



Cored Rock

WATER LEVELS

(Shown in Water Level Column)

- = Water Level At Termination of Boring
- = Water Level Taken After 24 Hours
- = Loss of Drilling Water
- HC = Hole Cave

CONSISTENCY OF COHESIVE SOILS

CONSISTENCY

STD. PENETRATION
RESISTANCE
BLOWS/FOOT

Very Soft	0 to 2
Soft	3 to 4
Firm	5 to 8
Stiff	9 to 15
Very Stiff	16 to 30
Hard	31 to 50
Very Hard	Over 50

RELATIVE DENSITY OF COHESIONLESS SOILS

RELATIVE DENSITY

STD. PENETRATION
RESISTANCE
BLOWS/FOOT

Very Loose	0 to 4
Loose	5 to 10
Medium Dense	11 to 30
Dense	31 to 50
Very Dense	Over 50

TERMS

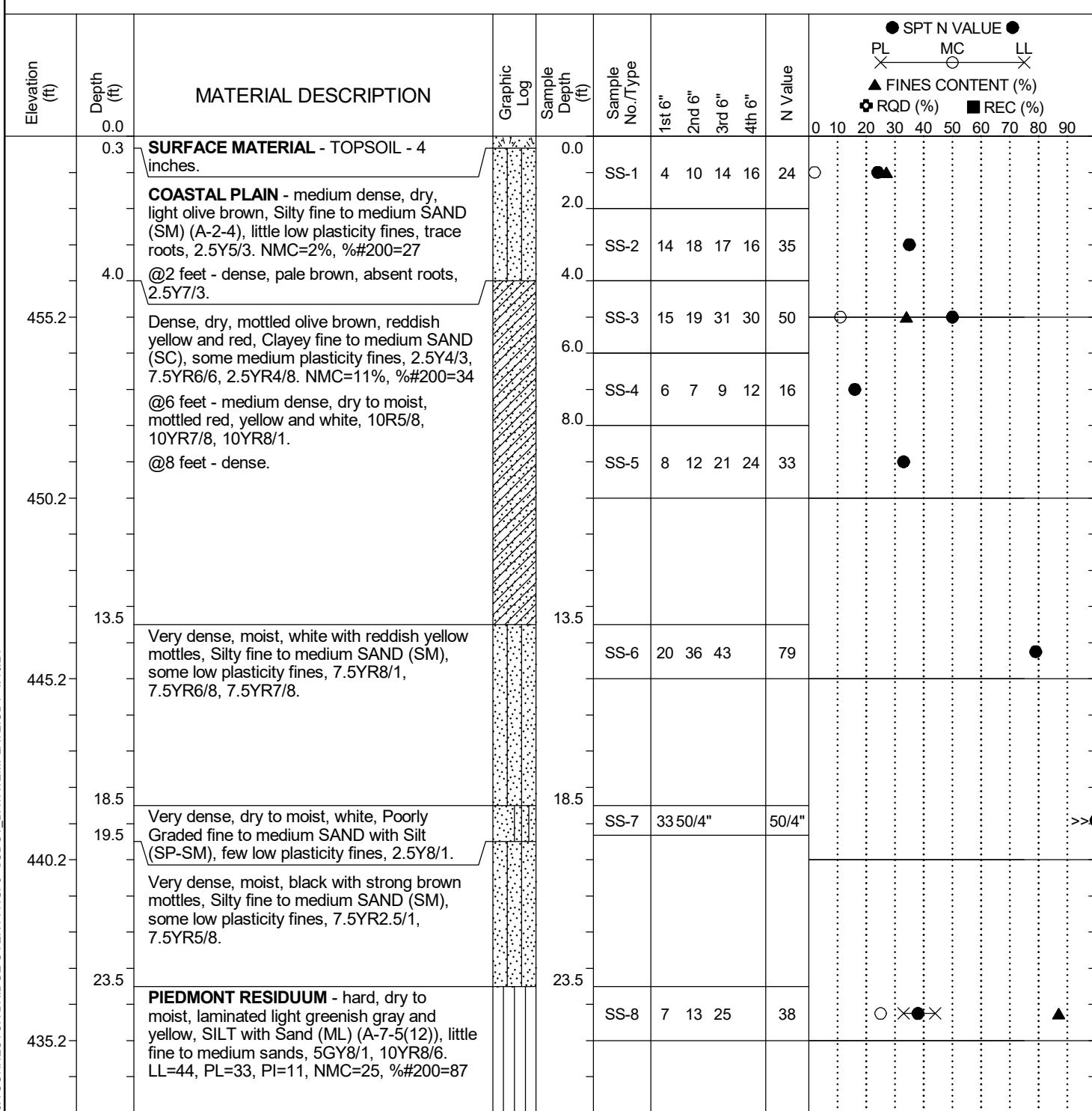
Standard Penetration Resistance - The Number of Blows of 140 lb. Hammer Falling 30 in. Required to Drive 1.4 in. I.D. Split Spoon Sampler 1 Foot. As Specified in ASTM D-1586.

REC - Total Length of Rock Recovered in the Core Barrel Divided by the Total Length of the Core Run Times 100%.

RQD - Total Length of Sound Rock Segments Recovered that are Longer Than or Equal to 4" (mechanical breaks excluded) Divided by the Total Length of the Core Run Times 100%.



Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-1C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	146+03.10	Offset:	-41.8	Alignment:	Proposed
Elev.:	460.2 ft		Latitude:	34.191064703	Longitude:	-80.98444034	Date Started:	10/9/2023
Total Depth:	98.7 ft	Soil Depth:	98.7 ft	Core Depth:	N/A ft	Date Completed:	10/10/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	NE

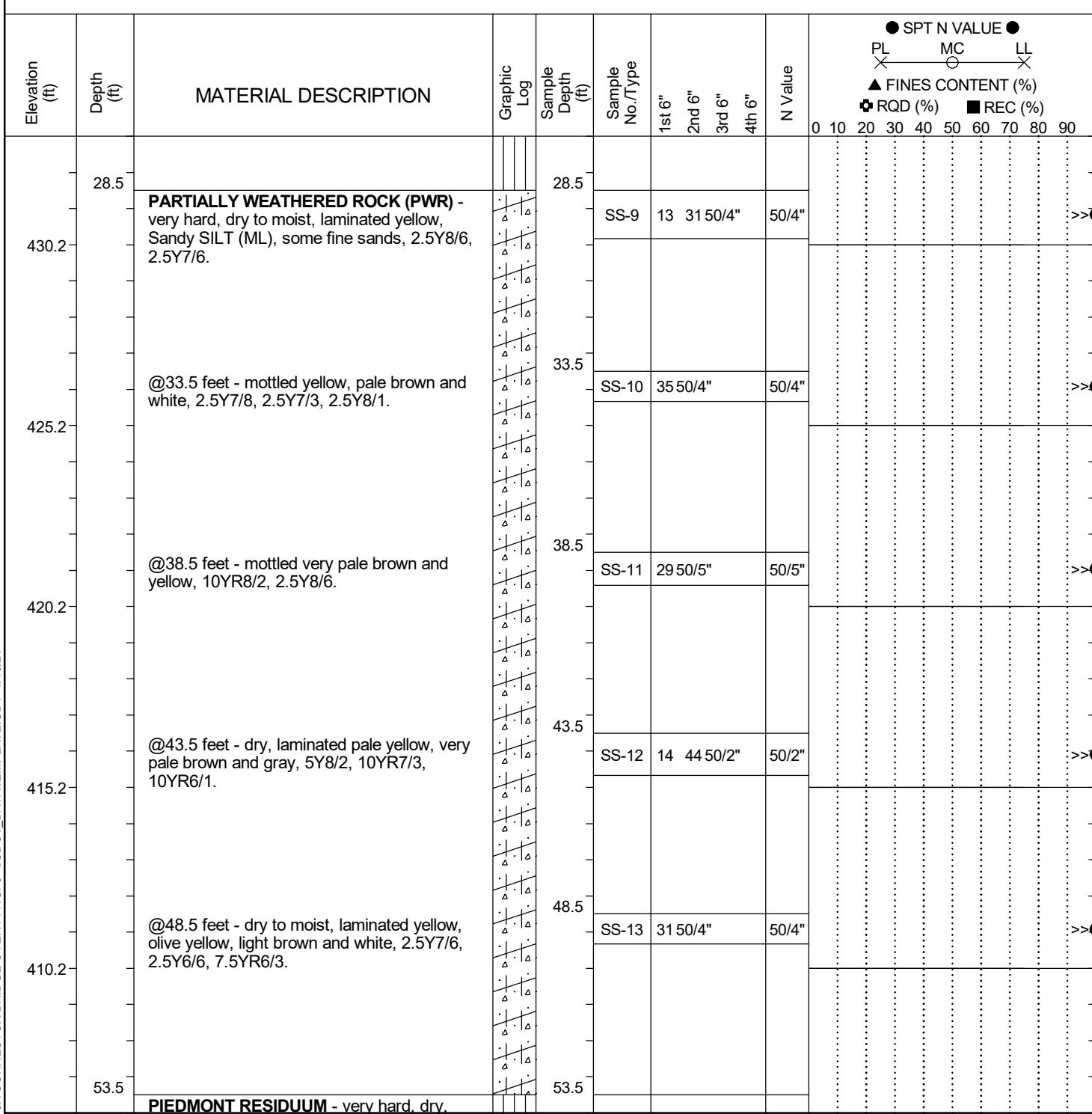


LEGEND

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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash				
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core				
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing					

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-1C		
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd		
Eng./Geo.:	E. Eastabrooks		Boring Location:	146+03.10		Offset:	-41.8	Alignment:	Proposed	
Elev.:	460.2 ft		Latitude:	34.191064703		Longitude:	-80.98444034		Date Started:	10/9/2023
Total Depth:	98.7 ft		Soil Depth:	98.7 ft		Core Depth:	N/A ft		Date Completed:	10/10/2023
Bore Hole Diameter (in):	4		Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y	(N)
Drill Machine:	CME-550X		Drill Method:	RW		Hammer Type:	Automatic		Energy Ratio:	91.6%
Core Size:	N/A		Driller:	L. Shrader		Groundwater:	TOB	N/A	24HR	NE

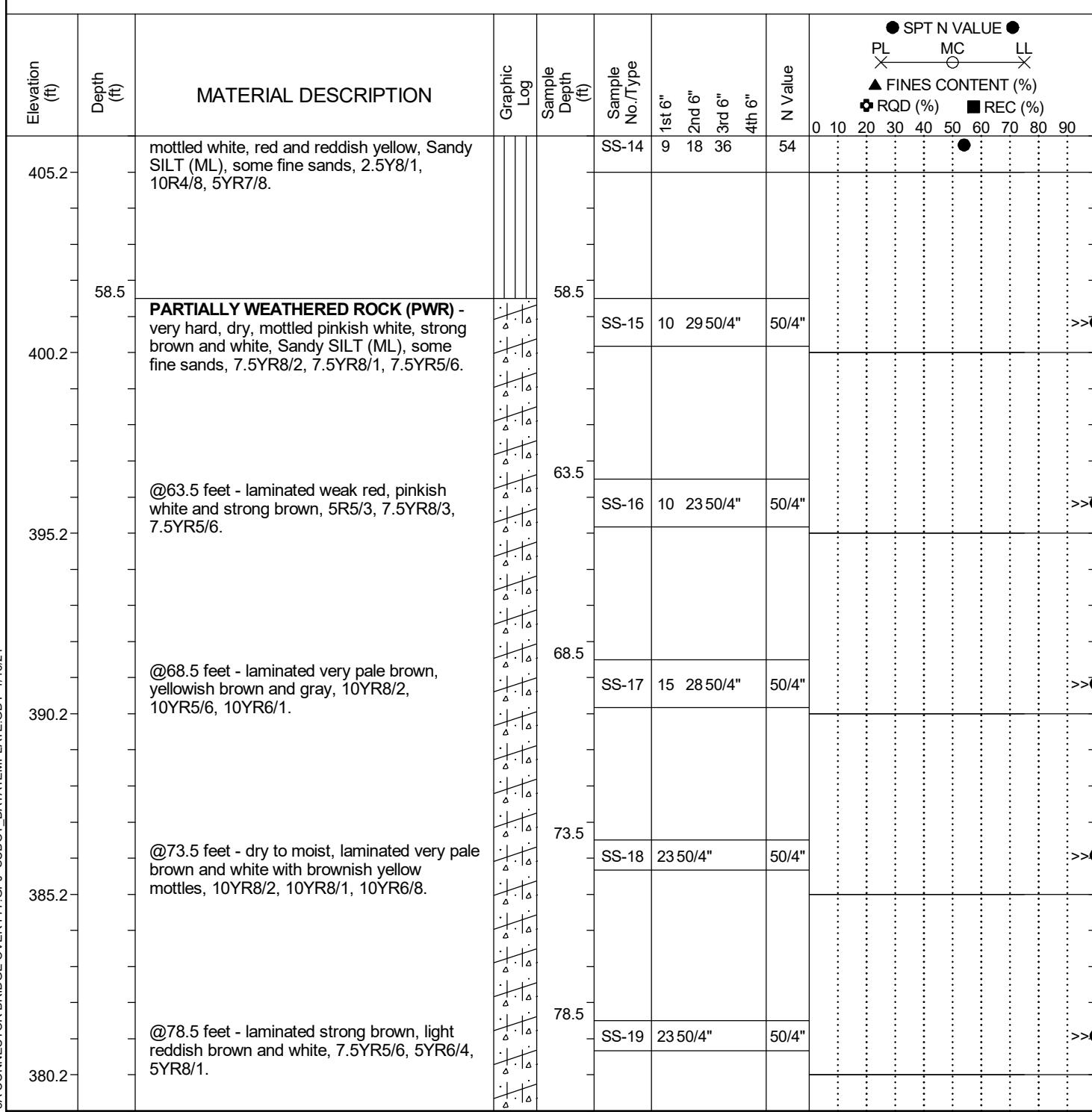


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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-1C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	146+03.10	Offset:	-41.8	Alignment:	Proposed
Elev.:	460.2 ft		Latitude:	34.191064703	Longitude:	-80.98444034	Date Started:	10/9/2023
Total Depth:	98.7 ft	Soil Depth:	98.7 ft	Core Depth:	N/A ft	Date Completed:	10/10/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	NE



LEGEND

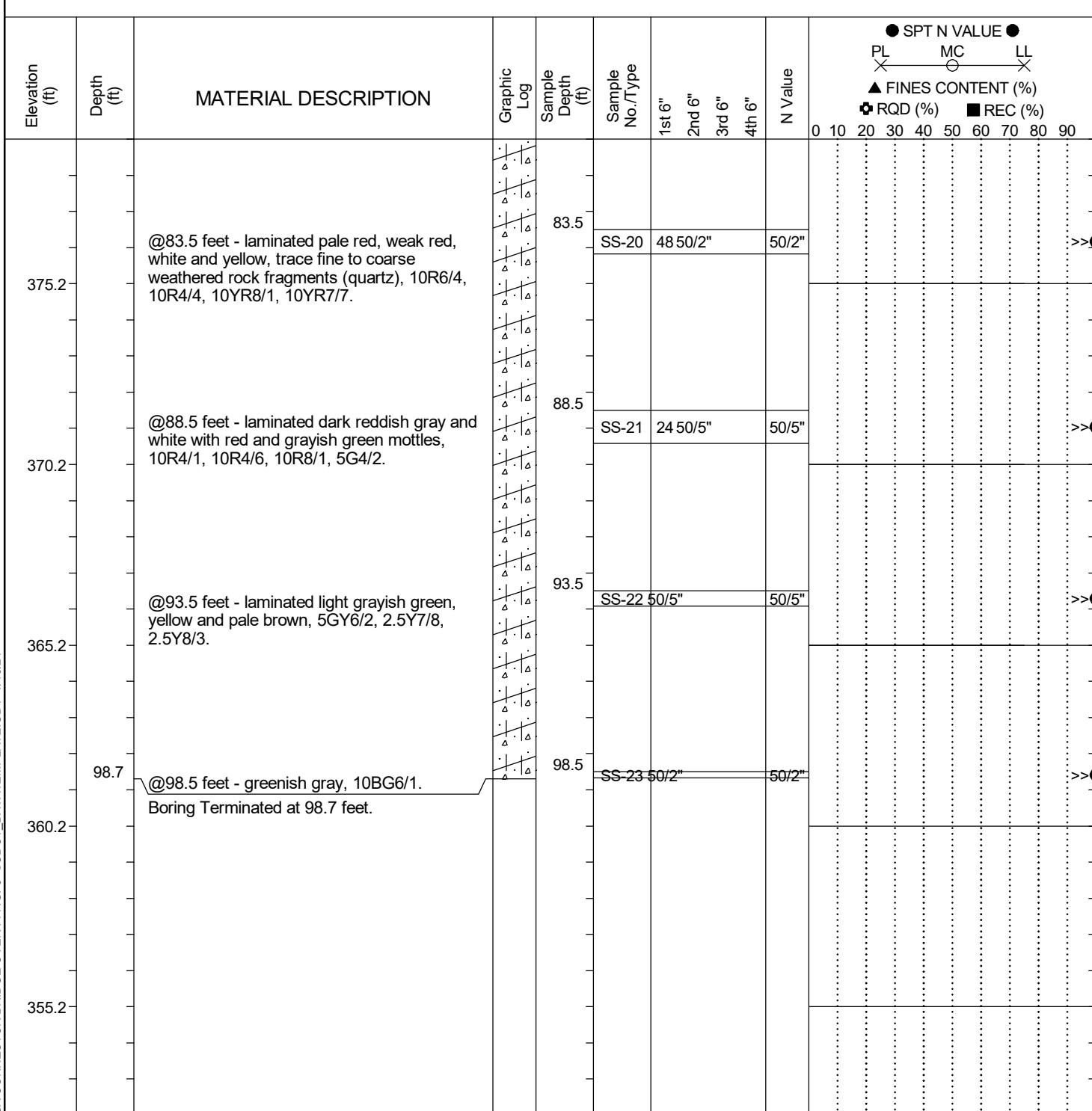
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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	CU - Cuttings	HSA - Hollow Stem Auger	RW - Rotary Wash			
UD - Undisturbed Sample		CT - Continuous Tube	CFA - Continuous Flight Augers	RC - Rock Core			
AWG - Rock Core, 1-1/8"			DC - Driving Casing				



Soil Test Log

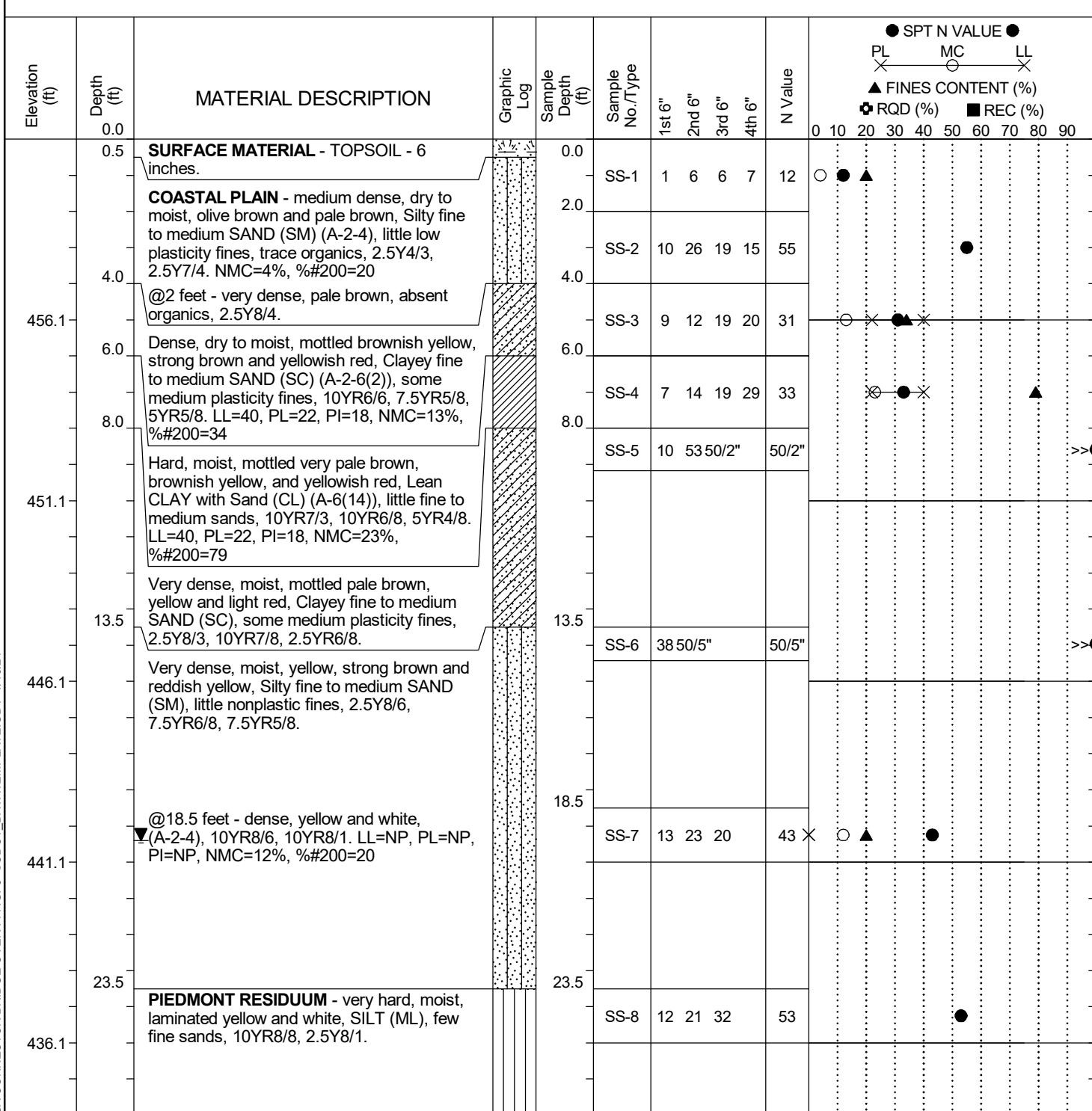
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Site Description:	I-77 Exit 26 Phase I					Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	146+03.10	Offset:	-41.8	Alignment:
Elev.:	460.2 ft	Latitude:	34.191064703	Longitude:	-80.98444034	Date Started:	10/9/2023
Total Depth:	98.7 ft	Soil Depth:	98.7 ft	Core Depth:	N/A ft	Date Completed:	10/10/2023
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-2C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	146+01.12		Offset:	80.3	Alignment:
Elev.:	461.1 ft		Latitude:	34.190743666		Longitude:	-80.984322444	
Total Depth:	99.1 ft		Soil Depth:	99.1 ft		Core Depth:	N/A ft	Date Completed:
Bore Hole Diameter (in):	4		Sampler Configuration		Liner Required:	Y	(N)	Liner Used:
Drill Machine:	CME-550X		Drill Method:	RW		Hammer Type:	Automatic	Energy Ratio:
Core Size:	N/A		Driller:	L. Shrader		Groundwater:	TOB	N/A
							24HR	19.4 ft

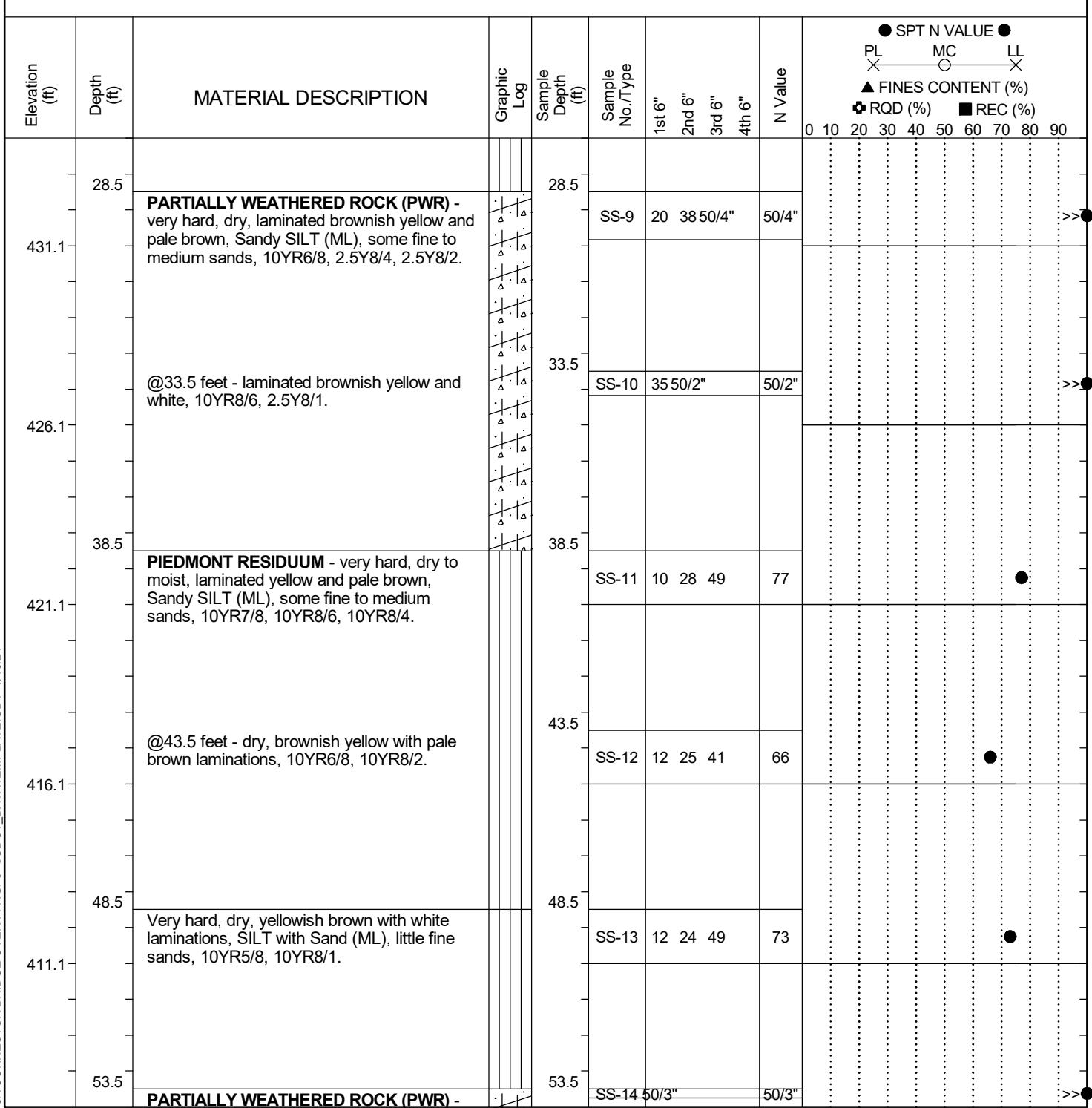


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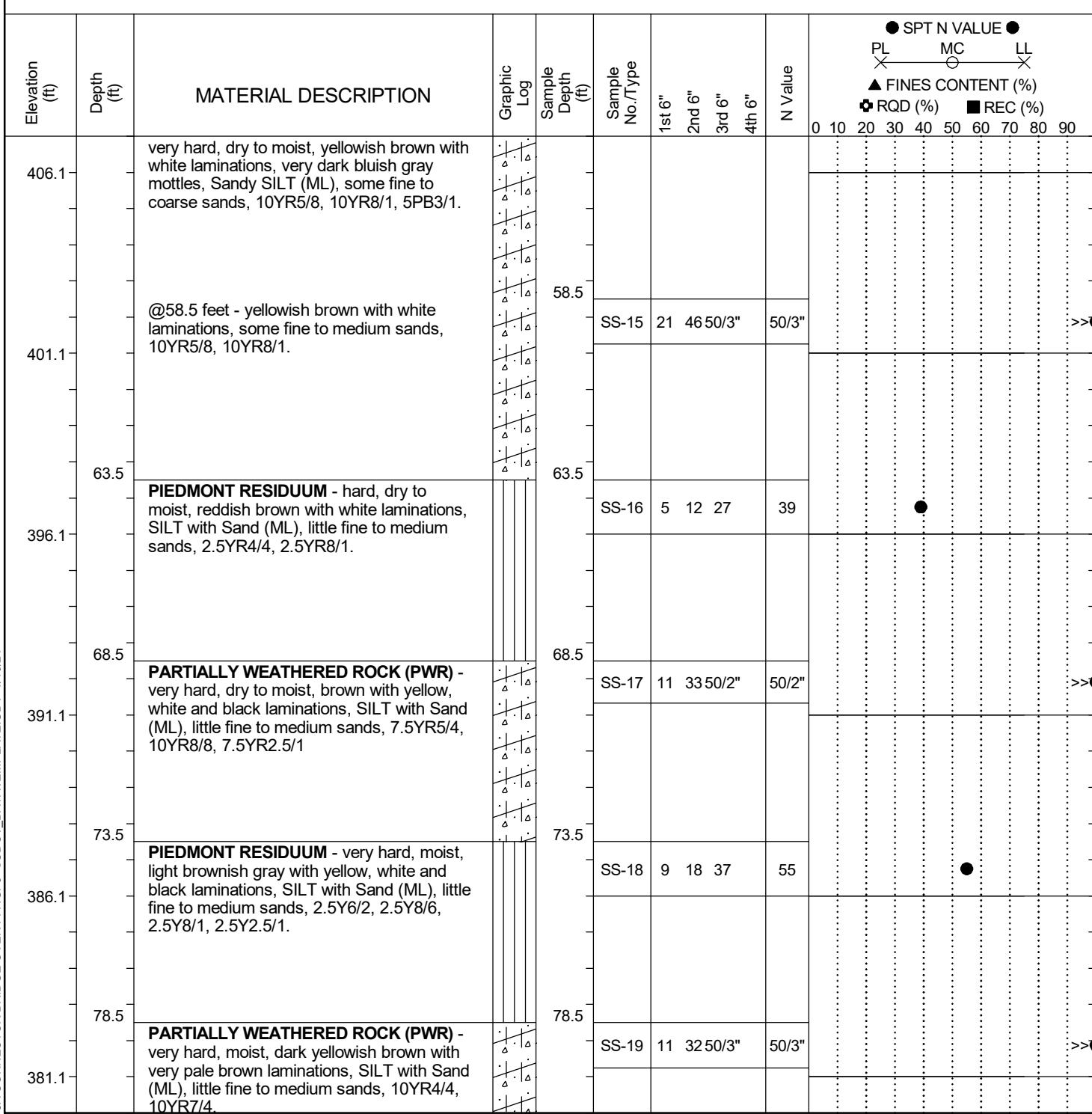
SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-2C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	146+01.12	Offset:	80.3	Alignment:	Proposed
Elev.:	461.1 ft		Latitude:	34.190743666	Longitude:	-80.984322444	Date Started:	9/28/2023
Total Depth:	99.1 ft	Soil Depth:	99.1 ft	Core Depth:	N/A ft	Date Completed:	10/2/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	19.4 ft



SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	UD - Undisturbed Sample	CU - Cuttings	HSA - Hollow Stem Auger	RW - Rotary Wash	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube			DC - Driving Casing			

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-2C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	146+01.12	Offset:	80.3	Alignment:	Proposed
Elev.:	461.1 ft		Latitude:	34.190743666	Longitude:	-80.984322444	Date Started:	9/28/2023
Total Depth:	99.1 ft	Soil Depth:	99.1 ft	Core Depth:	N/A ft	Date Completed:	10/2/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	19.4 ft



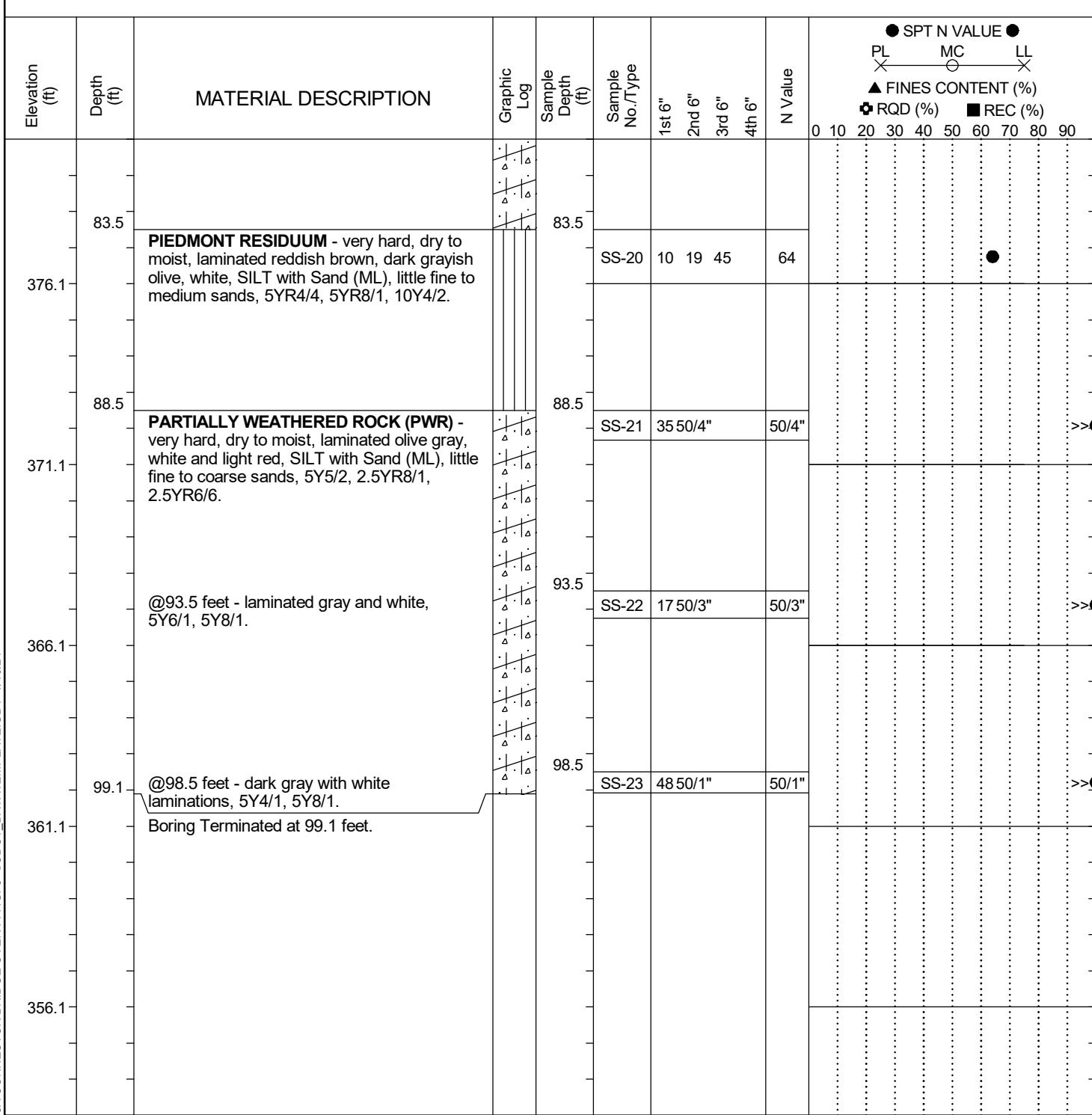
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Soil Test Log

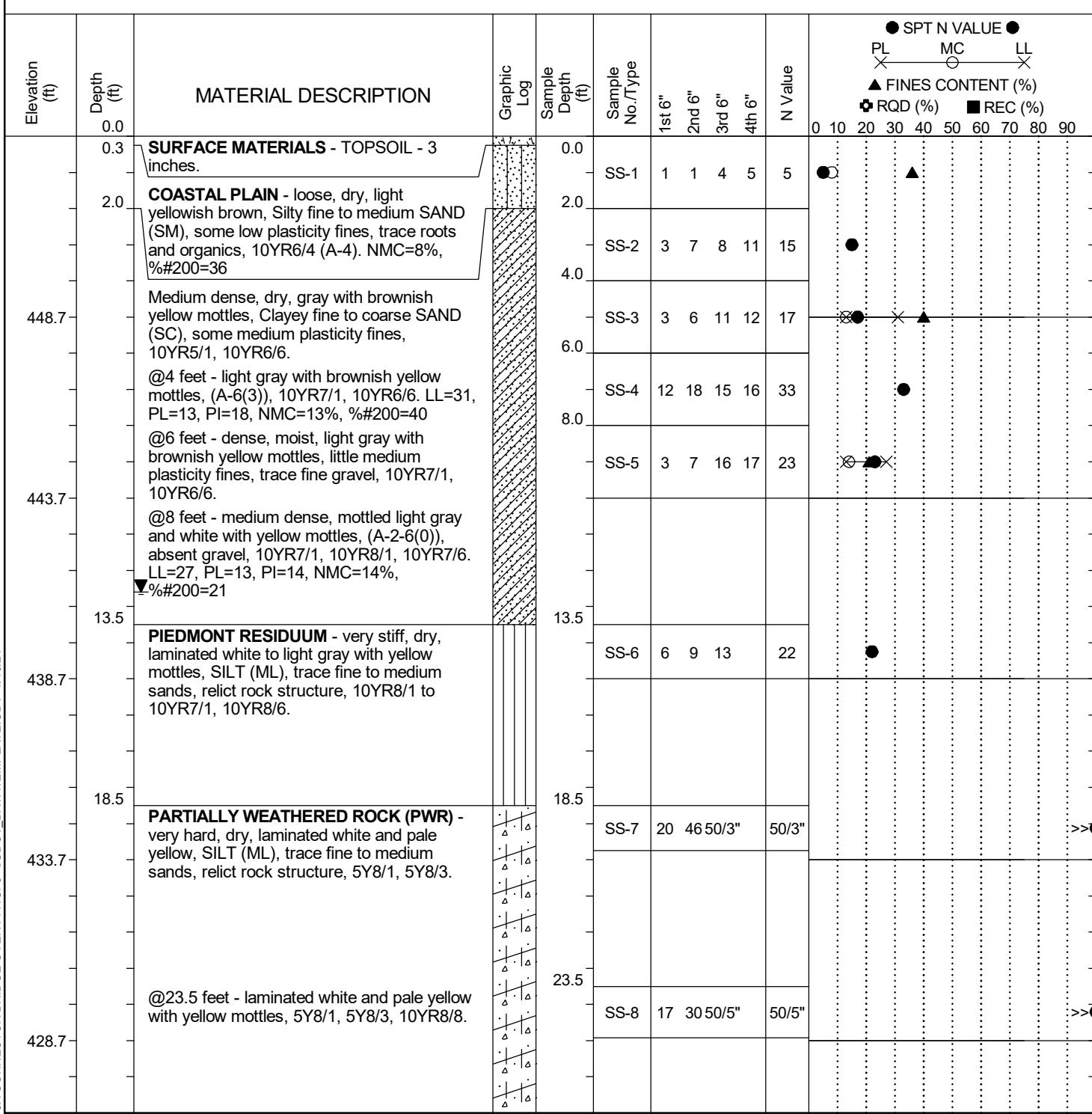
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Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks	Boring Location:	146+01.12	Offset:	80.3	Alignment:	Proposed	
Elev.:	461.1 ft	Latitude:	34.190743666	Longitude:	-80.984322444	Date Started:	9/28/2023	
Total Depth:	99.1 ft	Soil Depth:	99.1 ft	Core Depth:	N/A ft	Date Completed:	10/2/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	19.4 ft



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-3C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+04.68	Offset:	-41.5	Alignment:	Proposed	
Elev.:	453.7 ft	Latitude:	34.191402959	Longitude:	-80.98317639	Date Started:	10/18/2023	
Total Depth:	98.9 ft	Soil Depth:	98.9 ft	Core Depth:	N/A ft	Date Completed:	10/19/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	12.6 ft

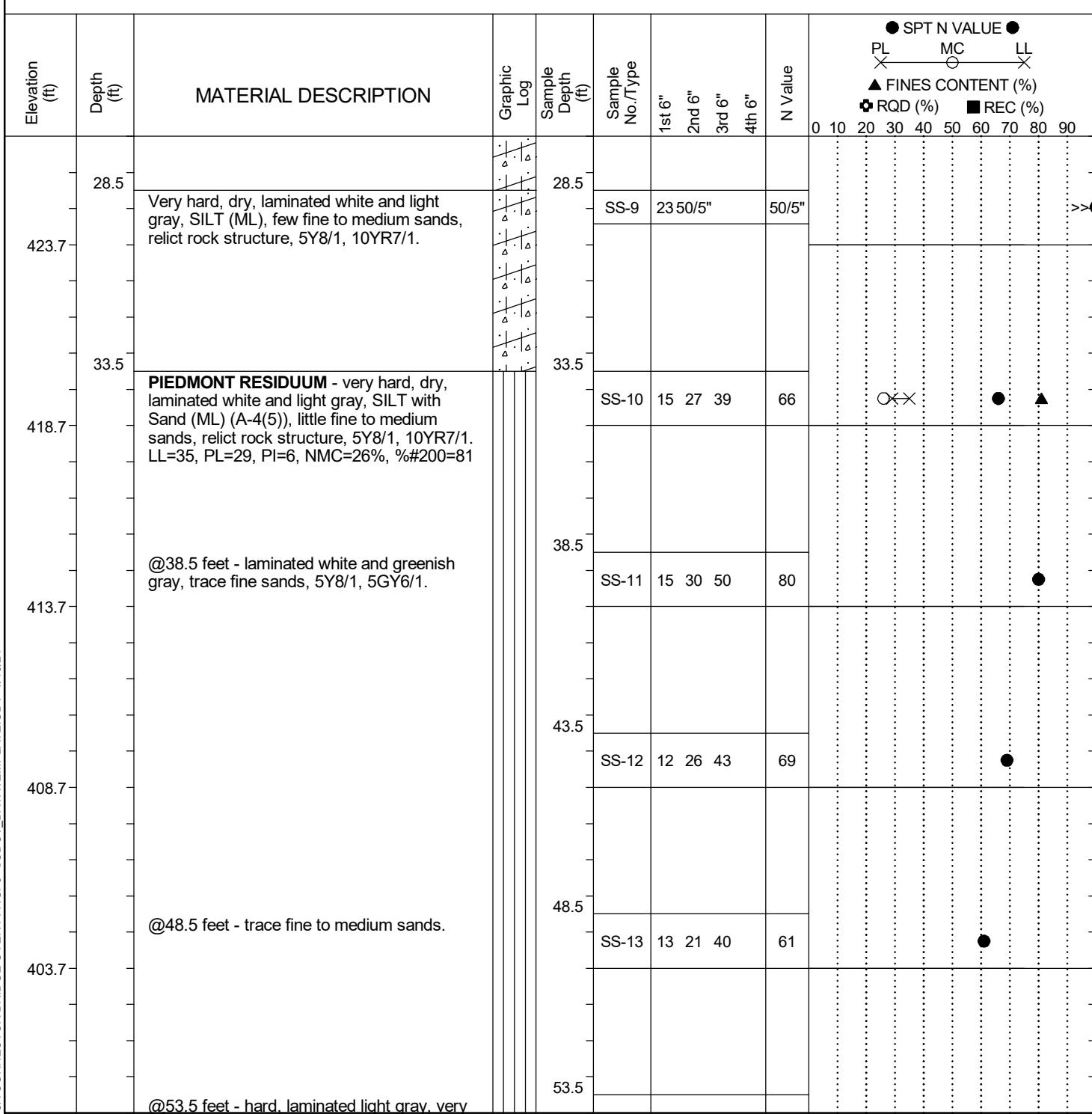


LEGEND

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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash				
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core				
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing					

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-3C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+04.68	Offset:	-41.5	Alignment:	Proposed	
Elev.:	453.7 ft	Latitude:	34.191402959	Longitude:	-80.98317639	Date Started:	10/18/2023	
Total Depth:	98.9 ft	Soil Depth:	98.9 ft	Core Depth:	N/A ft	Date Completed:	10/19/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	12.6 ft

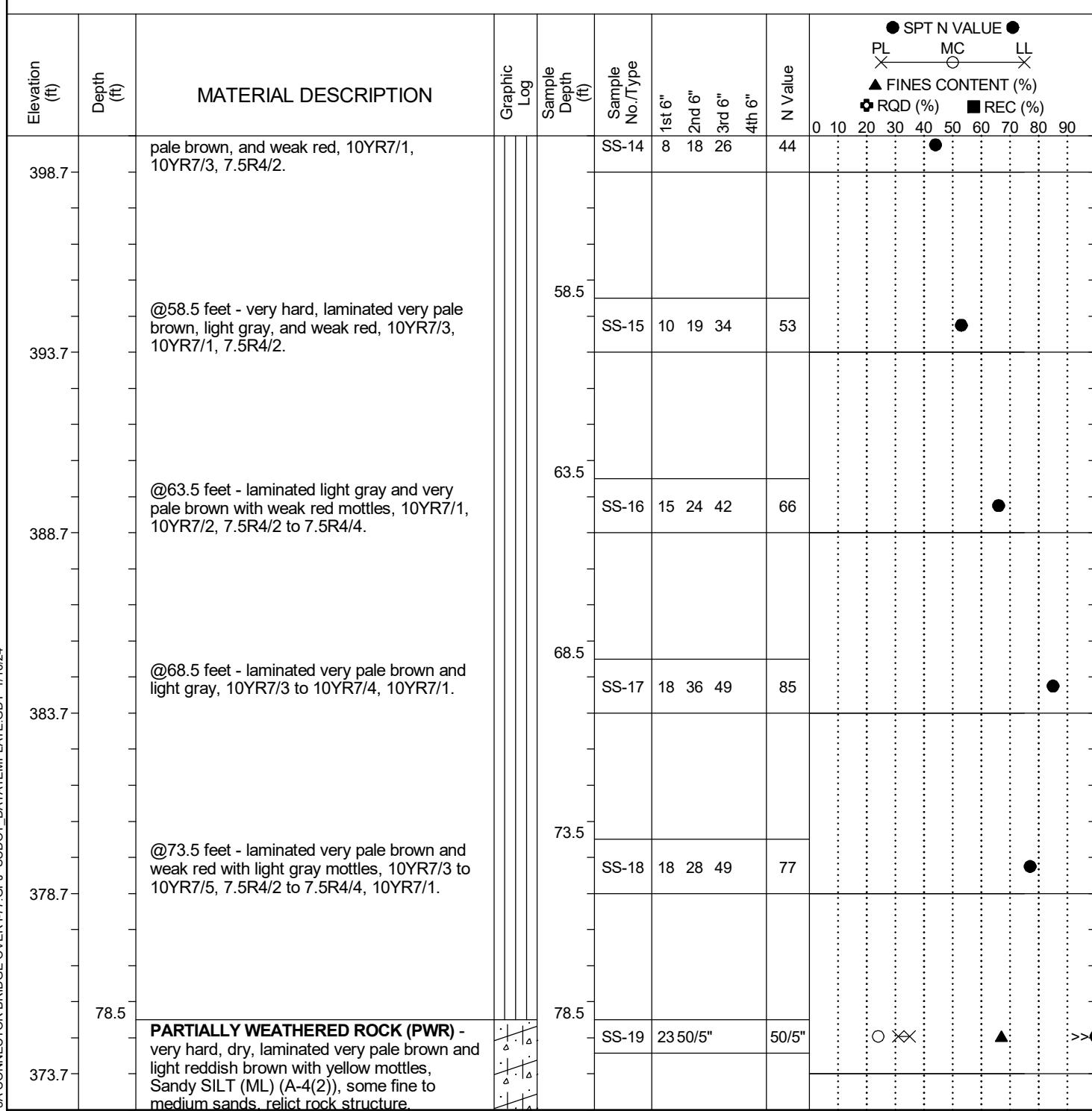


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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-3C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+04.68	Offset:	-41.5	Alignment:	Proposed	
Elev.:	453.7 ft	Latitude:	34.191402959	Longitude:	-80.98317639	Date Started:	10/18/2023	
Total Depth:	98.9 ft	Soil Depth:	98.9 ft	Core Depth:	N/A ft	Date Completed:	10/19/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	12.6 ft

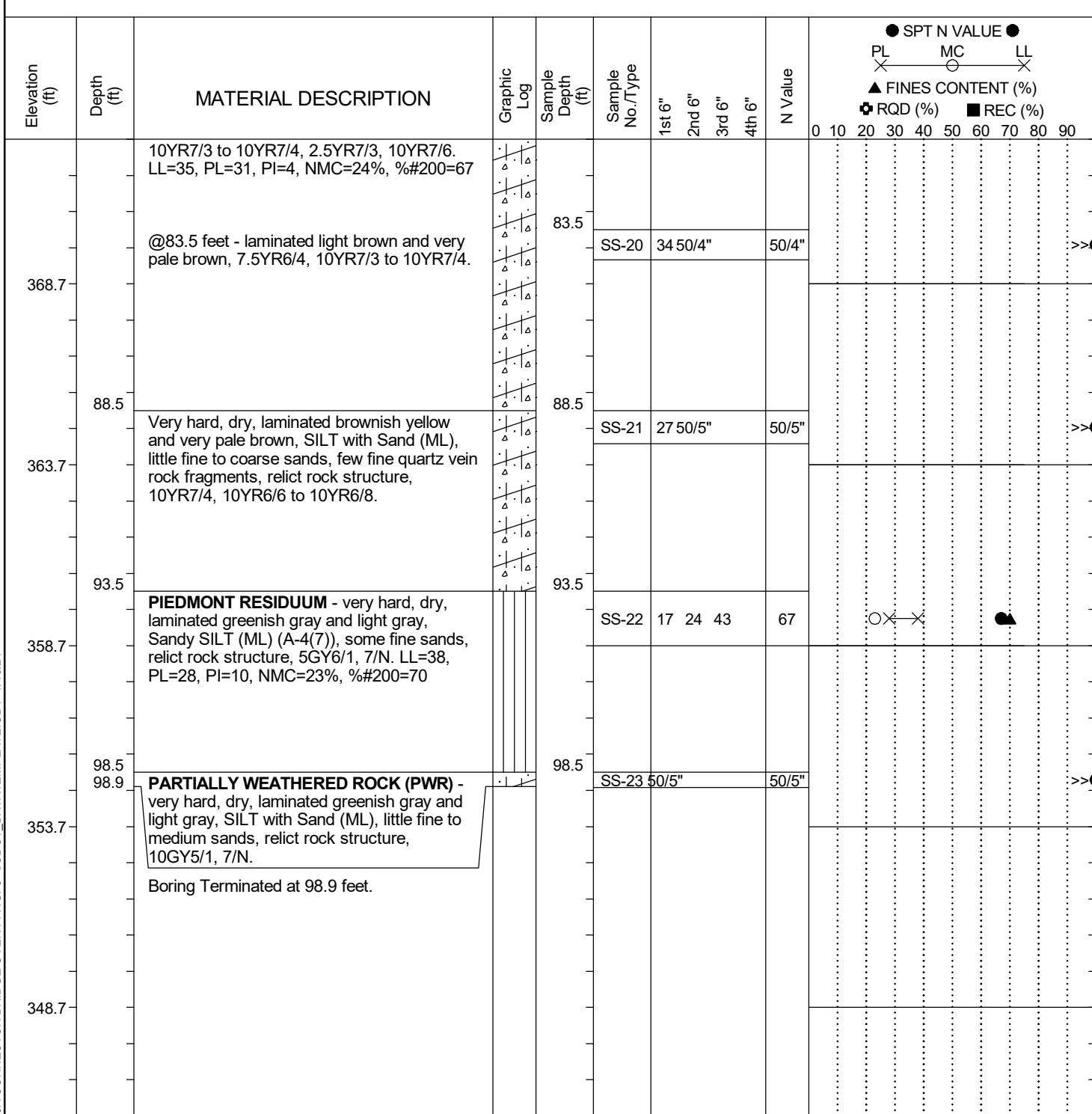


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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

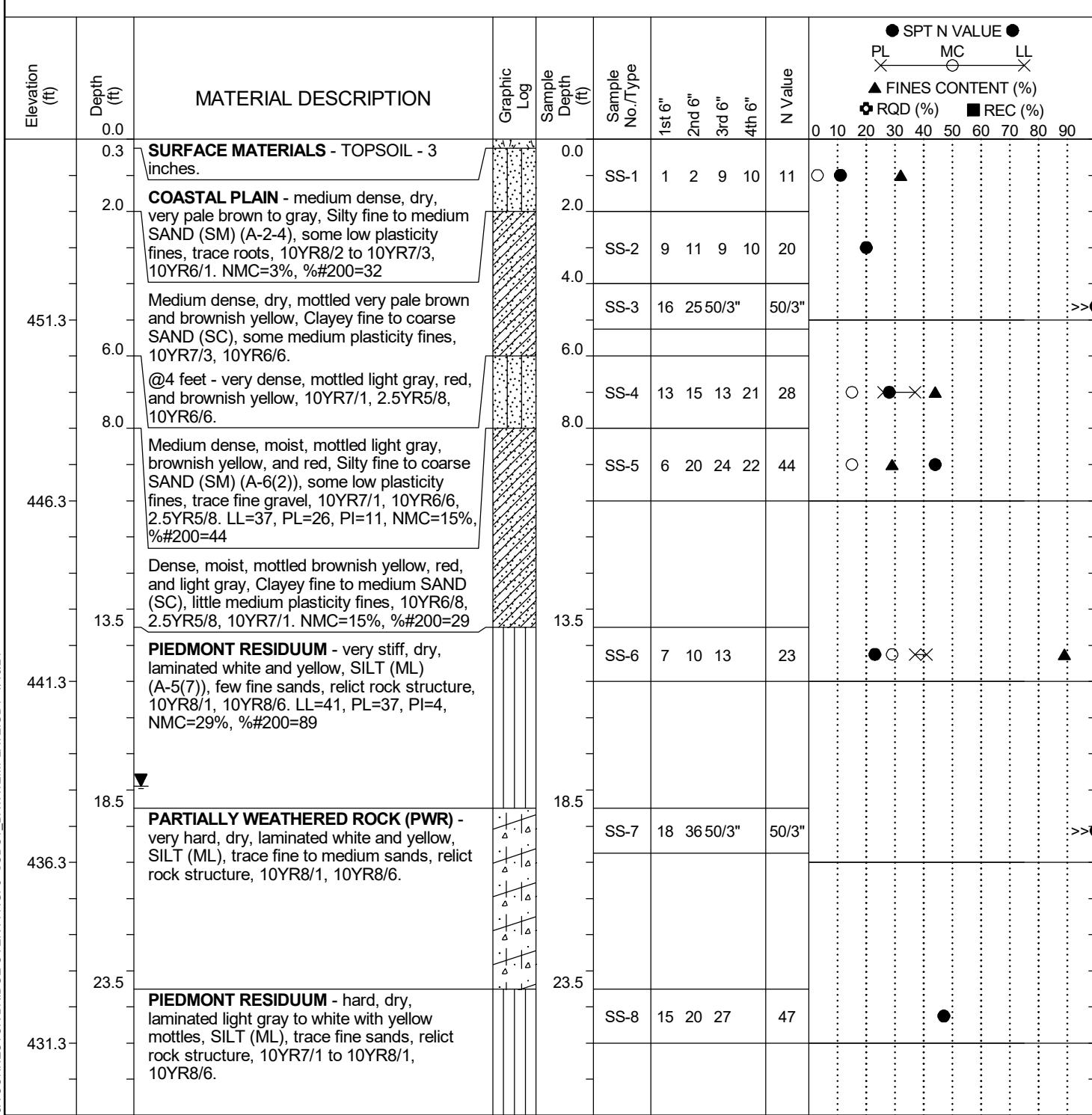
Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-3C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+04.68	Offset:	-41.5	Alignment:	Proposed	
Elev.:	453.7 ft	Latitude:	34.191402959	Longitude:	-80.98317639	Date Started:	10/18/2023	
Total Depth:	98.9 ft	Soil Depth:	98.9 ft	Core Depth:	N/A ft	Date Completed:	10/19/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	12.6 ft



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-4C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+06.47	Offset:	43.9	Alignment:	Proposed	
Elev.:	456.3 ft	Latitude:	34.191181179	Longitude:	-80.98308396	Date Started:	10/23/2023	
Total Depth:	99.2 ft	Soil Depth:	99.2 ft	Core Depth:	N/A ft	Date Completed:	10/24/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	17.9 ft

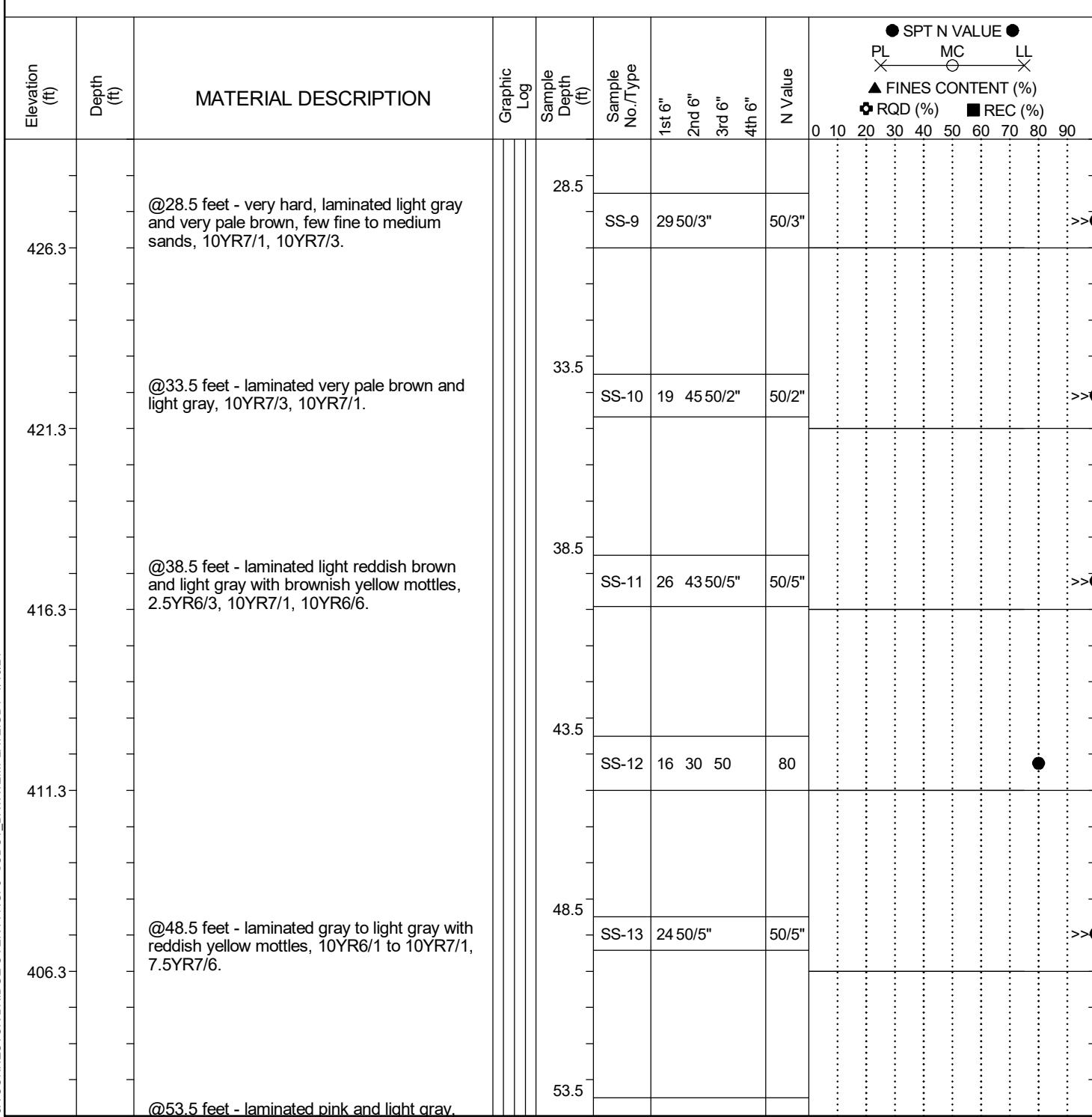


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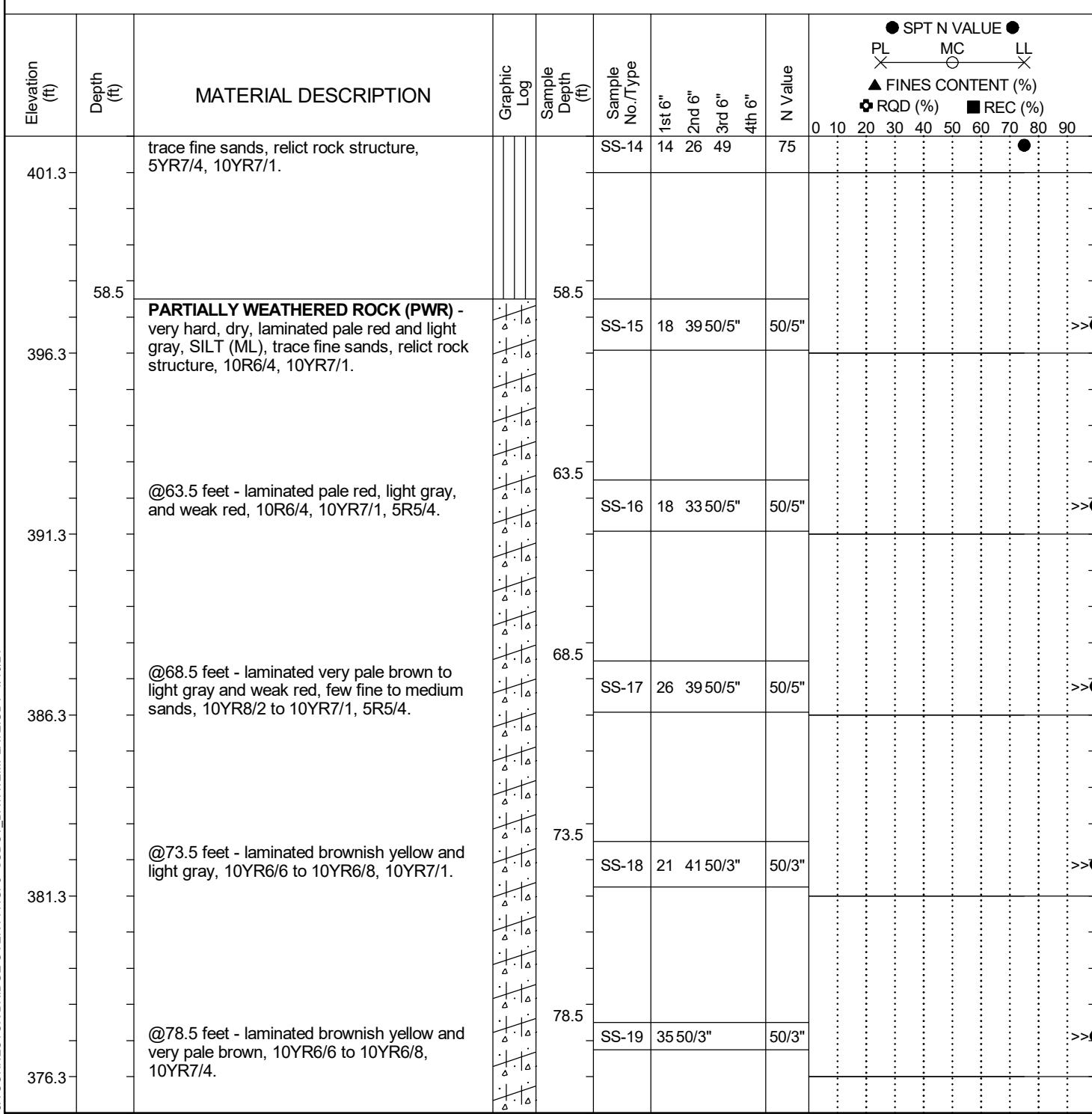
SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-4C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+06.47	Offset:	43.9	Alignment:	Proposed	
Elev.:	456.3 ft	Latitude:	34.191181179	Longitude:	-80.98308396	Date Started:	10/23/2023	
Total Depth:	99.2 ft	Soil Depth:	99.2 ft	Core Depth:	N/A ft	Date Completed:	10/24/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	17.9 ft



SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-4C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+06.47	Offset:	43.9	Alignment:	Proposed	
Elev.:	456.3 ft	Latitude:	34.191181179	Longitude:	-80.98308396	Date Started:	10/23/2023	
Total Depth:	99.2 ft	Soil Depth:	99.2 ft	Core Depth:	N/A ft	Date Completed:	10/24/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	17.9 ft

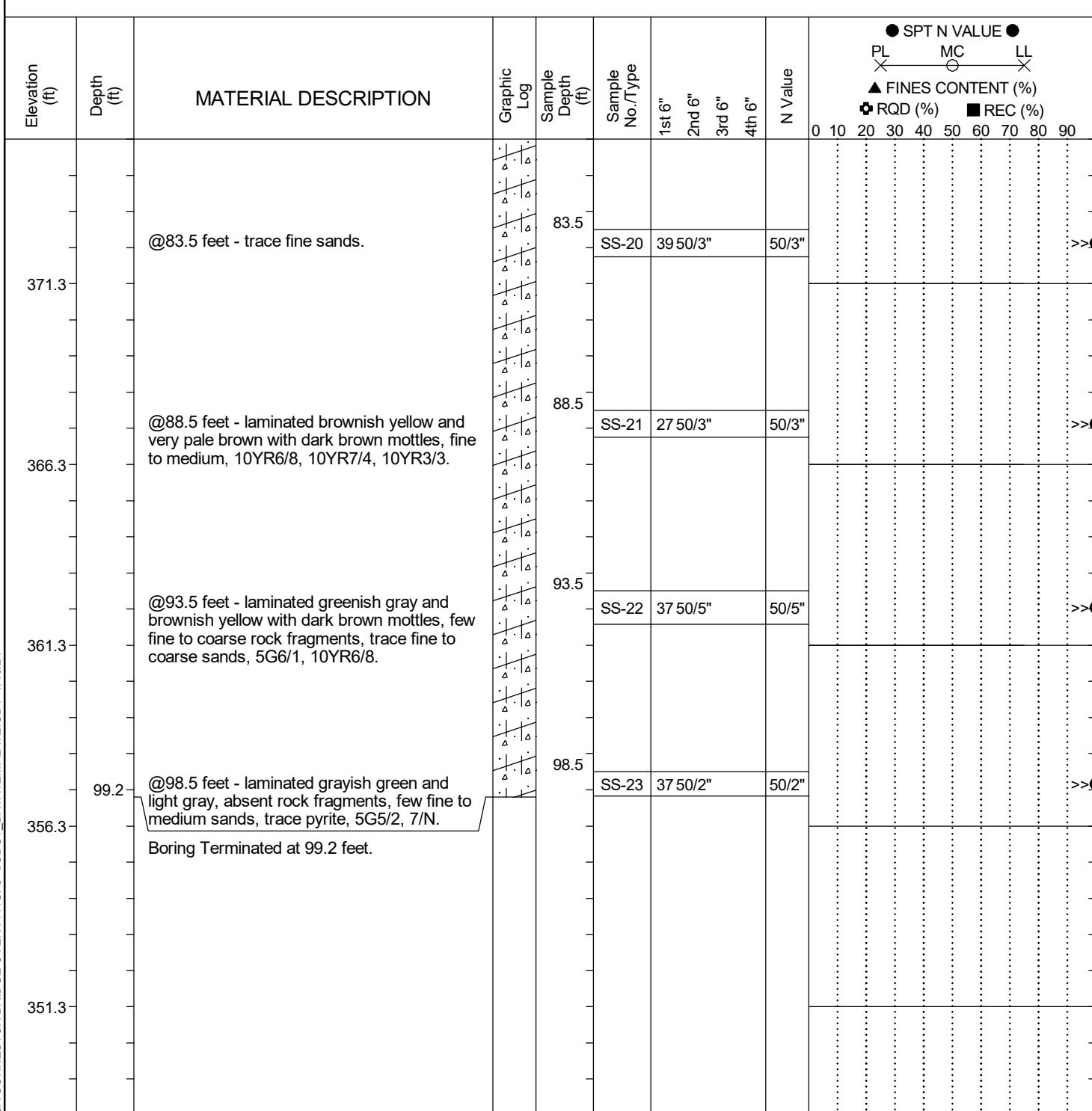


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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

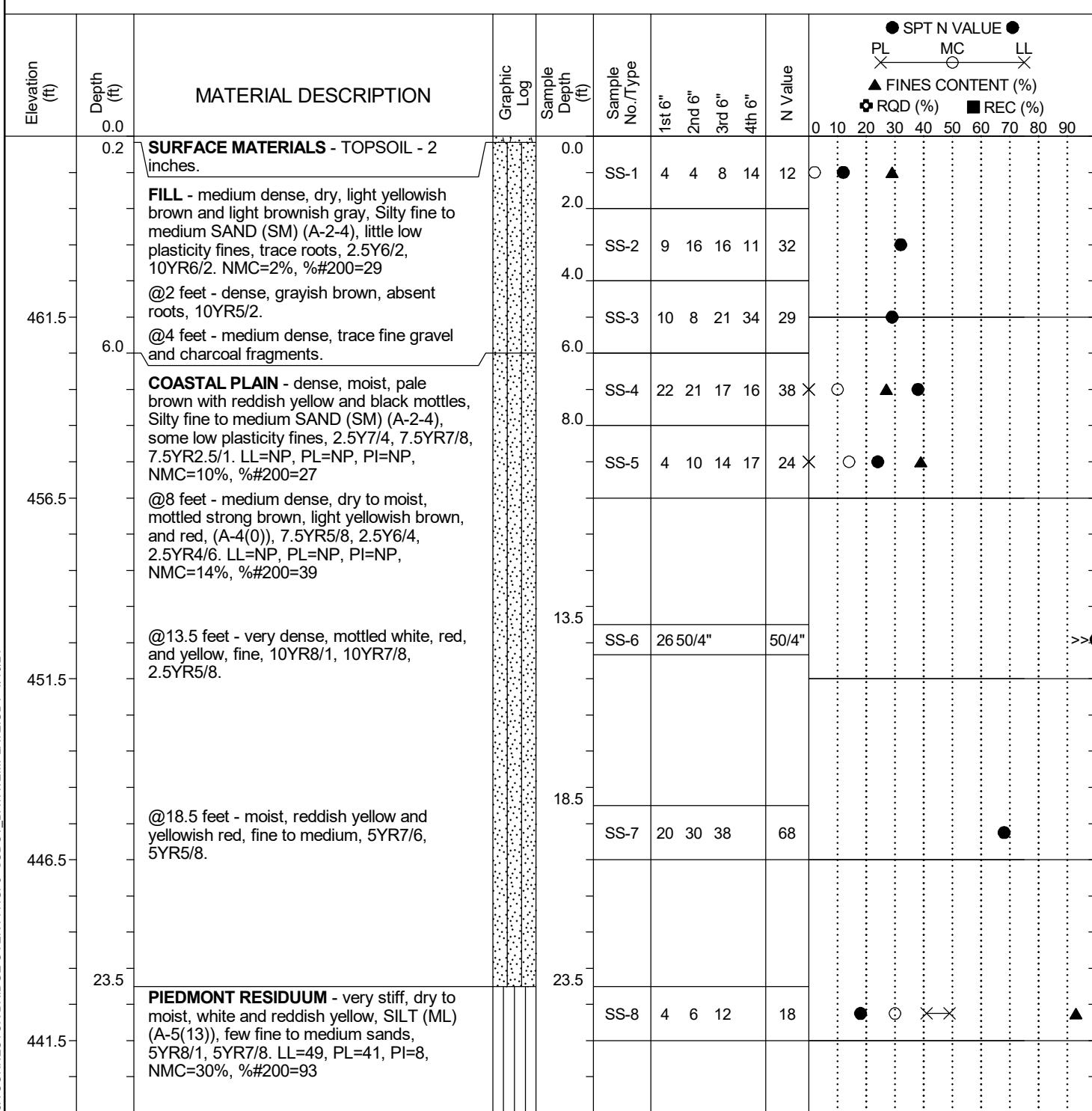
Project ID:	P042443 (S&ME 23610178A)		County:	Richland		Boring No.:	EB-4C
Site Description:	I-77 Exit 26 Phase I					Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+06.47	Offset:	43.9	Alignment:	Proposed
Elev.:	456.3 ft	Latitude:	34.191181179	Longitude:	-80.98308396	Date Started:	10/23/2023
Total Depth:	99.2 ft	Soil Depth:	99.2 ft	Core Depth:	N/A ft	Date Completed:	10/24/2023
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR



LEGEND

SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-5C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+23.93	Offset:	149.9	Alignment:	Proposed
Elev.:	466.5 ft		Latitude:	34.190665368	Longitude:	-80.98386528	Date Started:	10/25/2023
Total Depth:	98.8 ft	Soil Depth:	98.8 ft	Core Depth:	N/A ft	Date Completed:	10/26/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:		
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	30.2 ft

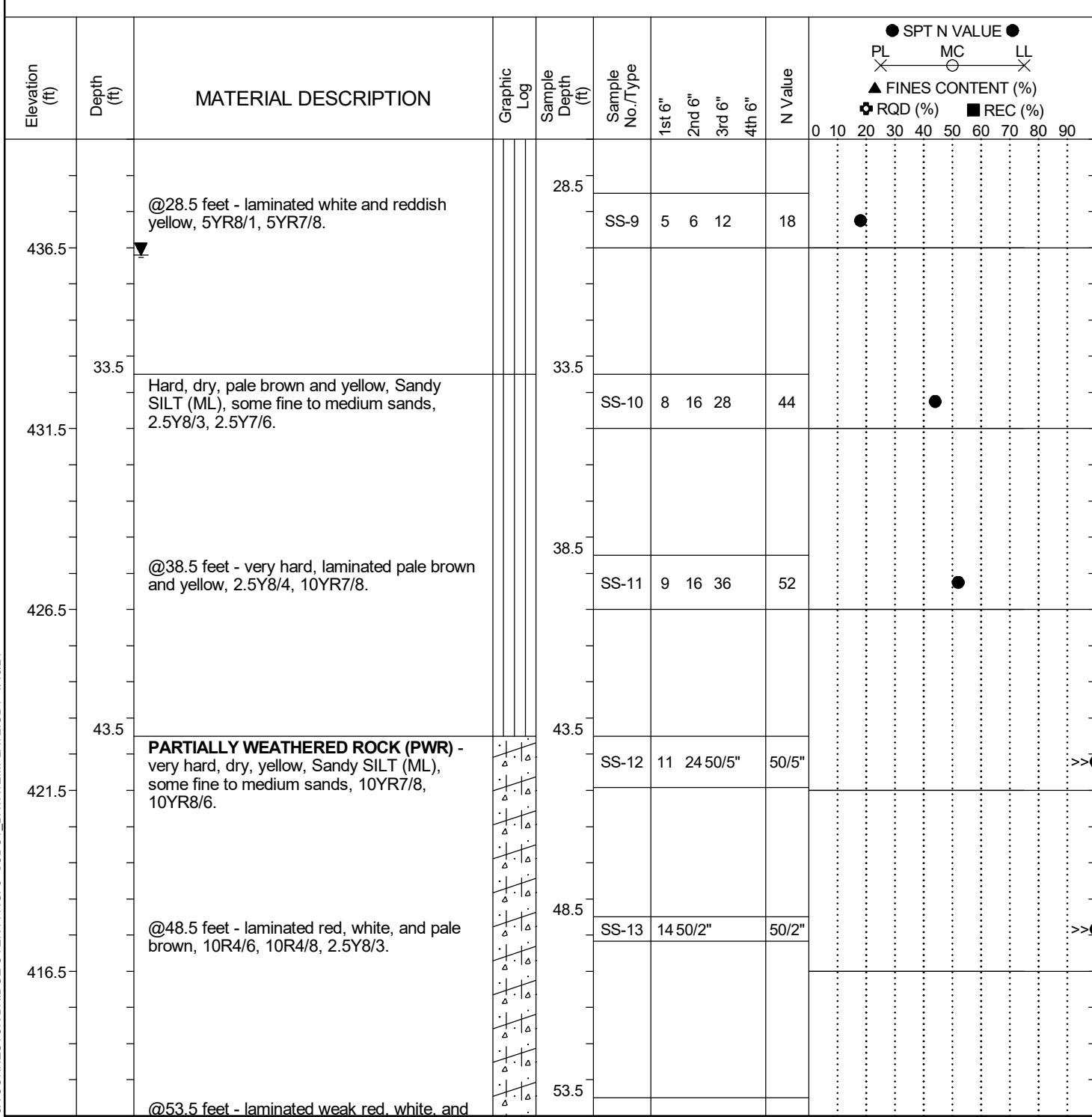


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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	CU - Cuttings	HSA - Hollow Stem Auger	RW - Rotary Wash			
UD - Undisturbed Sample		CT - Continuous Tube	CFA - Continuous Flight Augers	RC - Rock Core			
AWG - Rock Core, 1-1/8"			DC - Driving Casing				

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-5C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+23.93	Offset:	149.9	Alignment:	Proposed
Elev.:	466.5 ft		Latitude:	34.190665368	Longitude:	-80.98386528	Date Started:	10/25/2023
Total Depth:	98.8 ft	Soil Depth:	98.8 ft	Core Depth:	N/A ft	Date Completed:	10/26/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:		
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	30.2 ft

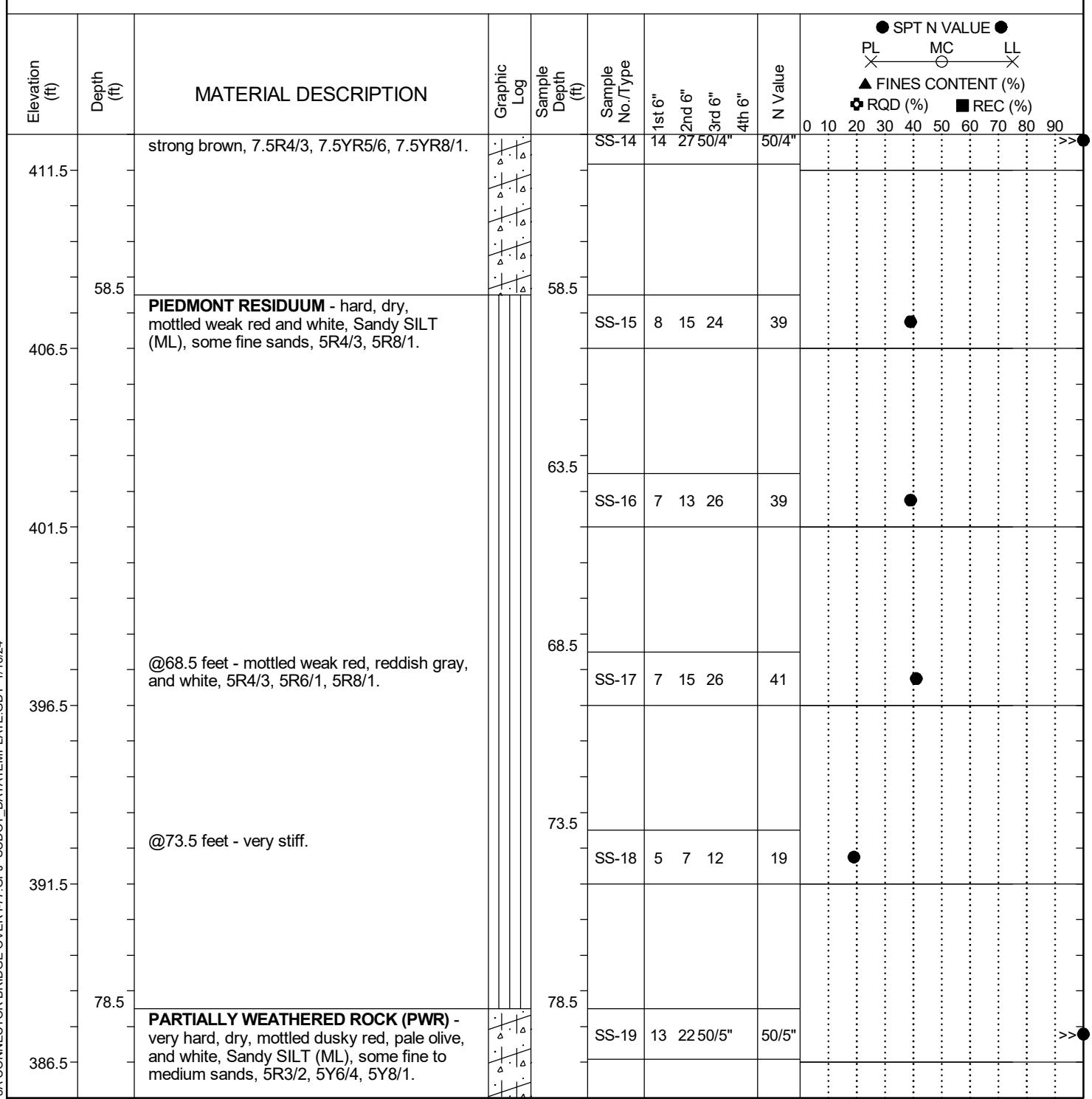


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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash				
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core				
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing					

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-5C		
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd		
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+23.93		Offset:	149.9	Alignment:	Proposed	
Elev.:	466.5 ft		Latitude:	34.190665368		Longitude:	-80.98386528		Date Started:	10/25/2023
Total Depth:	98.8 ft		Soil Depth:	98.8 ft		Core Depth:	N/A ft	Date Completed:	10/26/2023	
Bore Hole Diameter (in):	4		Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y	(N)
Drill Machine:	CME-550X		Drill Method:	RW		Hammer Type:	Automatic		Energy Ratio:	91.6%
Core Size:	N/A		Driller:	L. Shrader		Groundwater:	TOB	N/A	24HR	30.2 ft

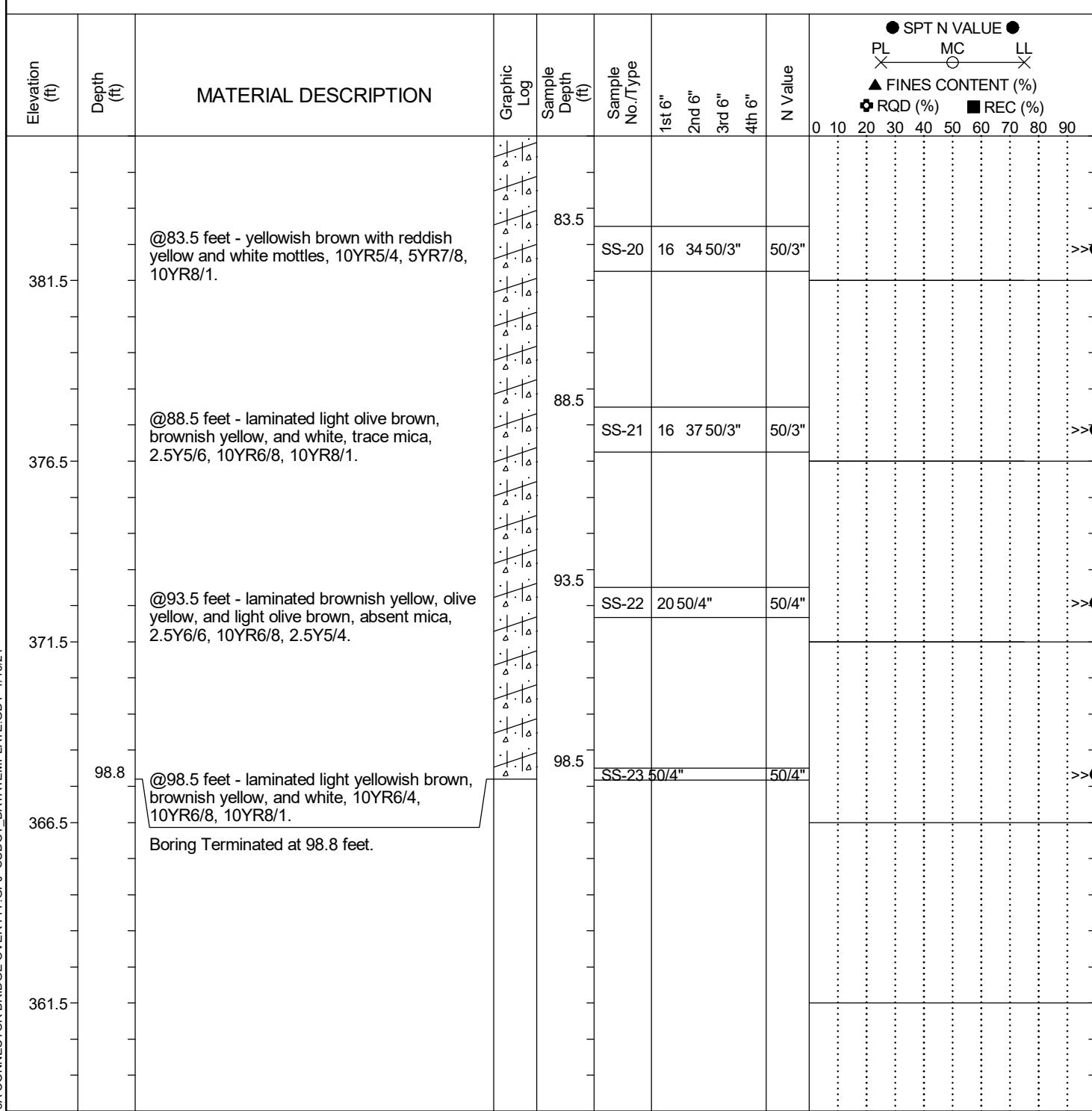


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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash				
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core				
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing					

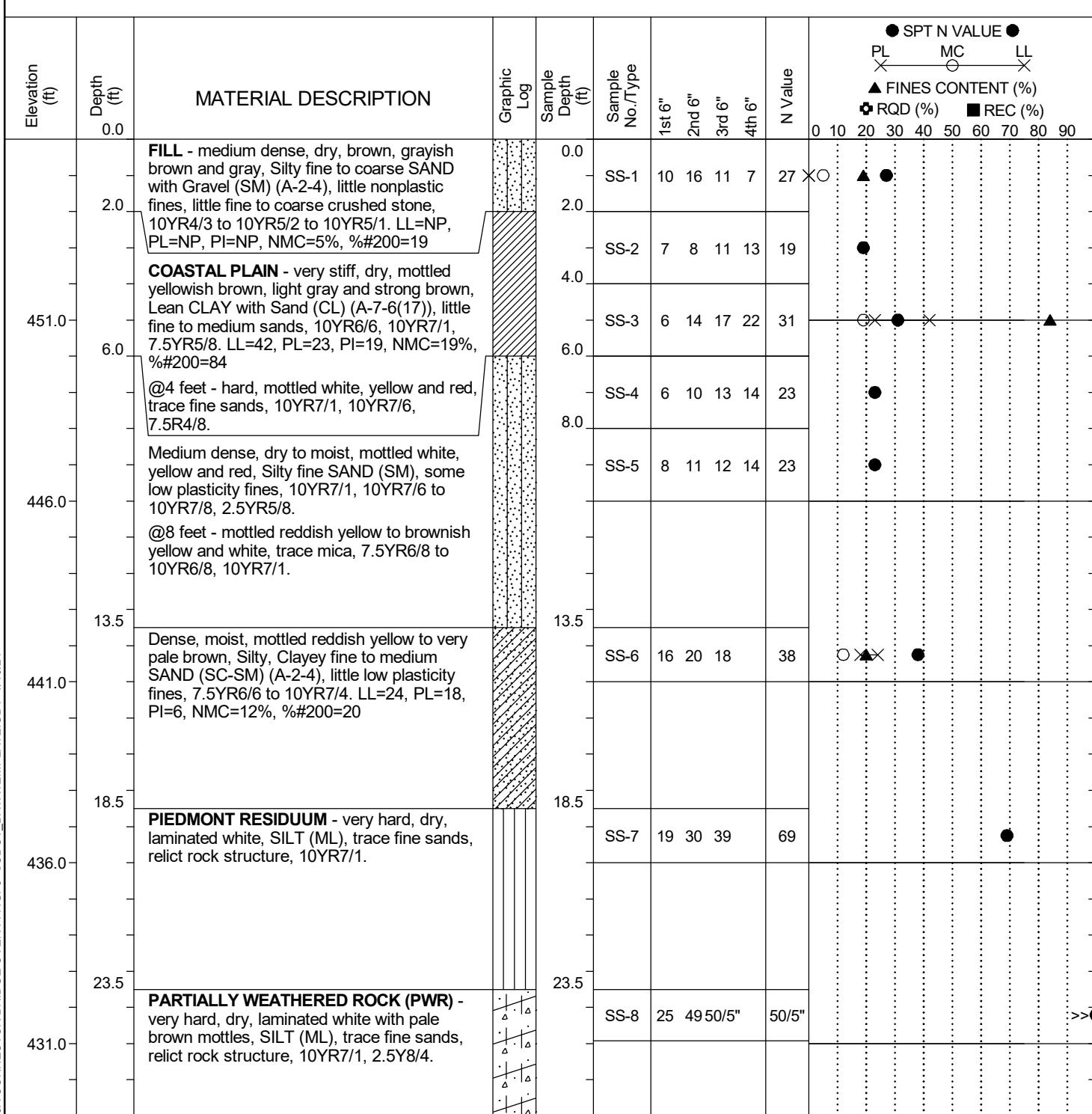
Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-5C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+23.93	Offset:	149.9	Alignment:	Proposed
Elev.:	466.5 ft		Latitude:	34.190665368	Longitude:	-80.98386528	Date Started:	10/25/2023
Total Depth:	98.8 ft	Soil Depth:	98.8 ft	Core Depth:	N/A ft	Date Completed:	10/26/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic		Energy Ratio:	91.6%
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	30.2 ft



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-6C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+67.20	Offset:	148.4	Alignment:	Proposed	
Elev.:	456.0 ft	Latitude:	34.190705874	Longitude:	-80.98373065	Date Started:	11/9/2023	
Total Depth:	98.9 ft	Soil Depth:	98.9 ft	Core Depth:	N/A ft	Date Completed:	11/9/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	NE

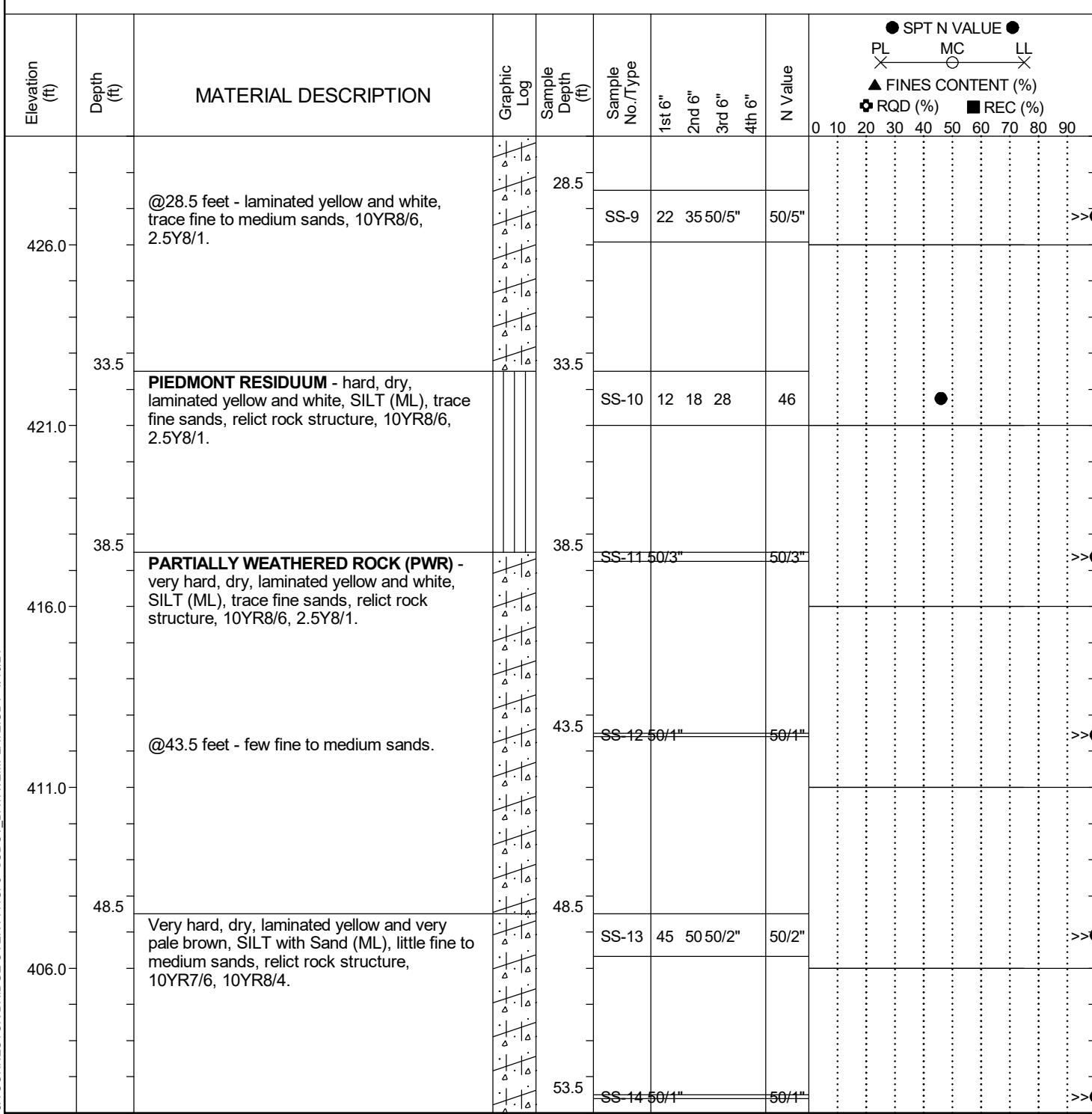


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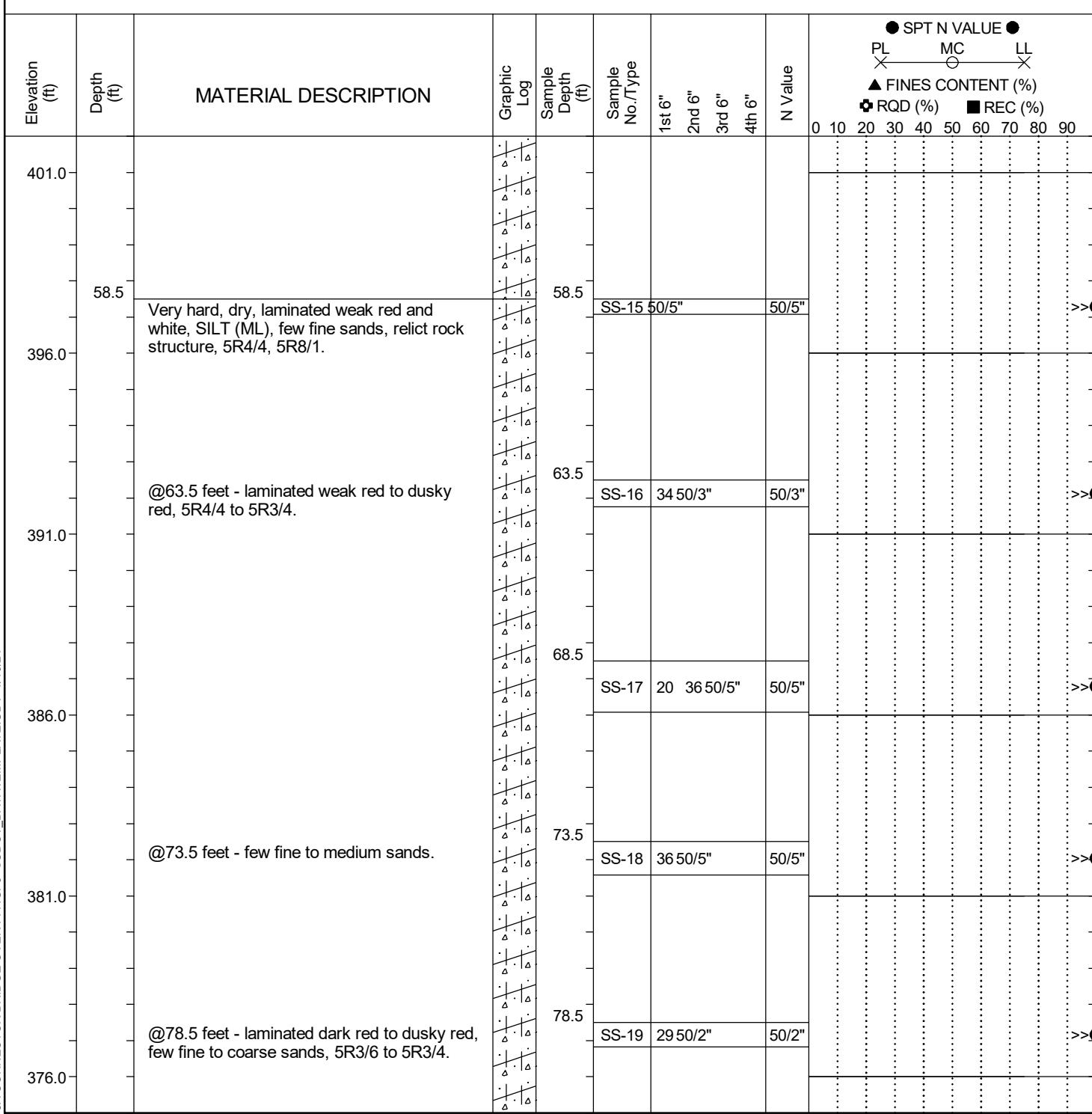
SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-6C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+67.20	Offset:	148.4	Alignment:	Proposed	
Elev.:	456.0 ft	Latitude:	34.190705874	Longitude:	-80.98373065	Date Started:	11/9/2023	
Total Depth:	98.9 ft	Soil Depth:	98.9 ft	Core Depth:	N/A ft	Date Completed:	11/9/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	NE



SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash				
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core				
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing					

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EB-6C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+67.20	Offset:	148.4	Alignment:	Proposed	
Elev.:	456.0 ft	Latitude:	34.190705874	Longitude:	-80.98373065	Date Started:	11/9/2023	
Total Depth:	98.9 ft	Soil Depth:	98.9 ft	Core Depth:	N/A ft	Date Completed:	11/9/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	NE



LEGEND

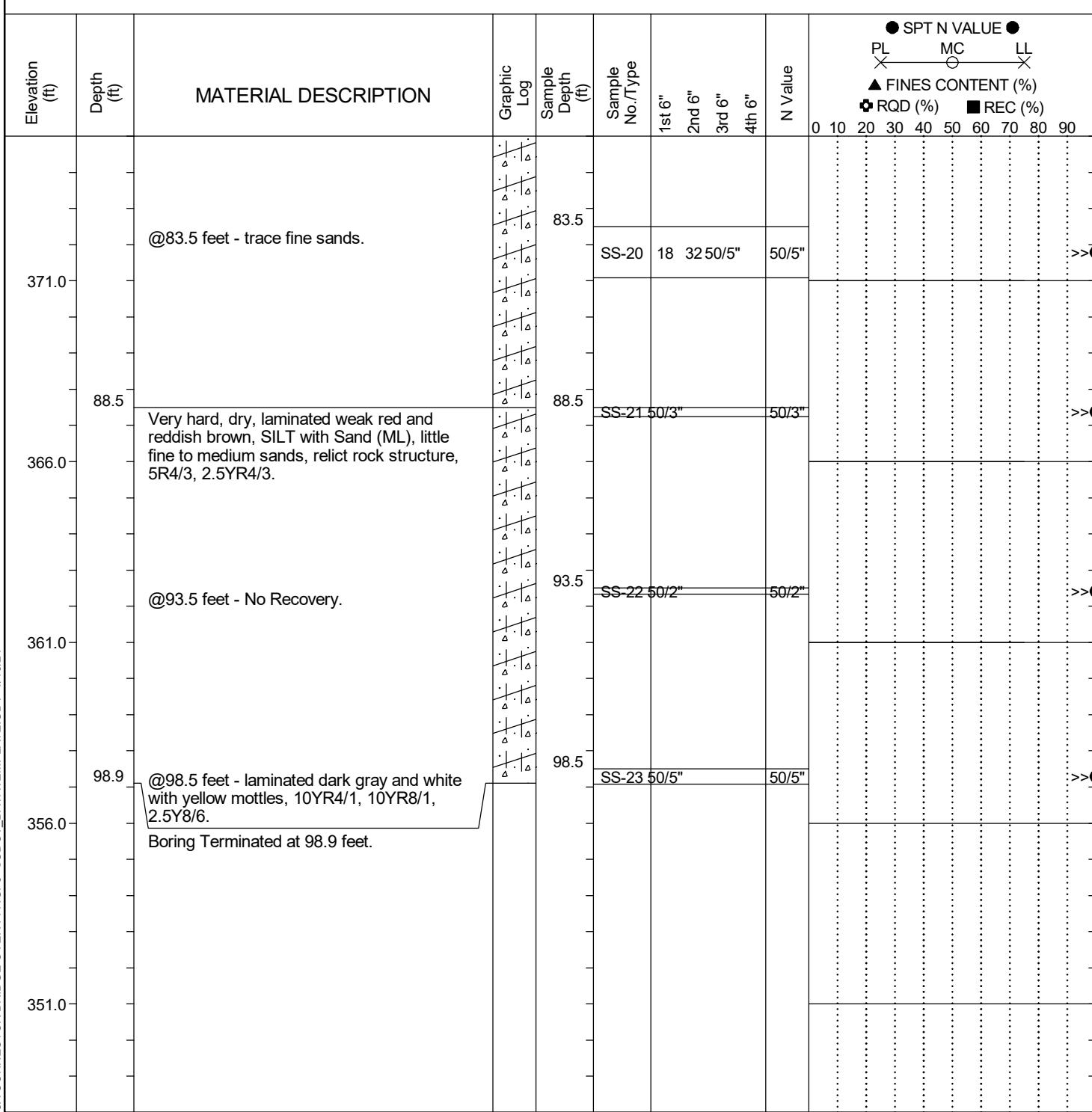
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



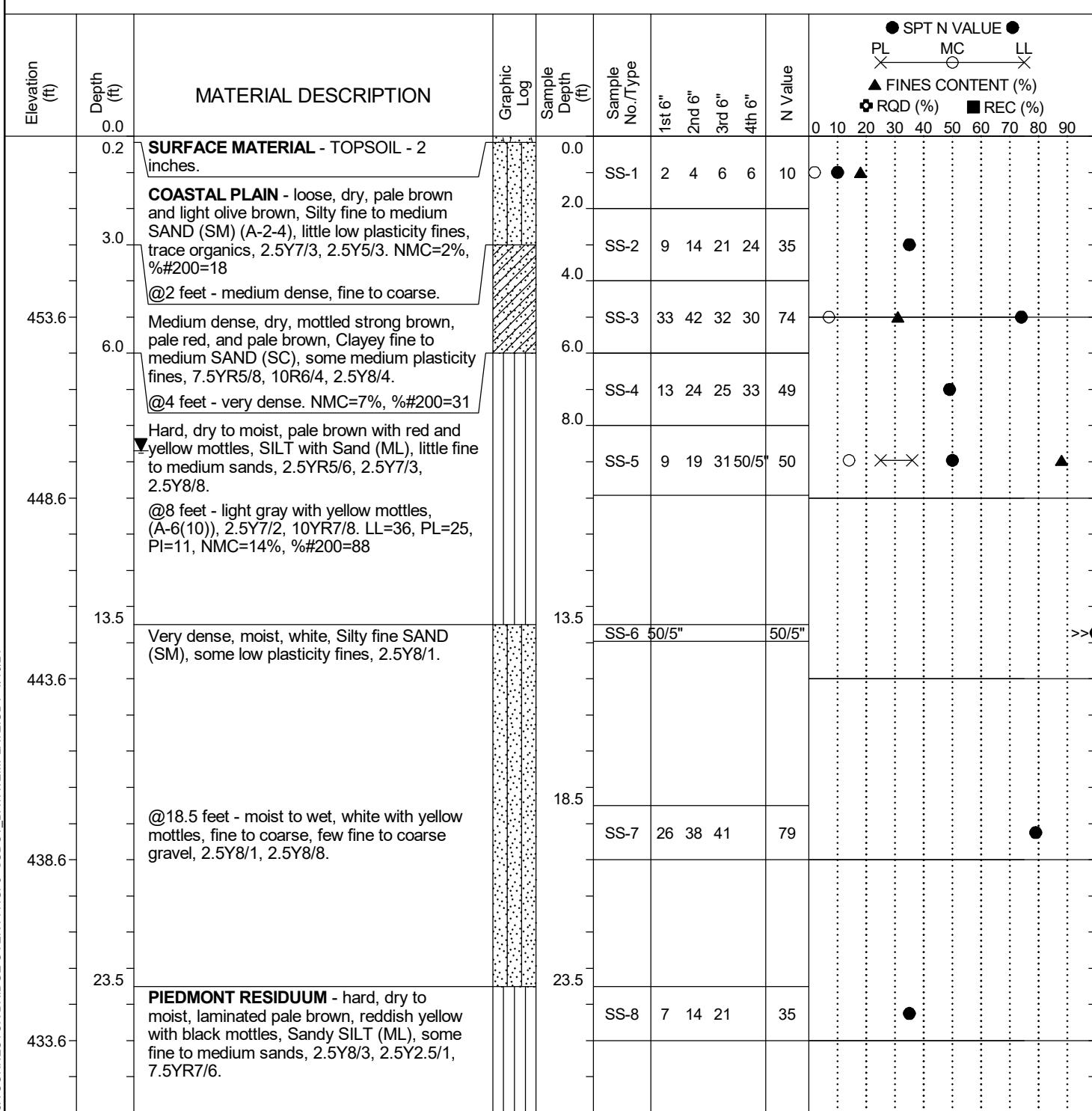
Soil Test Log

Project ID:	P042443 (S&ME 23610178A)		County:	Richland		Boring No.:	EB-6C
Site Description:	I-77 Exit 26 Phase I					Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+67.20	Offset:	148.4	Alignment:	Proposed
Elev.:	456.0 ft	Latitude:	34.190705874	Longitude:	-80.98373065	Date Started:	11/9/2023
Total Depth:	98.9 ft	Soil Depth:	98.9 ft	Core Depth:	N/A ft	Date Completed:	11/9/2023
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR NE



SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EM- 1
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	145+29.84	Offset:	35.5	Alignment:	Proposed
Elev.:	458.6 ft		Latitude:	34.190800788	Longitude:	-80.984592326	Date Started:	10/3/2023
Total Depth:	38.8 ft	Soil Depth:	38.8 ft	Core Depth:	N/A ft	Date Completed:	10/3/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic		Energy Ratio:	91.6%
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	8.7 ft



LEGEND

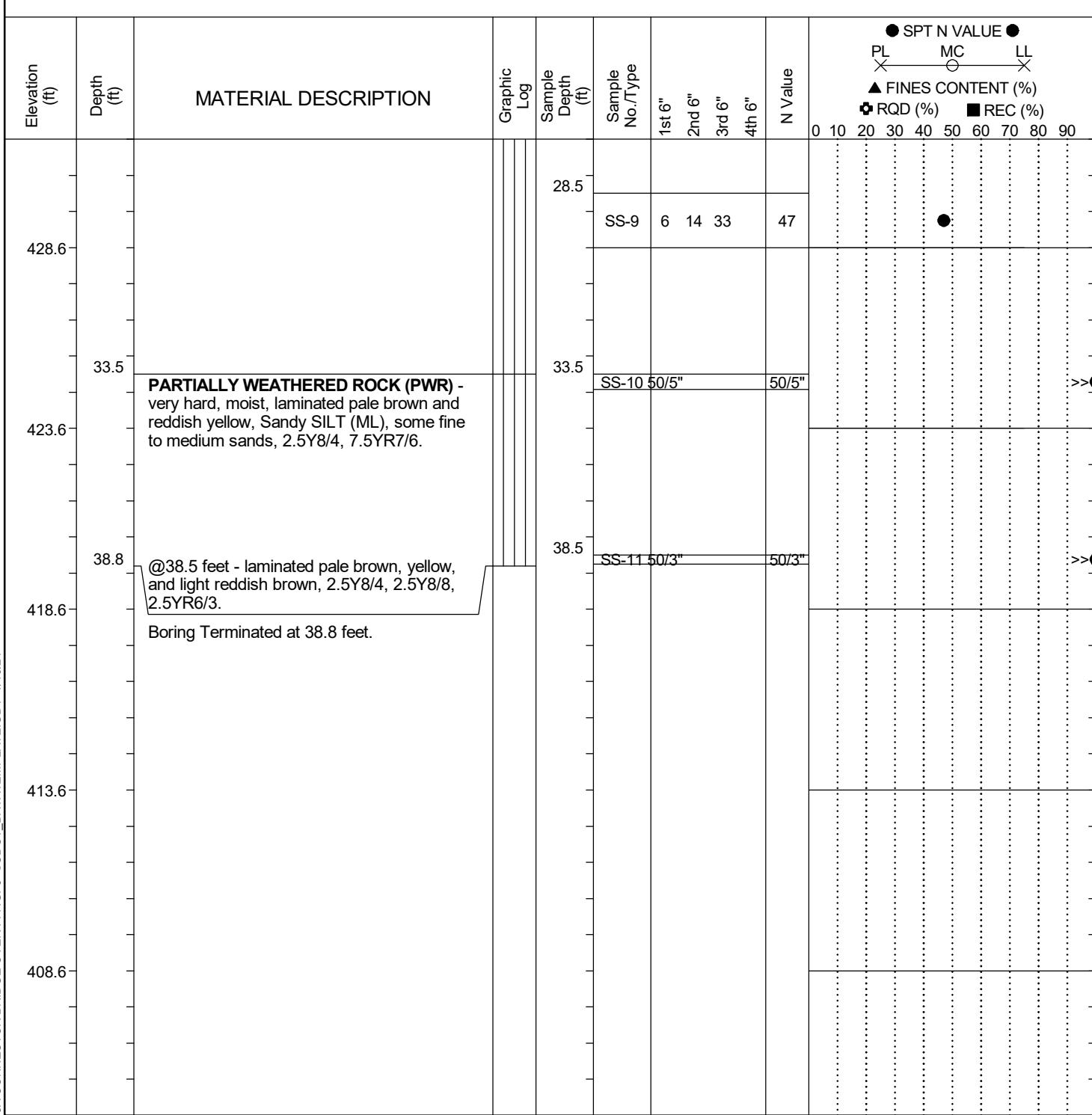
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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"			HSA - Hollow Stem Auger	RW - Rotary Wash		
UD - Undisturbed Sample	CU - Cuttings			CFA - Continuous Flight Augers	RC - Rock Core		
AWG - Rock Core, 1-1/8"	CT - Continuous Tube			DC - Driving Casing			



Soil Test Log

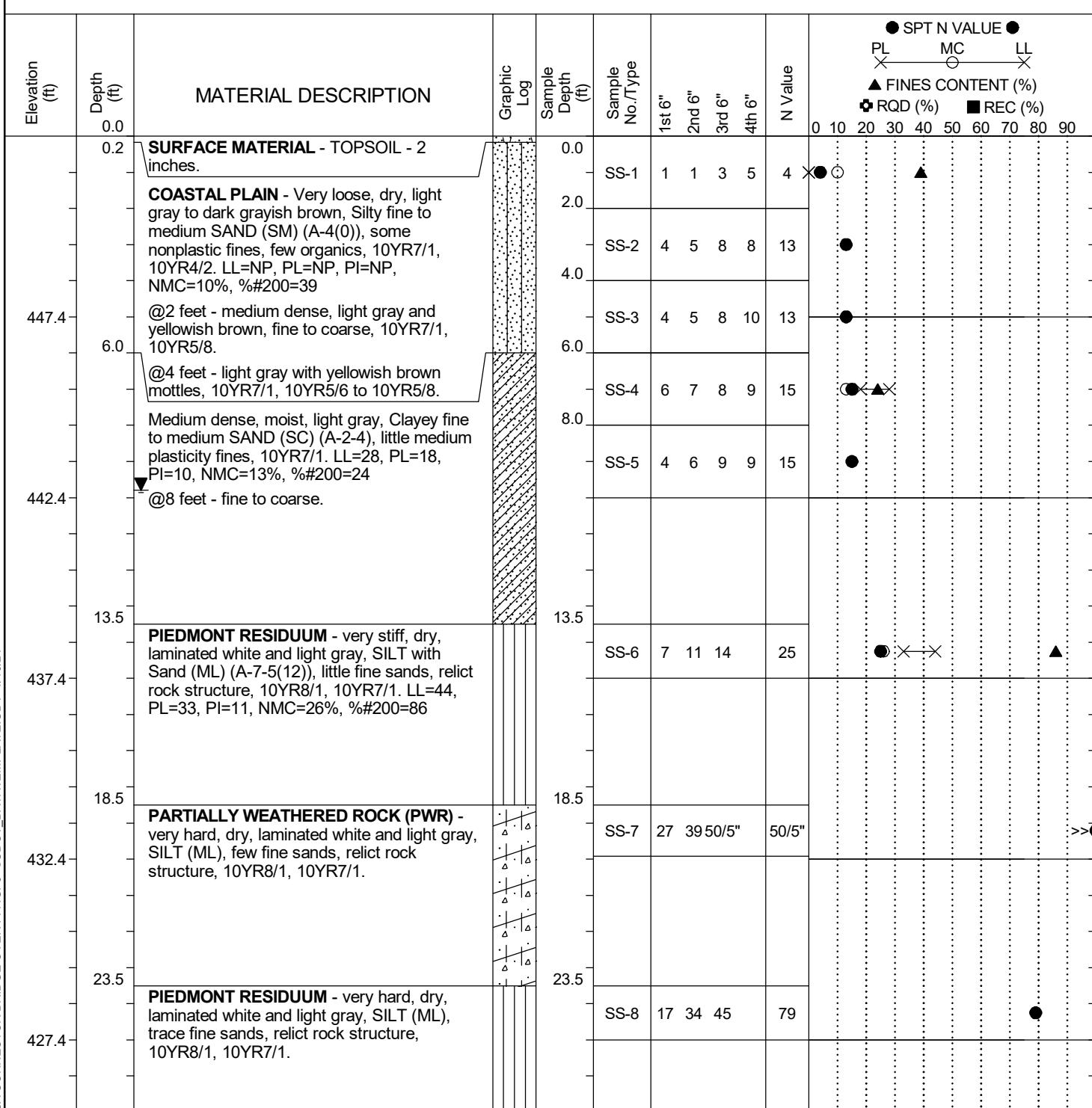
Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EM- 1
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	145+29.84	Offset:	35.5	Alignment:	Proposed
Elev.:	458.6 ft		Latitude:	34.190800788	Longitude:	-80.984592326	Date Started:	10/3/2023
Total Depth:	38.8 ft		Soil Depth:	38.8 ft	Core Depth:	N/A ft	Date Completed:	10/3/2023
Bore Hole Diameter (in):	4		Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)
Drill Machine:	CME-550X		Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%
Core Size:	N/A		Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EM- 2
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+61.97	Offset:	-31.4	Alignment:	Proposed	
Elev.:	452.4 ft	Latitude:	34.19142508	Longitude:	-80.98298593	Date Started:	10/2/2023	
Total Depth:	40 ft	Soil Depth:	40 ft	Core Depth:	N/A ft	Date Completed:	10/2/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	9.8 ft



LEGEND

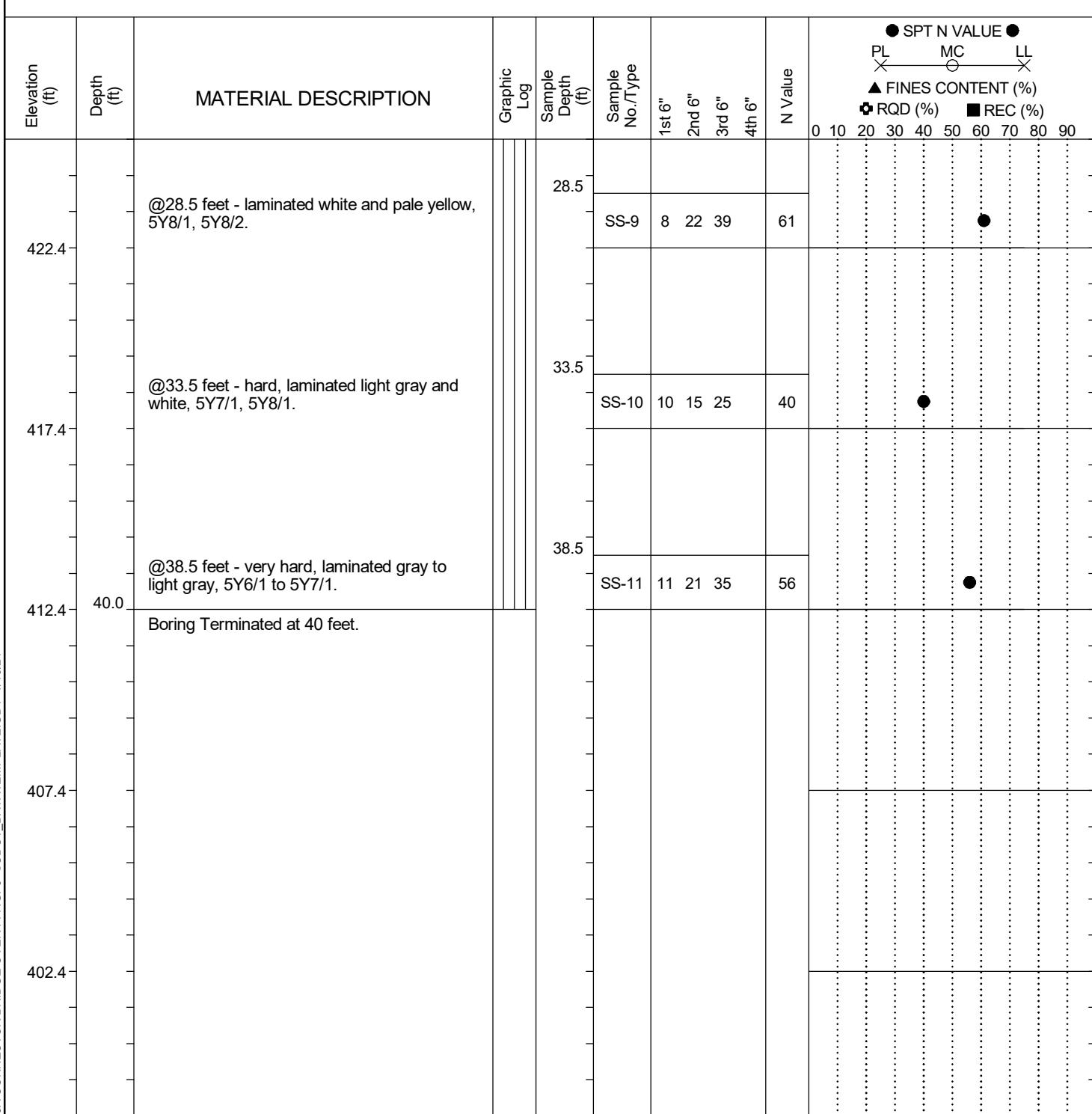
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



Soil Test Log

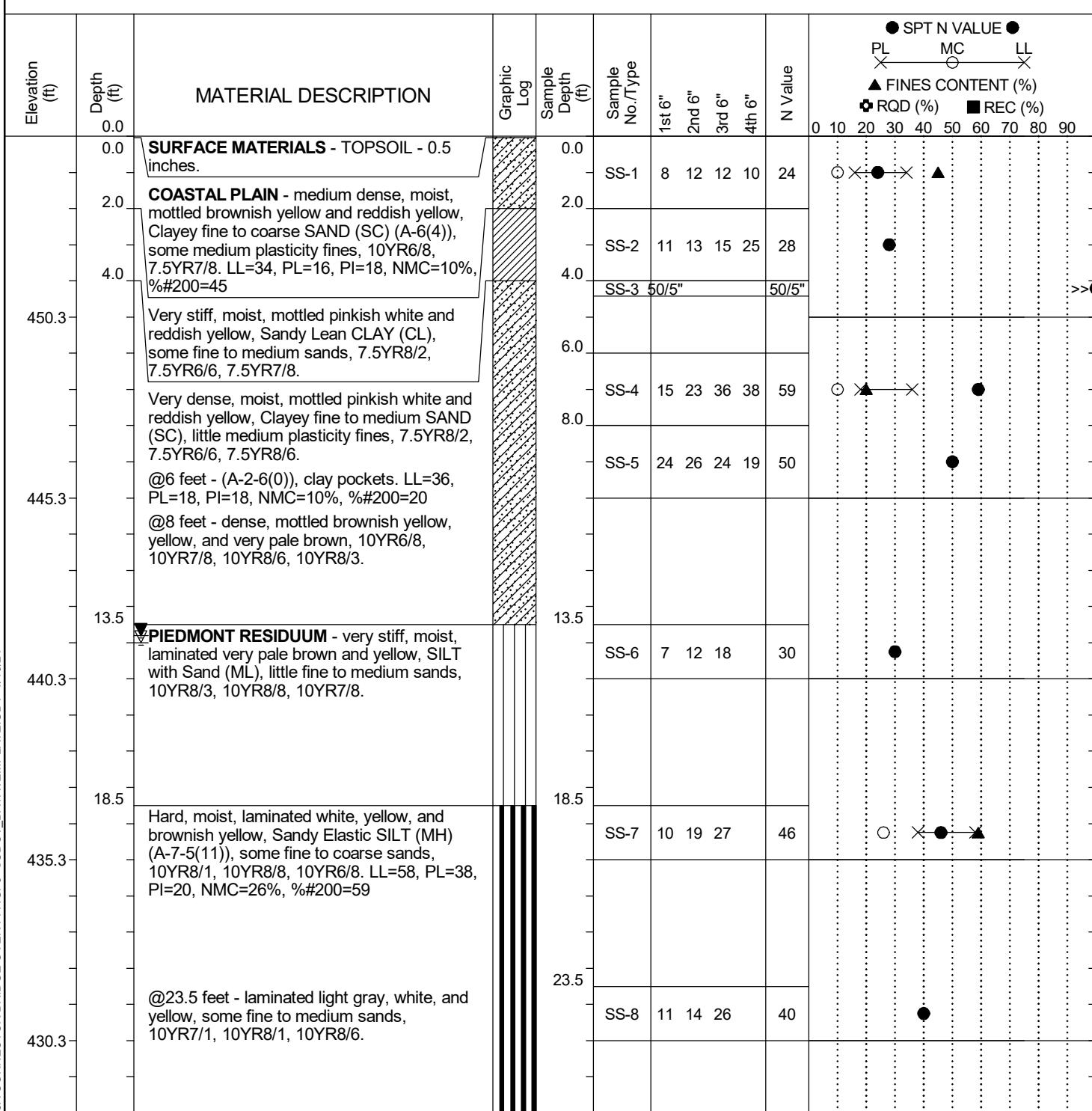
Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	EM- 2
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+61.97		Offset:	-31.4	Alignment:	Proposed
Elev.:	452.4 ft	Latitude:	34.19142508		Longitude:	-80.98298593	Date Started:	10/2/2023
Total Depth:	40 ft	Soil Depth:	40 ft		Core Depth:	N/A ft	Date Completed:	10/2/2023
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y <input checked="" type="checkbox"/>	N <input type="checkbox"/>	Liner Used:	Y <input checked="" type="checkbox"/>
Drill Machine:	CME-550X	Drill Method:	RW		Hammer Type:	Automatic	Energy Ratio:	87.6%
Core Size:	N/A	Driller:	S. Eubanks		Groundwater:	TOB	N/A	24HR



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 1C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	H. Skerkis		Boring Location:	148+68.15	Offset:	-38.1	Alignment:	Proposed
Elev.:	455.3 ft	Latitude:	34.19127875	Longitude:	-80.98360253	Date Started:	11/10/2023	
Total Depth:	100 ft	Soil Depth:	100 ft	Core Depth:	N/A ft	Date Completed:	11/10/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	D-50	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	96.8%	
Core Size:	N/A	Driller:	F. Crane	Groundwater:	TOB	N/A	24HR	13.8 ft

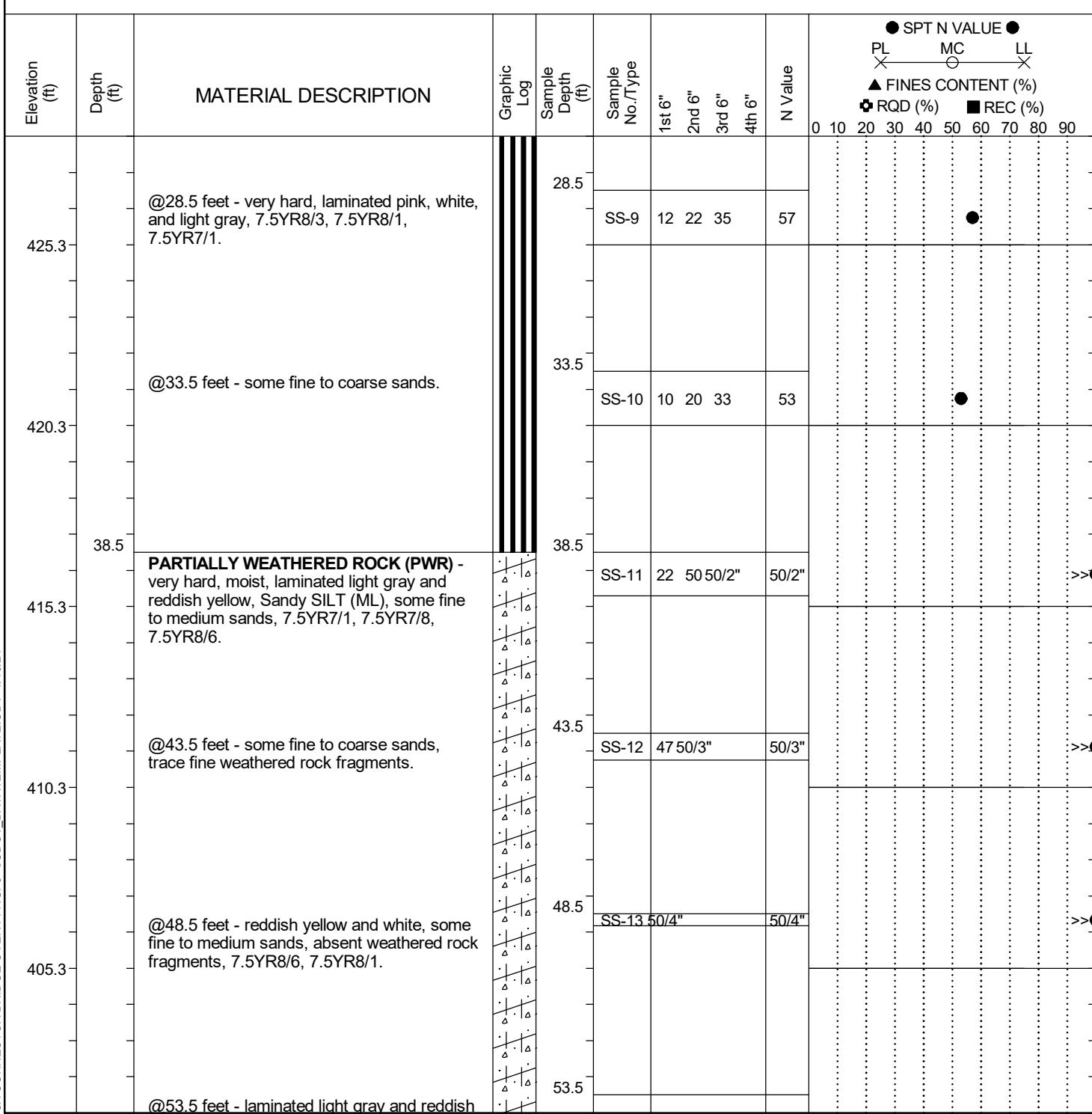


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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"			HSA - Hollow Stem Auger	RW - Rotary Wash		
UD - Undisturbed Sample	CU - Cuttings			CFA - Continuous Flight Augers	RC - Rock Core		
AWG - Rock Core, 1-1/8"	CT - Continuous Tube			DC - Driving Casing			

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 1C		
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd		
Eng./Geo.:	H. Skerkis		Boring Location:	148+68.15		Offset:	-38.1	Alignment:	Proposed	
Elev.:	455.3 ft		Latitude:	34.19127875		Longitude:	-80.98360253		Date Started:	11/10/2023
Total Depth:	100 ft		Soil Depth:	100 ft		Core Depth:	N/A ft		Date Completed:	11/10/2023
Bore Hole Diameter (in):	4		Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y	(N)
Drill Machine:	D-50		Drill Method:	RW		Hammer Type:	Automatic		Energy Ratio:	96.8%
Core Size:	N/A		Driller:	F. Crane		Groundwater:	TOB	N/A	24HR	13.8 ft

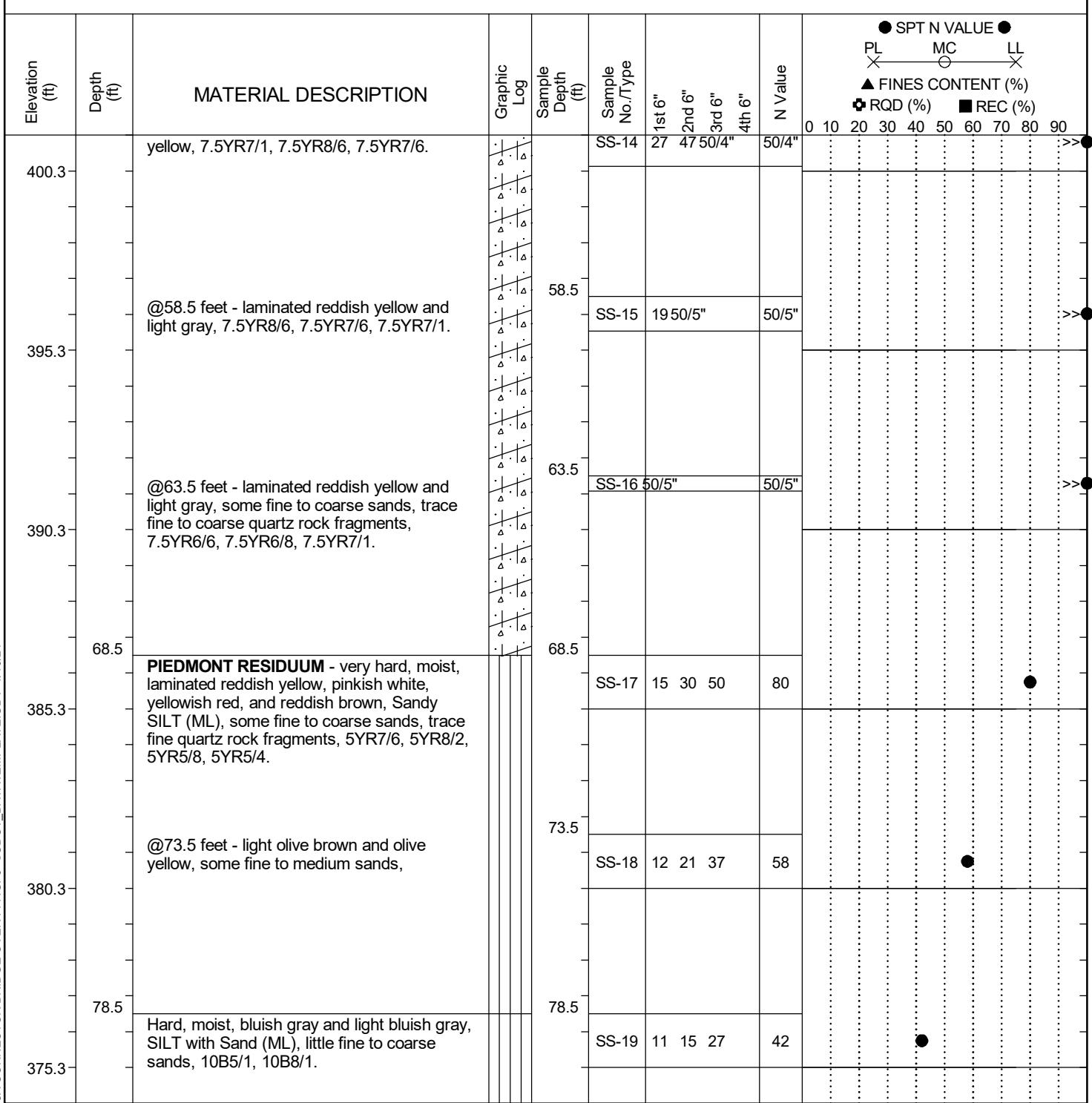


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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	UD - Undisturbed Sample	CU - Cuttings	HSA - Hollow Stem Auger	RW - Rotary Wash	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube			DC - Driving Casing			

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 1C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	H. Skerkis		Boring Location:	148+68.15	Offset:	-38.1	Alignment:	Proposed
Elev.:	455.3 ft	Latitude:	34.19127875	Longitude:	-80.98360253	Date Started:	11/10/2023	
Total Depth:	100 ft	Soil Depth:	100 ft	Core Depth:	N/A ft	Date Completed:	11/10/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	D-50	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	96.8%	
Core Size:	N/A	Driller:	F. Crane	Groundwater:	TOB	N/A	24HR	13.8 ft



LEGEND

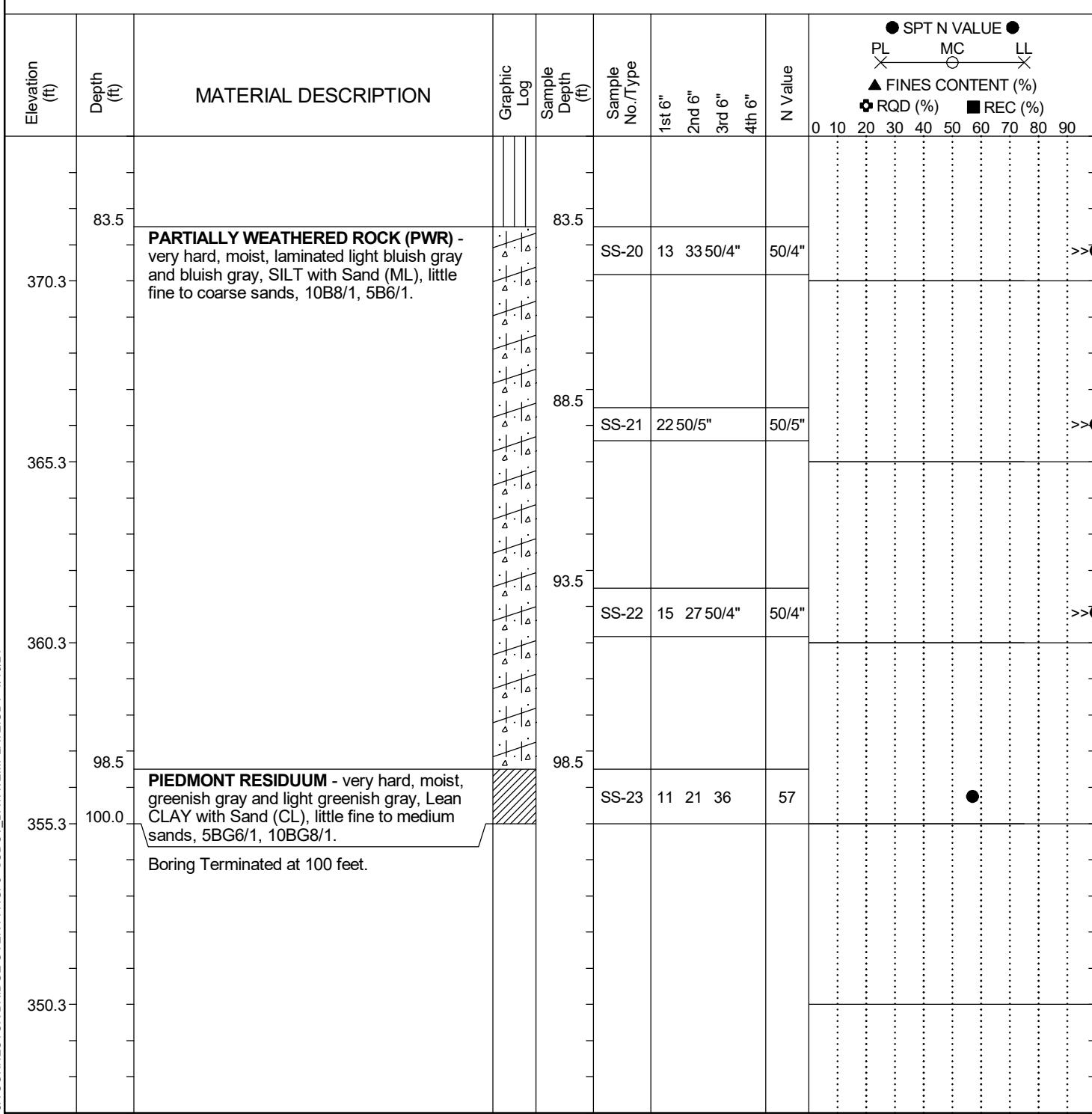
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



Soil Test Log

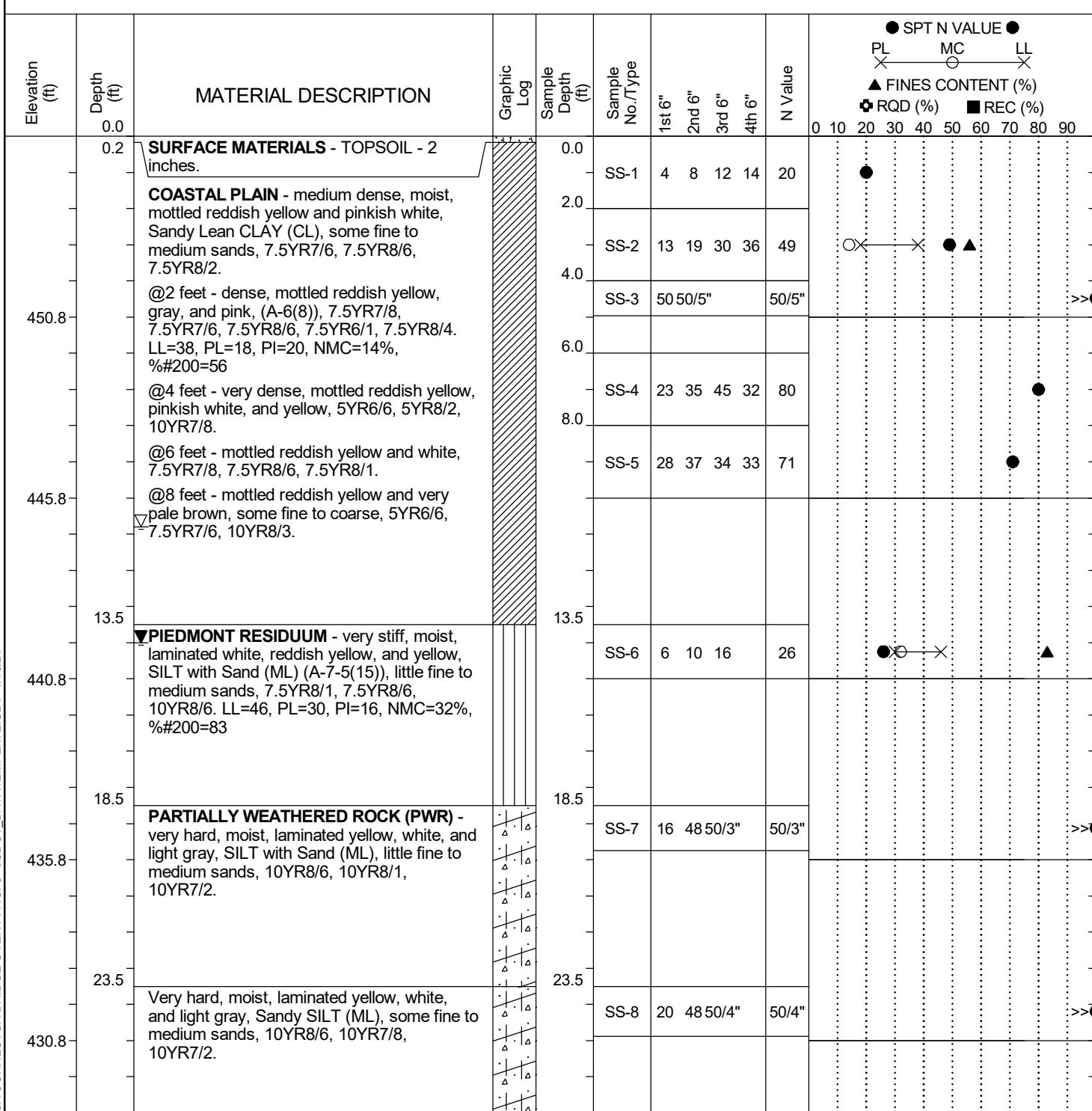
Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 1C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	H. Skerkis		Boring Location:	148+68.15	Offset:	-38.1	Alignment:	Proposed
Elev.:	455.3 ft	Latitude:	34.19127875	Longitude:	-80.98360253	Date Started:	11/10/2023	
Total Depth:	100 ft	Soil Depth:	100 ft	Core Depth:	N/A ft	Date Completed:	11/10/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	D-50	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	96.8%	
Core Size:	N/A	Driller:	F. Crane	Groundwater:	TOB	N/A	24HR	13.8 ft



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 2C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	H. Skerkis		Boring Location:	148+68.15	Offset:	9.4	Alignment:	Proposed
Elev.:	455.8 ft	Latitude:	34.191154573	Longitude:	-80.98355426	Date Started:	11/15/2023	
Total Depth:	99.3 ft	Soil Depth:	99.3 ft	Core Depth:	N/A ft	Date Completed:	11/15/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	D-50	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	96.8%	
Core Size:	N/A	Driller:	F. Crane	Groundwater:	TOB	N/A	24HR	14 ft

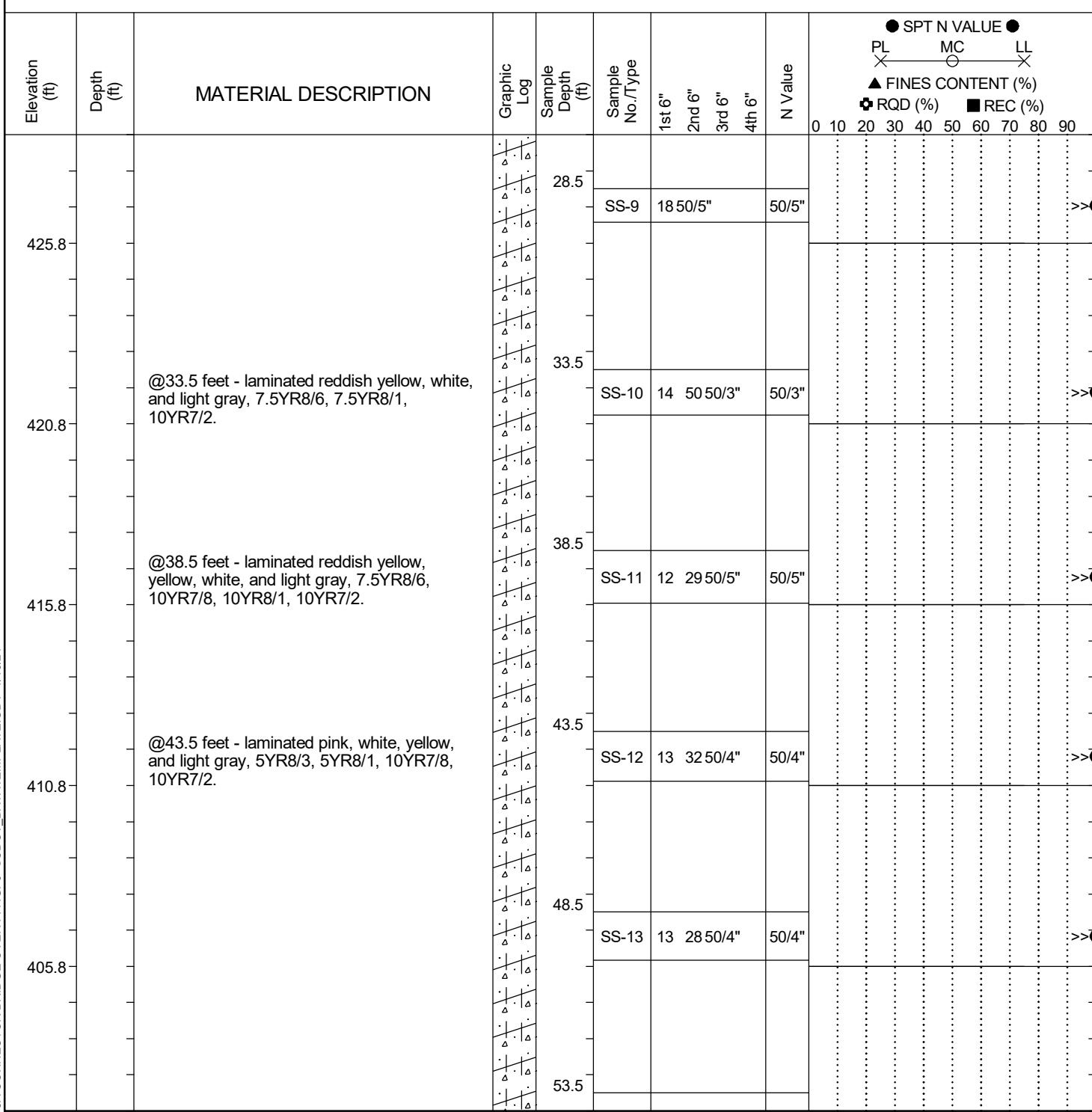


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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash				
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core				
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing					

Project ID:	P042443 (S&ME 23610178A)		County:	Richland		Boring No.:	IB- 2C	
Site Description:	I-77 Exit 26 Phase I					Route:	Connector Rd	
Eng./Geo.:	H. Skerkis		Boring Location:	148+68.15		Offset:	9.4	Alignment:
Elev.:	455.8 ft	Latitude:	34.191154573	Longitude:	-80.98355426	Date Started:	11/15/2023	
Total Depth:	99.3 ft	Soil Depth:	99.3 ft	Core Depth:	N/A ft	Date Completed:	11/15/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	D-50	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	96.8%	
Core Size:	N/A	Driller:	F. Crane	Groundwater:	TOB	N/A	24HR	14 ft

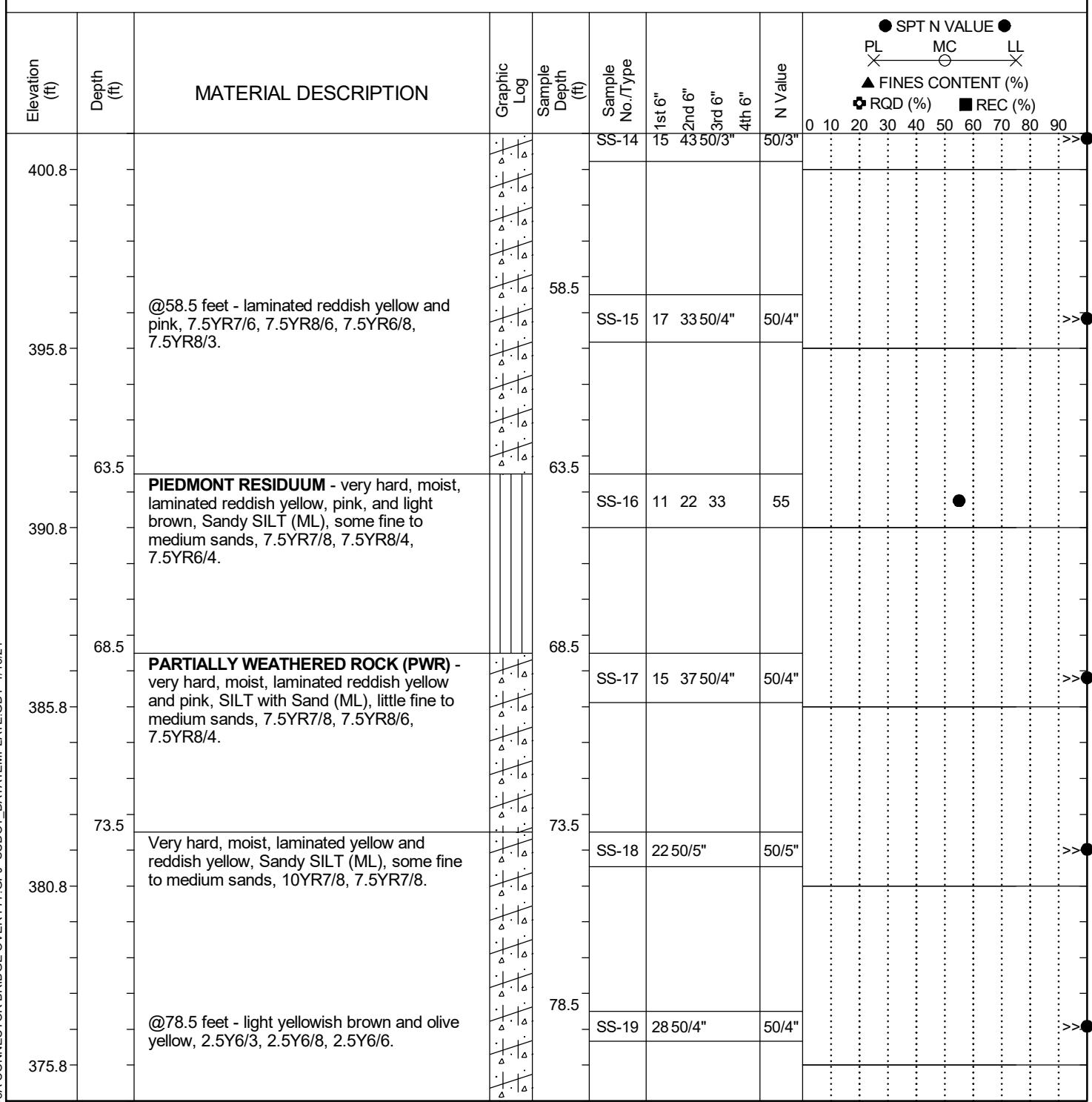


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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 2C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	H. Skerkis		Boring Location:	148+68.15	Offset:	9.4	Alignment:	Proposed
Elev.:	455.8 ft	Latitude:	34.191154573	Longitude:	-80.98355426	Date Started:	11/15/2023	
Total Depth:	99.3 ft	Soil Depth:	99.3 ft	Core Depth:	N/A ft	Date Completed:	11/15/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	D-50	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	96.8%	
Core Size:	N/A	Driller:	F. Crane	Groundwater:	TOB	N/A	24HR	14 ft



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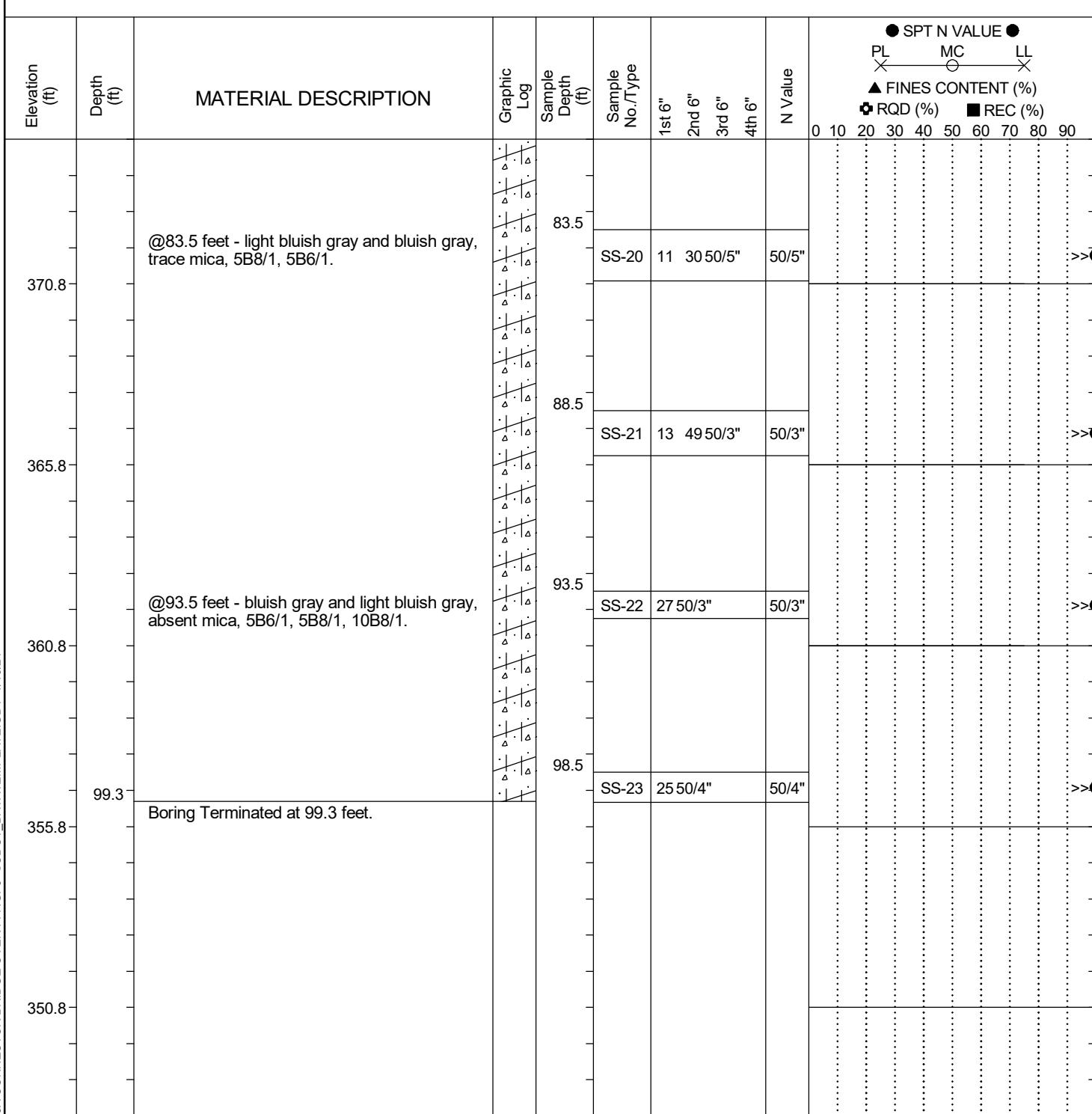
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



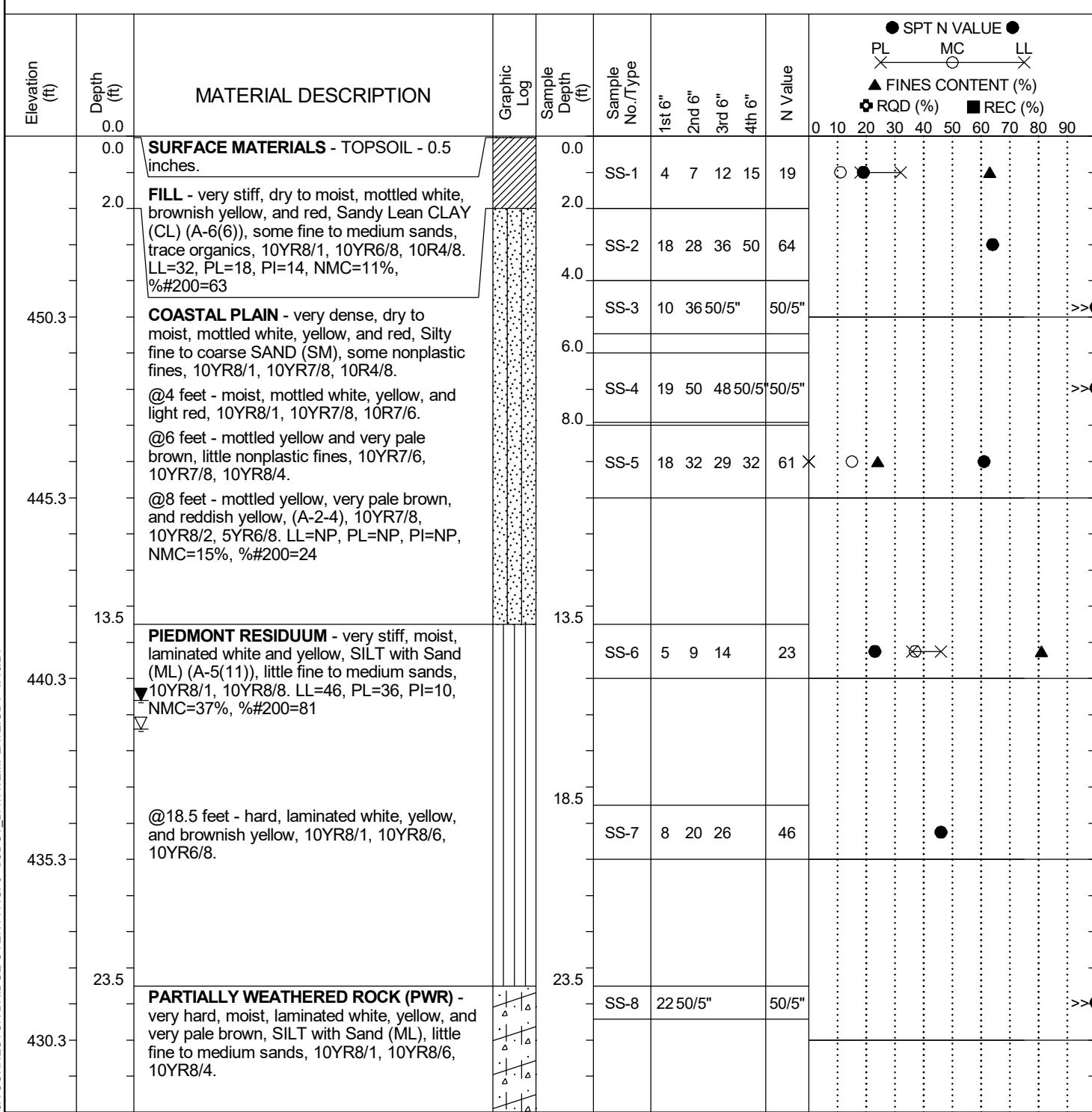
Soil Test Log

Project ID:	P042443 (S&ME 23610178A)		County:	Richland		Boring No.:	IB- 2C	
Site Description:	I-77 Exit 26 Phase I					Route:	Connector Rd	
Eng./Geo.:	H. Skerkis		Boring Location:	148+68.15	Offset:	9.4	Alignment:	Proposed
Elev.:	455.8 ft	Latitude:	34.191154573	Longitude:	-80.98355426	Date Started:	11/15/2023	
Total Depth:	99.3 ft	Soil Depth:	99.3 ft	Core Depth:	N/A ft	Date Completed:	11/15/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	D-50	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	96.8%	
Core Size:	N/A	Driller:	F. Crane	Groundwater:	TOB	N/A	24HR	



SAMPLER TYPE		DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 3C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	H. Skerkis		Boring Location:	148+68.32	Offset:	58.4	Alignment:	Proposed
Elev.:	455.3 ft	Latitude:	34.191026746	Longitude:	-80.98350398	Date Started:	11/2/2023	
Total Depth:	100 ft	Soil Depth:	100 ft	Core Depth:	N/A ft	Date Completed:	11/2/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.0%	
Core Size:	N/A	Driller:	T. Shearin	Groundwater:	TOB	N/A	24HR	15.6 ft

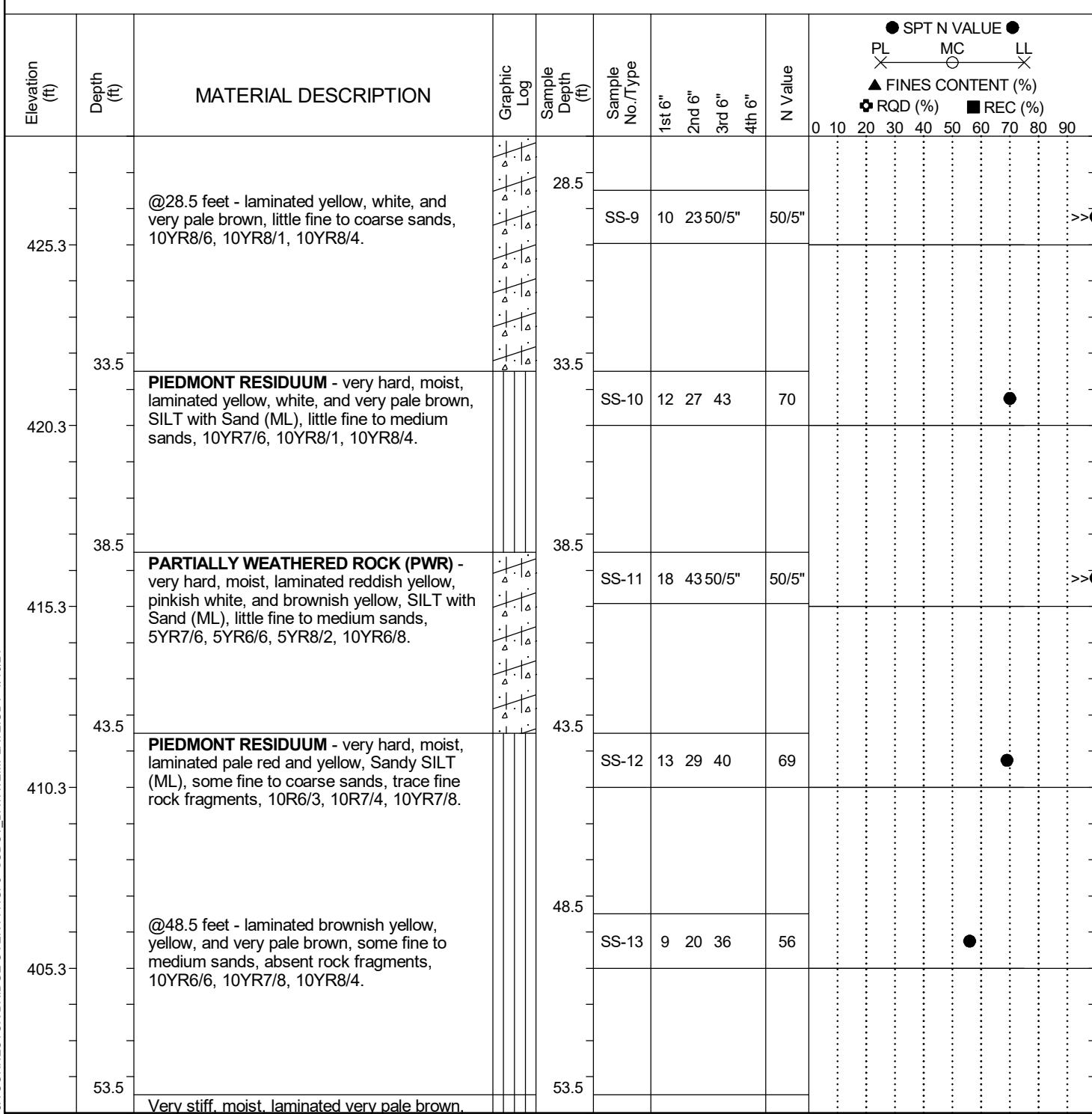


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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash				
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core				
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing					

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 3C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	H. Skerkis		Boring Location:	148+68.32	Offset:	58.4	Alignment:	Proposed
Elev.:	455.3 ft	Latitude:	34.191026746	Longitude:	-80.98350398	Date Started:	11/2/2023	
Total Depth:	100 ft	Soil Depth:	100 ft	Core Depth:	N/A ft	Date Completed:	11/2/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.0%	
Core Size:	N/A	Driller:	T. Shearin	Groundwater:	TOB	N/A	24HR	15.6 ft

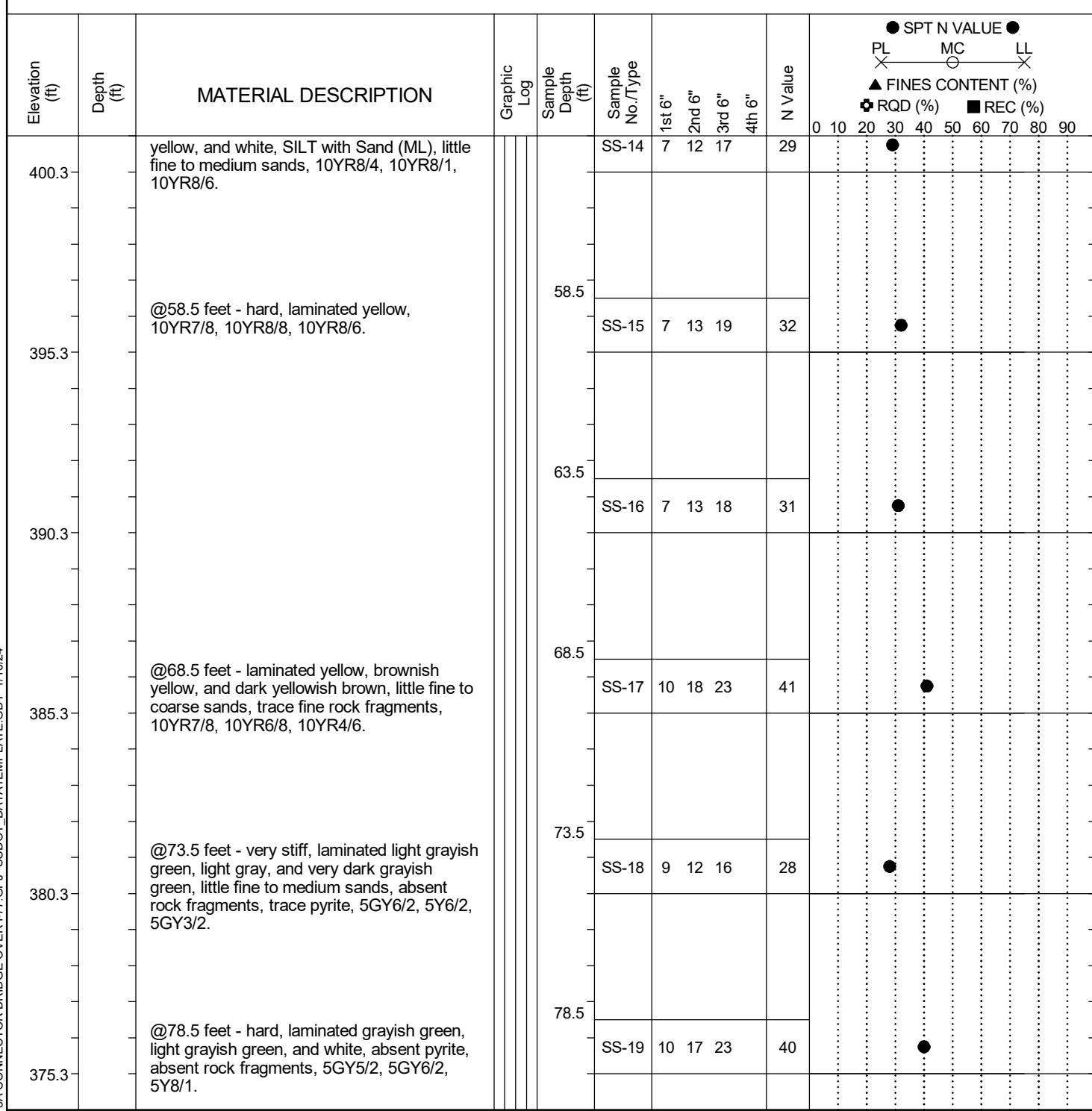


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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash				
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core				
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing					

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 3C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	H. Skerkis		Boring Location:	148+68.32	Offset:	58.4	Alignment:	Proposed
Elev.:	455.3 ft	Latitude:	34.191026746	Longitude:	-80.98350398	Date Started:	11/2/2023	
Total Depth:	100 ft	Soil Depth:	100 ft	Core Depth:	N/A ft	Date Completed:	11/2/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.0%	
Core Size:	N/A	Driller:	T. Shearin	Groundwater:	TOB	N/A	24HR	15.6 ft

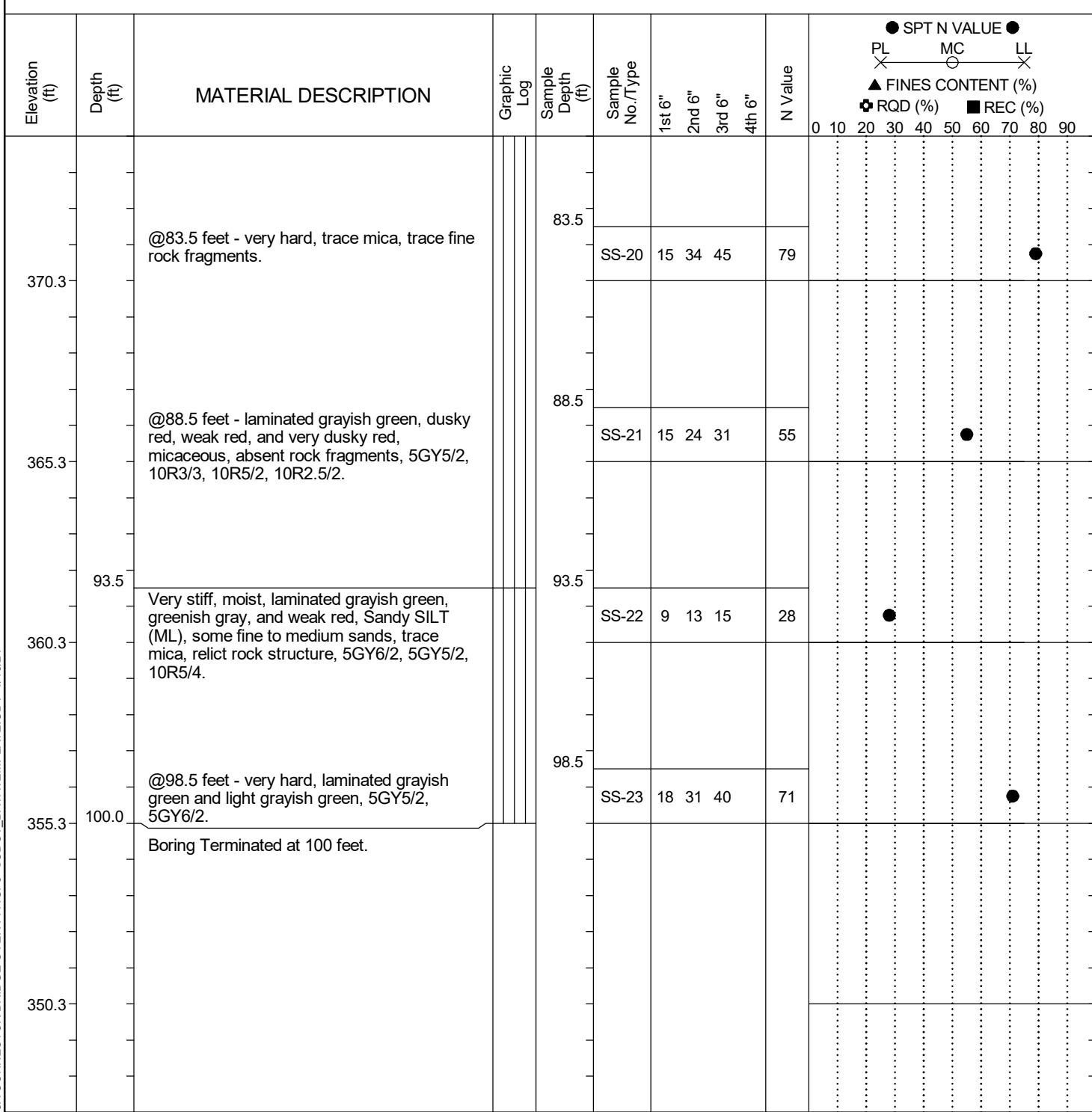


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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

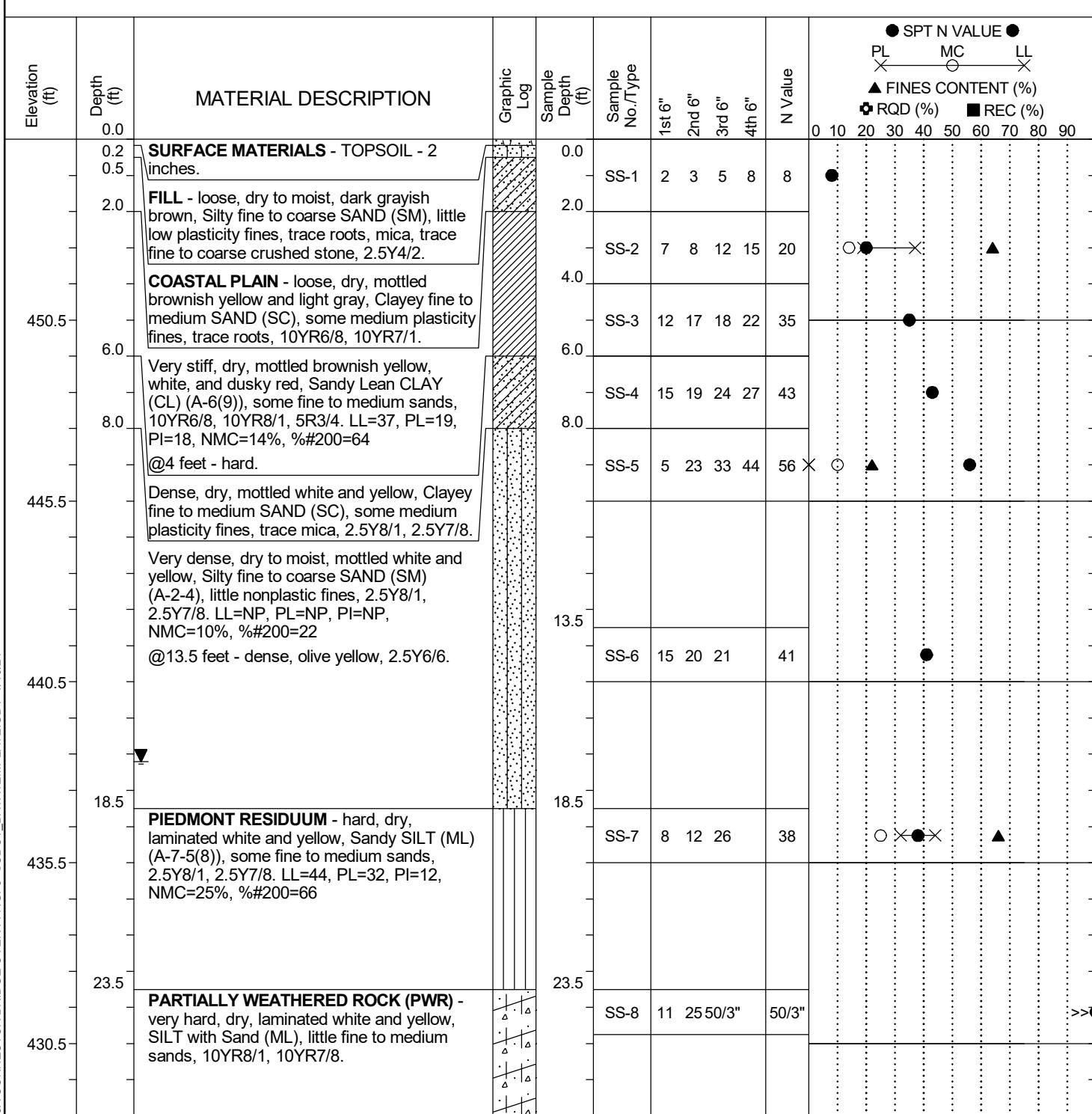
Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 3C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	H. Skerkis		Boring Location:	148+68.32	Offset:	58.4	Alignment:	Proposed
Elev.:	455.3 ft	Latitude:	34.191026746	Longitude:	-80.98350398	Date Started:	11/2/2023	
Total Depth:	100 ft	Soil Depth:	100 ft	Core Depth:	N/A ft	Date Completed:	11/2/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.0%	
Core Size:	N/A	Driller:	T. Shearin	Groundwater:	TOB	N/A	24HR	15.6 ft



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 4C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+68.19	Offset:	-54.5	Alignment:	Proposed
Elev.:	455.5 ft		Latitude:	34.191237361	Longitude:	-80.9839338	Date Started:	11/15/2023
Total Depth:	100 ft		Soil Depth:	100 ft	Core Depth:	N/A ft	Date Completed:	11/16/2023
Bore Hole Diameter (in):	4		Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)
Drill Machine:	CME-550X		Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%
Core Size:	N/A		Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR

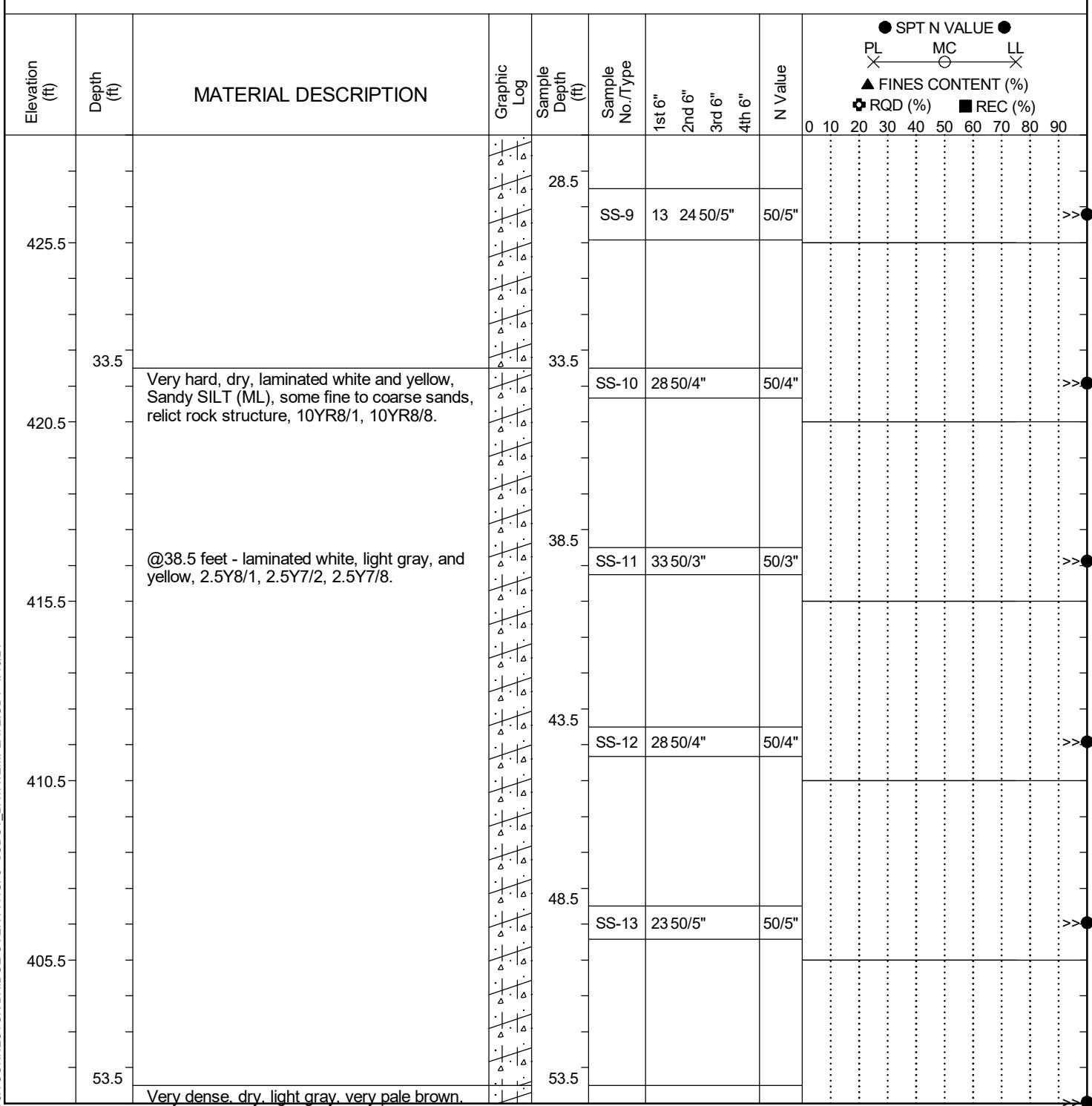


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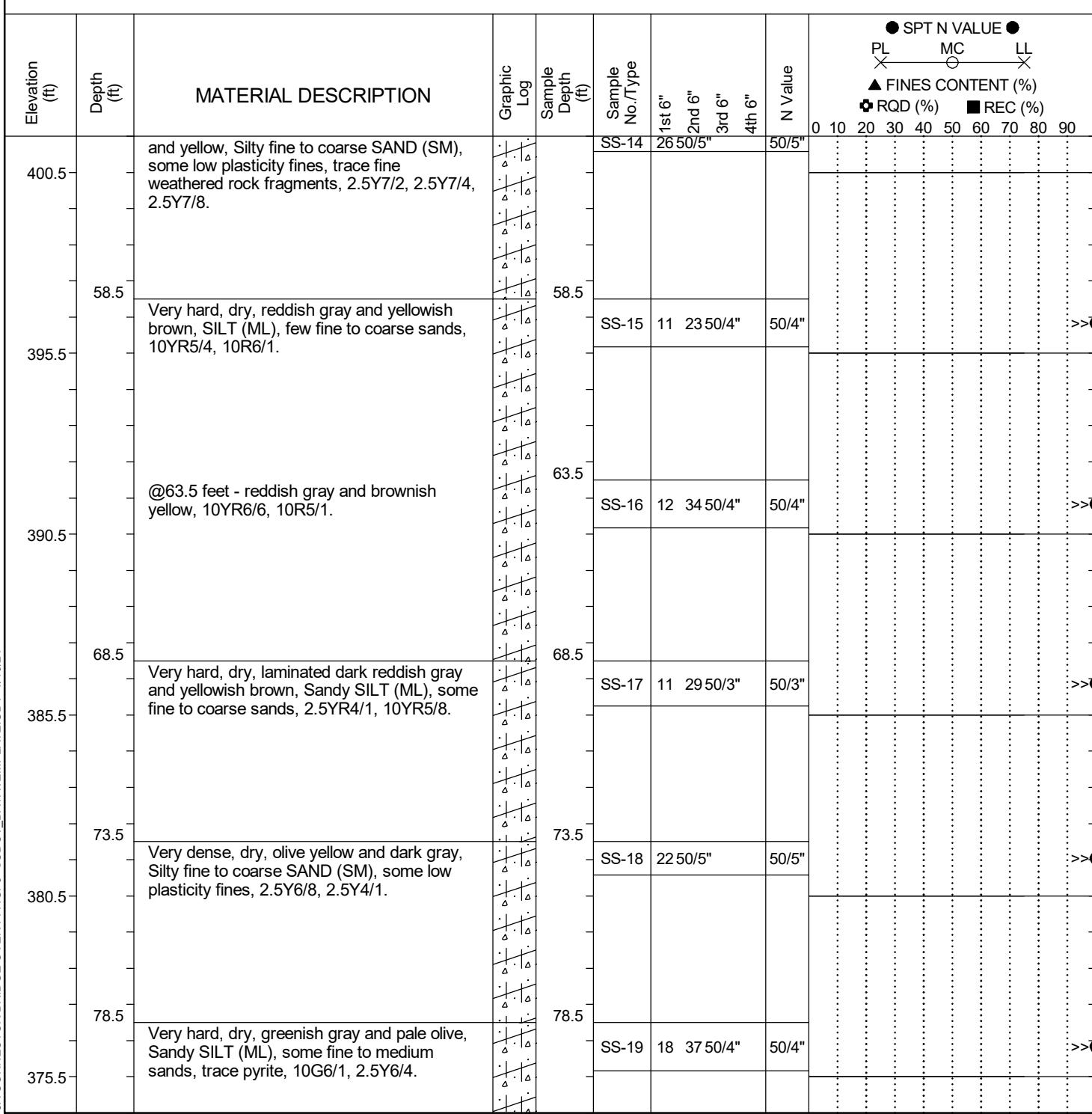
SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	UD - Undisturbed Sample	CU - Cuttings	HSA - Hollow Stem Auger	RW - Rotary Wash	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube			DC - Driving Casing			

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 4C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+68.19	Offset:	-54.5	Alignment:	Proposed
Elev.:	455.5 ft		Latitude:	34.191237361	Longitude:	-80.9839338	Date Started:	11/15/2023
Total Depth:	100 ft	Soil Depth:	100 ft	Core Depth:	N/A ft	Date Completed:	11/16/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic		Energy Ratio:	91.6%
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	17.2 ft



SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 4C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+68.19	Offset:	-54.5	Alignment:	Proposed
Elev.:	455.5 ft		Latitude:	34.191237361	Longitude:	-80.9839338	Date Started:	11/15/2023
Total Depth:	100 ft	Soil Depth:	100 ft	Core Depth:	N/A ft	Date Completed:	11/16/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:		
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	17.2 ft



LEGEND

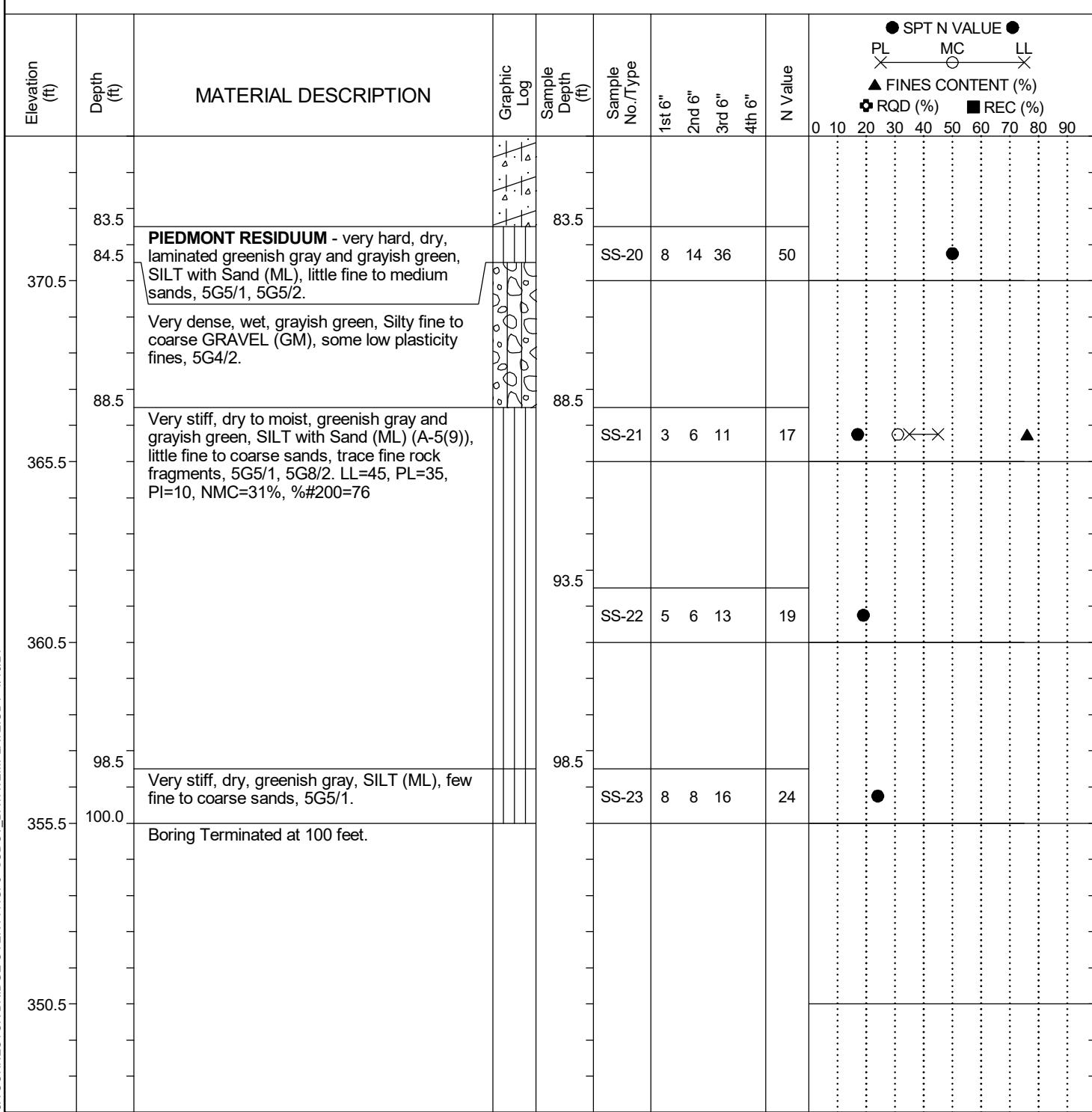
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



Soil Test Log

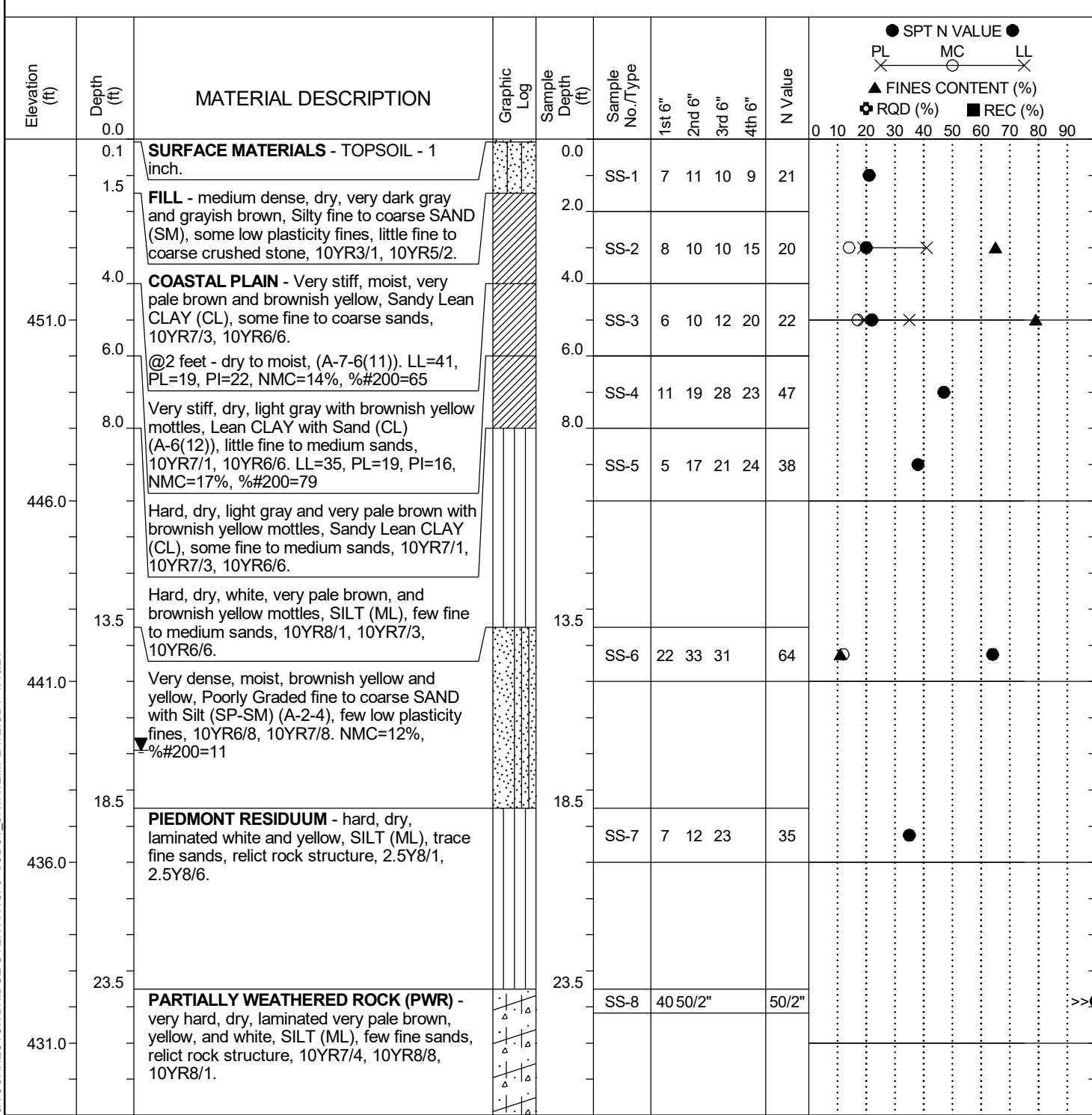
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Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+68.19	Offset:	-54.5	Alignment:	Proposed
Elev.:	455.5 ft		Latitude:	34.191237361	Longitude:	-80.9839338	Date Started:	11/15/2023
Total Depth:	100 ft	Soil Depth:	100 ft	Core Depth:	N/A ft	Date Completed:		11/16/2023
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:		
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:		
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	17.2 ft



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

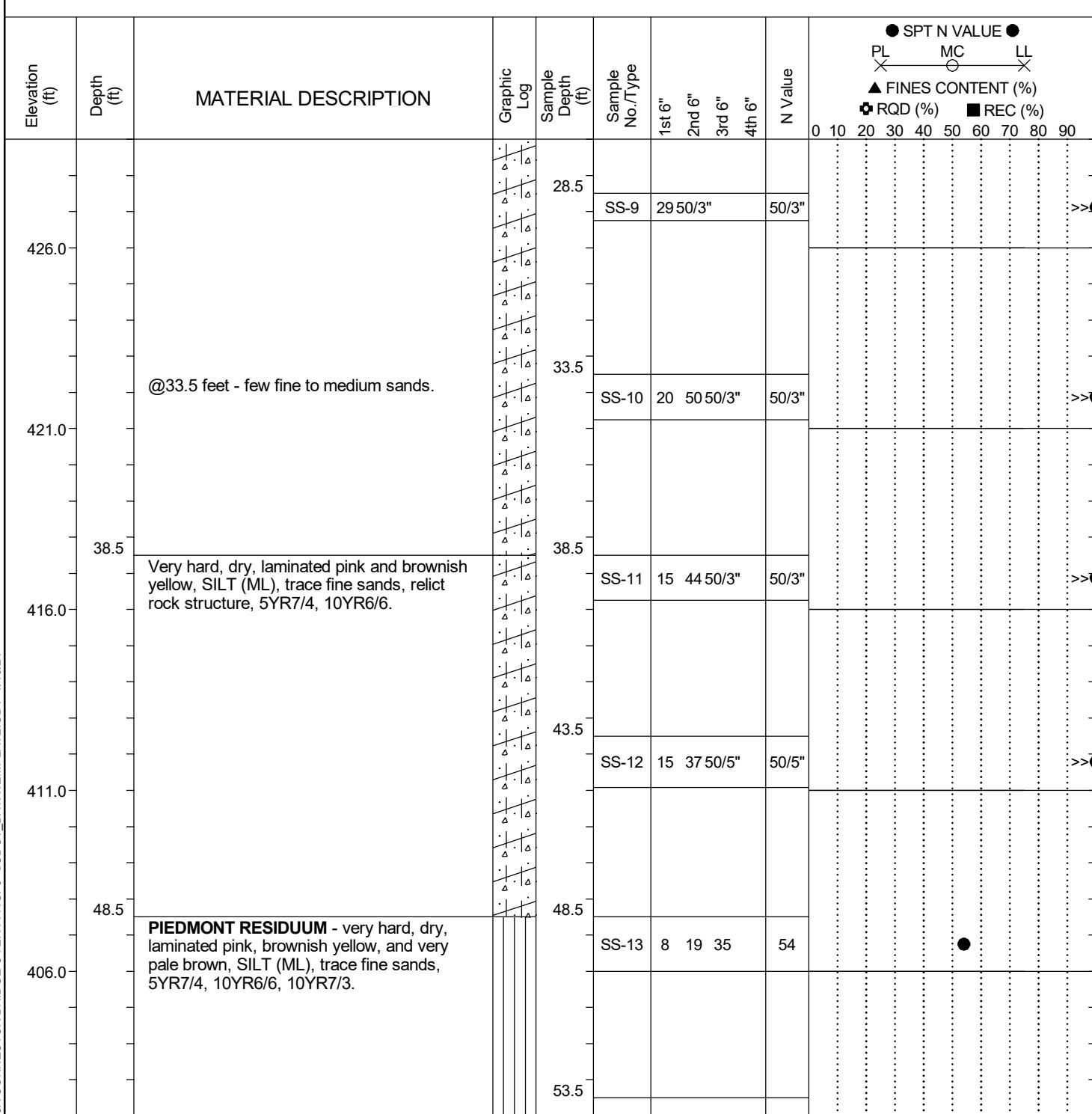
Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 5C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+67.50	Offset:	-7.4	Alignment:	Proposed	
Elev.:	456.0 ft	Latitude:	34.19111364	Longitude:	-80.98388809	Date Started:	11/14/2023	
Total Depth:	99.3 ft	Soil Depth:	99.3 ft	Core Depth:	N/A ft	Date Completed:	11/14/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	16.9 ft



Continued Next Page

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 5C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+67.50	Offset:	-7.4	Alignment:	Proposed	
Elev.:	456.0 ft	Latitude:	34.19111364	Longitude:	-80.98388809	Date Started:	11/14/2023	
Total Depth:	99.3 ft	Soil Depth:	99.3 ft	Core Depth:	N/A ft	Date Completed:	11/14/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	16.9 ft

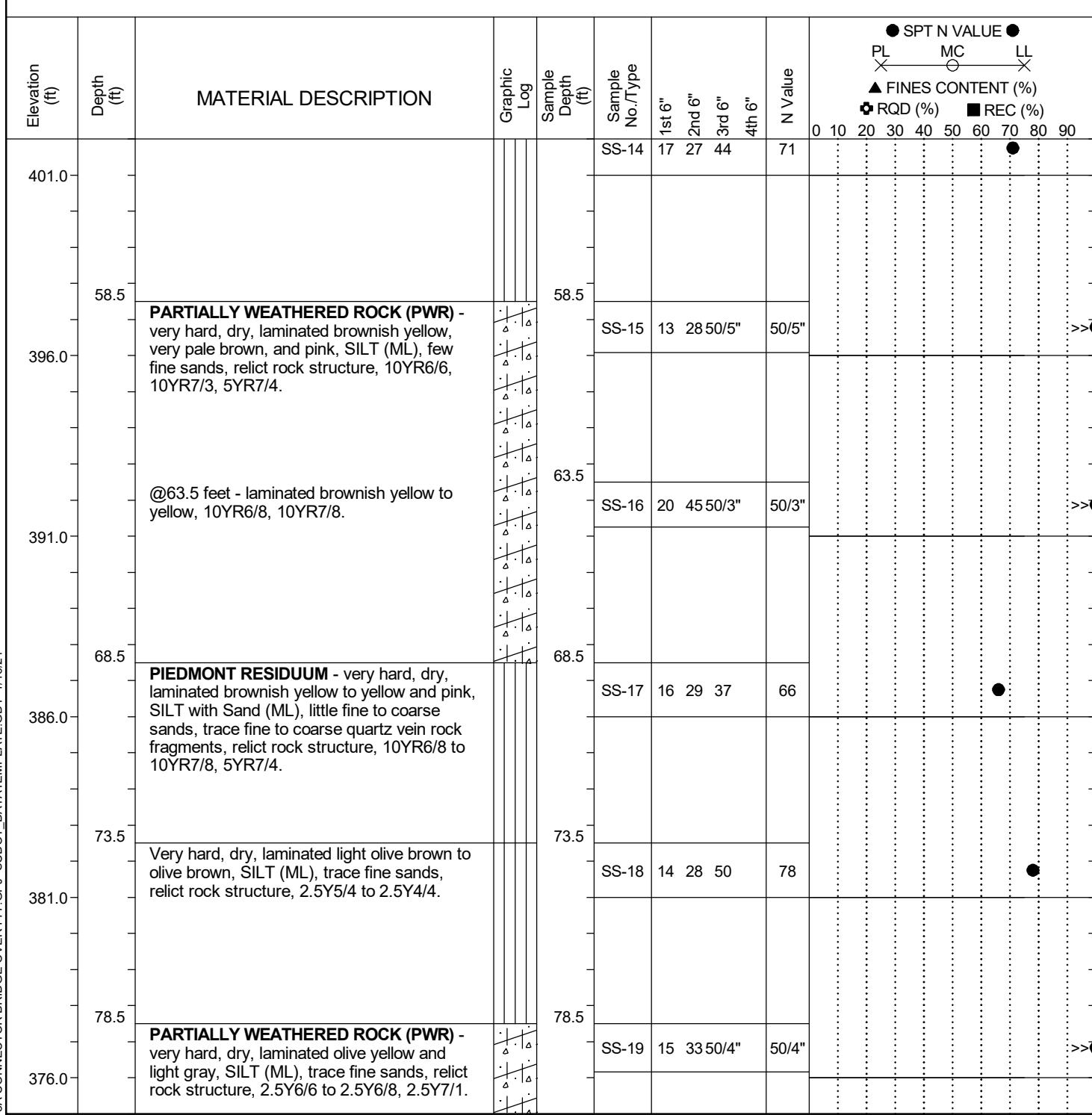


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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 5C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+67.50	Offset:	-7.4	Alignment:	Proposed	
Elev.:	456.0 ft	Latitude:	34.19111364	Longitude:	-80.98388809	Date Started:	11/14/2023	
Total Depth:	99.3 ft	Soil Depth:	99.3 ft	Core Depth:	N/A ft	Date Completed:	11/14/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	16.9 ft



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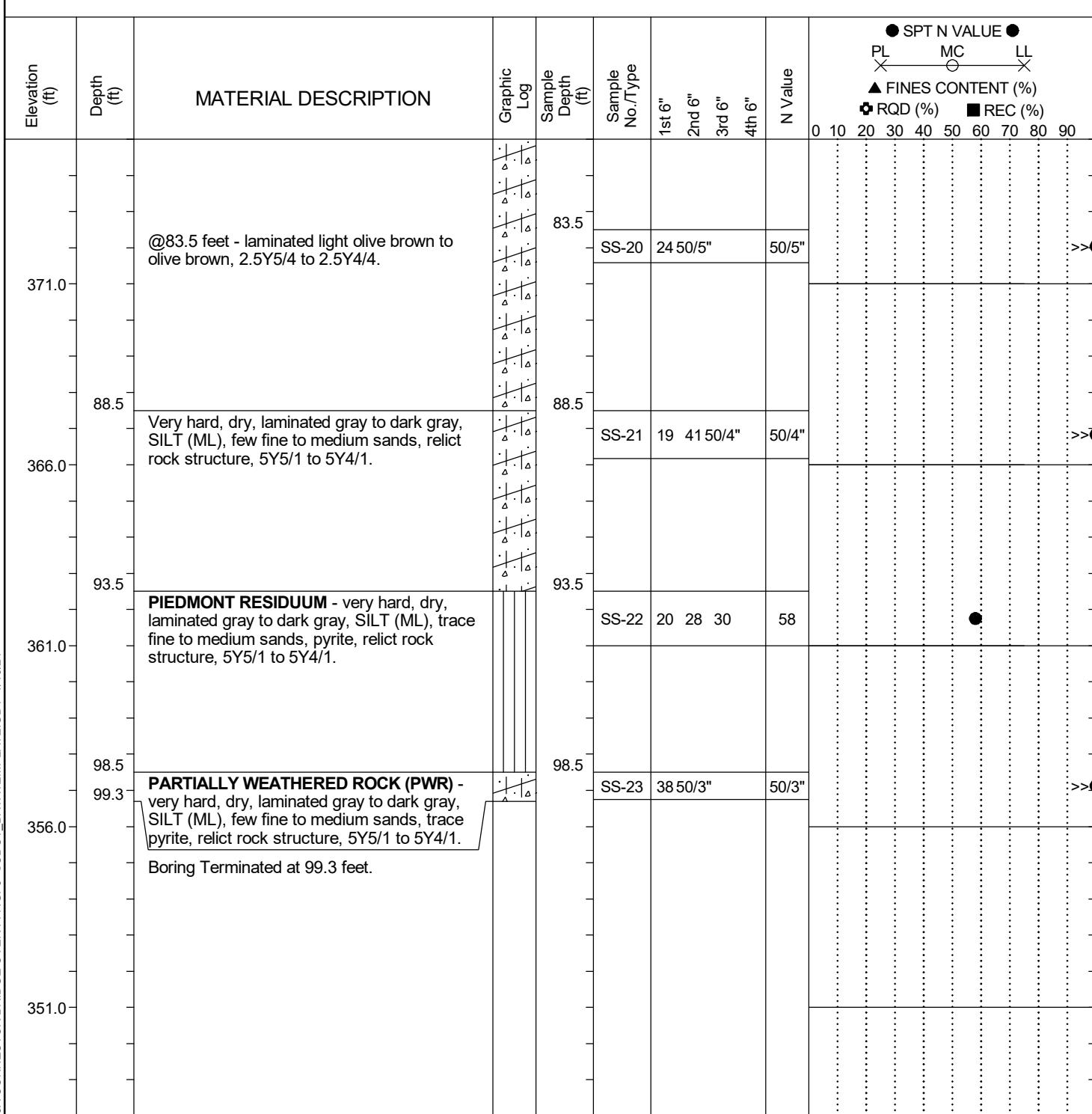
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



Soil Test Log

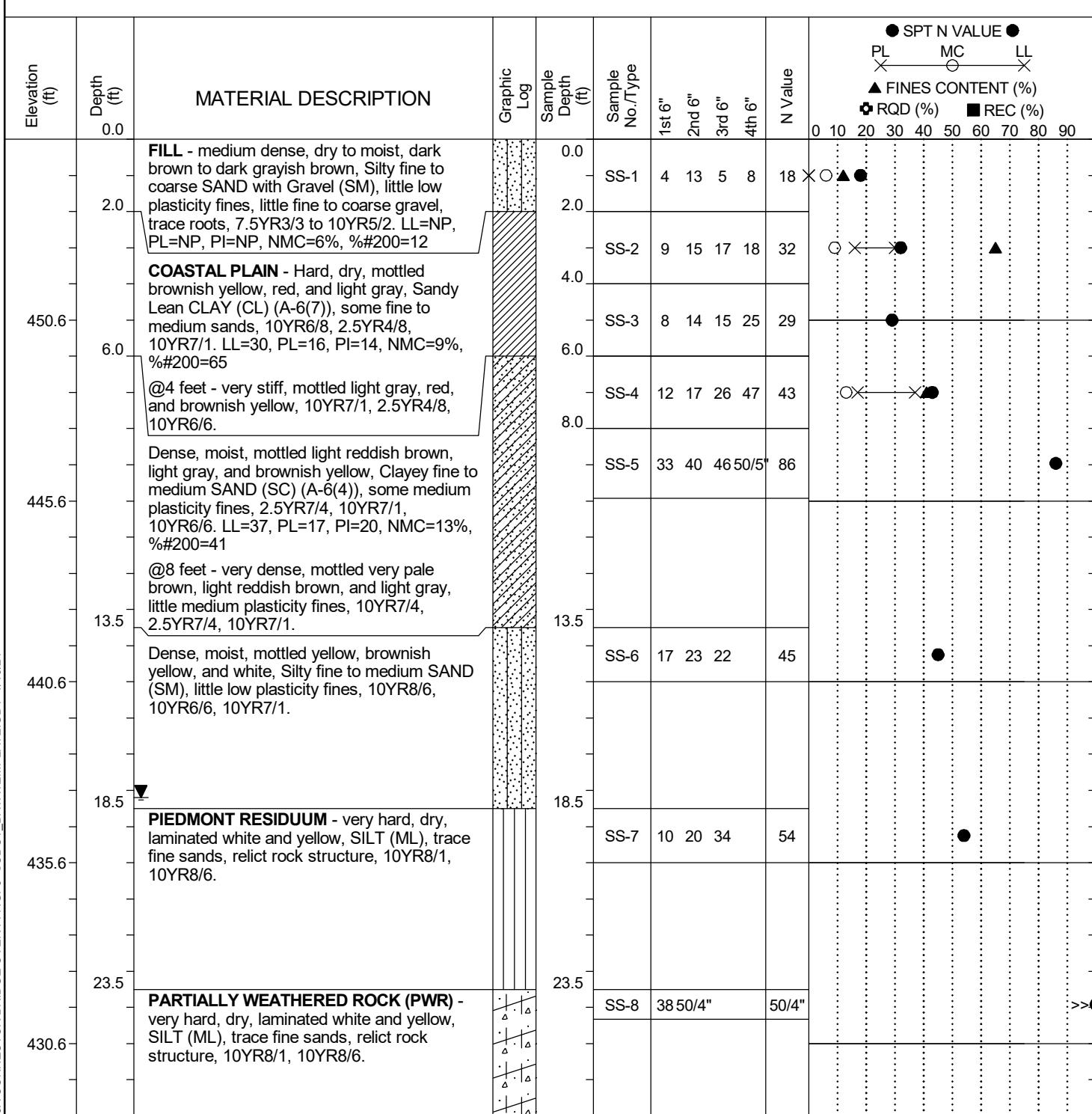
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Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+67.50		Offset:	-7.4	Alignment:	Proposed
Elev.:	456.0 ft	Latitude:	34.19111364		Longitude:	-80.98388809	Date Started:	11/14/2023
Total Depth:	99.3 ft	Soil Depth:	99.3 ft		Core Depth:	N/A ft	Date Completed:	11/14/2023
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW		Hammer Type:	Automatic	Energy Ratio:	87.6%
Core Size:	N/A	Driller:	S. Eubanks		Groundwater:	TOB	N/A	24HR



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 6C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+68.45	Offset:	35.5	Alignment:	Proposed	
Elev.:	455.6 ft	Latitude:	34.191002104	Longitude:	-80.98384144	Date Started:	11/13/2023	
Total Depth:	100 ft	Soil Depth:	100 ft	Core Depth:	N/A ft	Date Completed:	11/13/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	18.2 ft

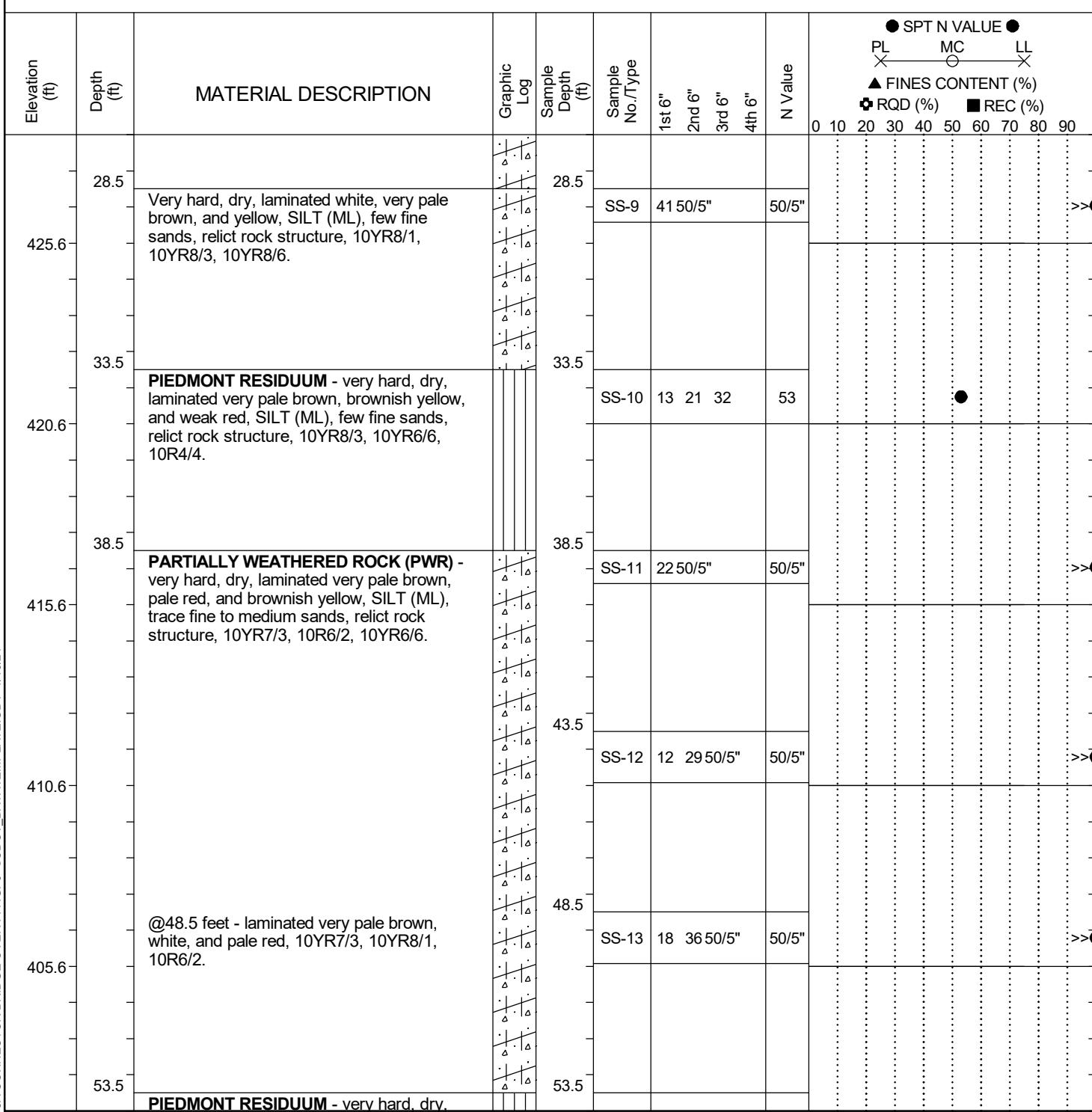


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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 6C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+68.45	Offset:	35.5	Alignment:	Proposed	
Elev.:	455.6 ft	Latitude:	34.191002104	Longitude:	-80.98384144	Date Started:	11/13/2023	
Total Depth:	100 ft	Soil Depth:	100 ft	Core Depth:	N/A ft	Date Completed:	11/13/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	18.2 ft



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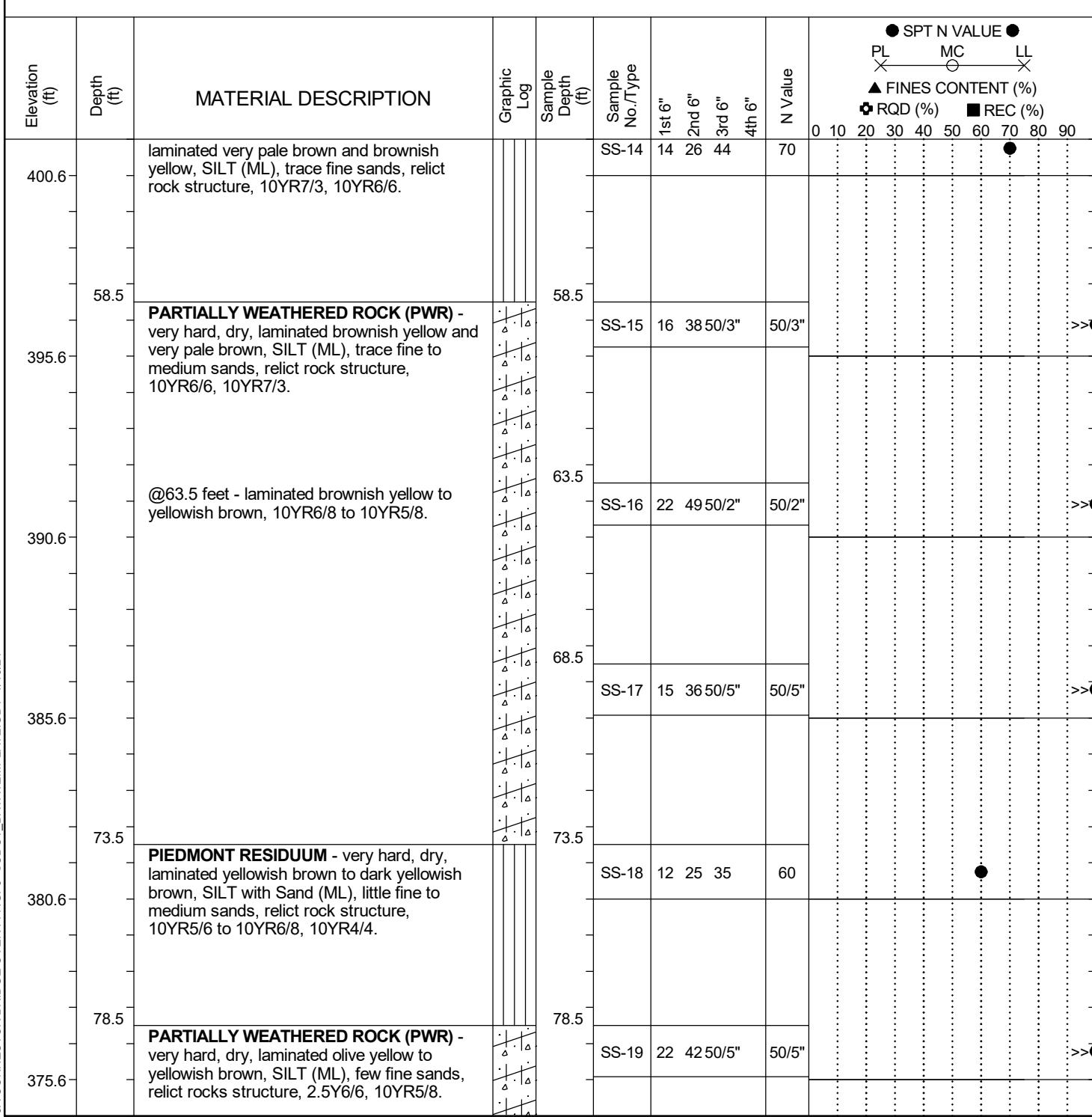
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



Soil Test Log

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 6C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+68.45	Offset:	35.5	Alignment:	Proposed	
Elev.:	455.6 ft	Latitude:	34.191002104	Longitude:	-80.98384144	Date Started:	11/13/2023	
Total Depth:	100 ft	Soil Depth:	100 ft	Core Depth:	N/A ft	Date Completed:	11/13/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	18.2 ft



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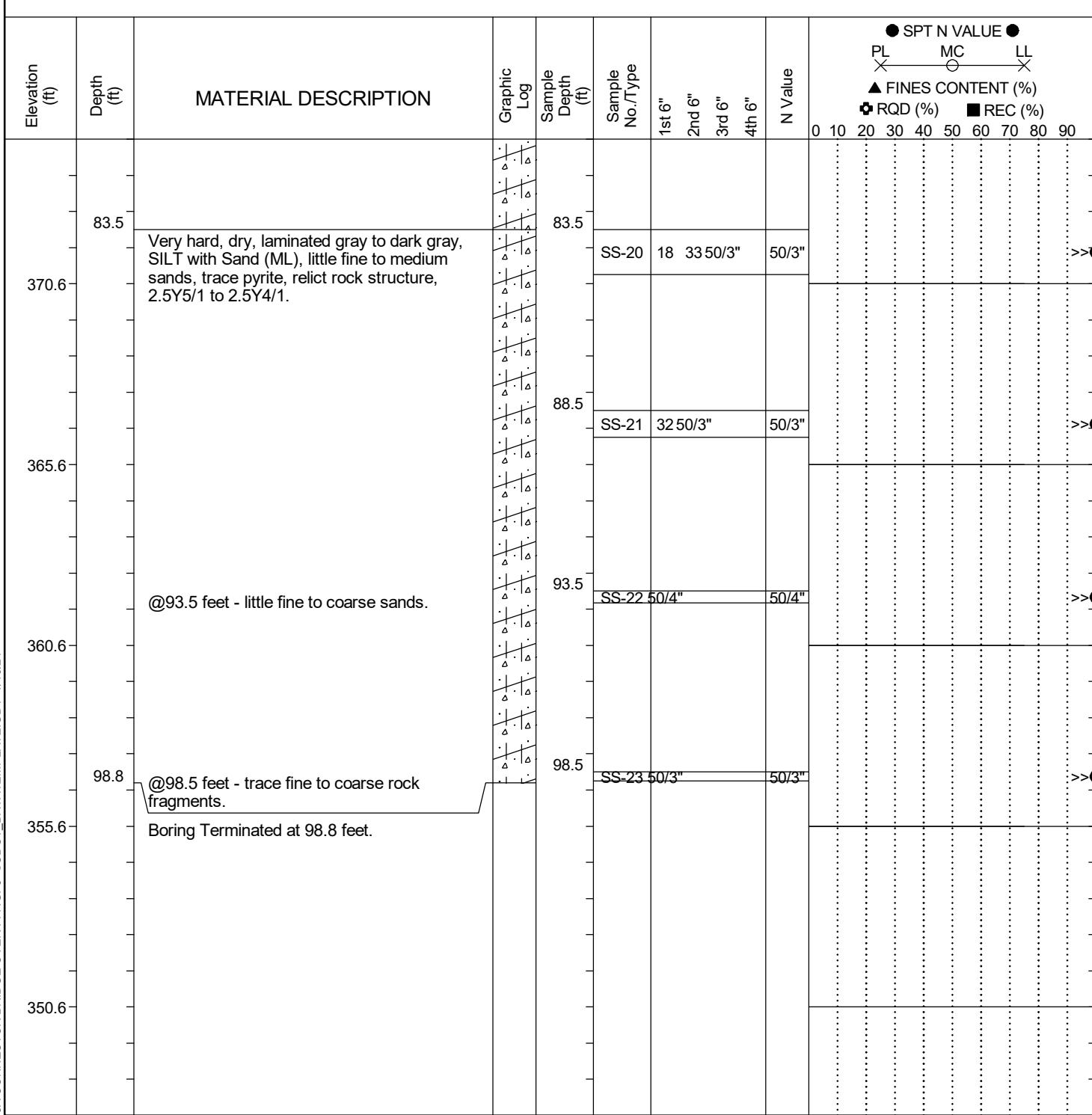
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



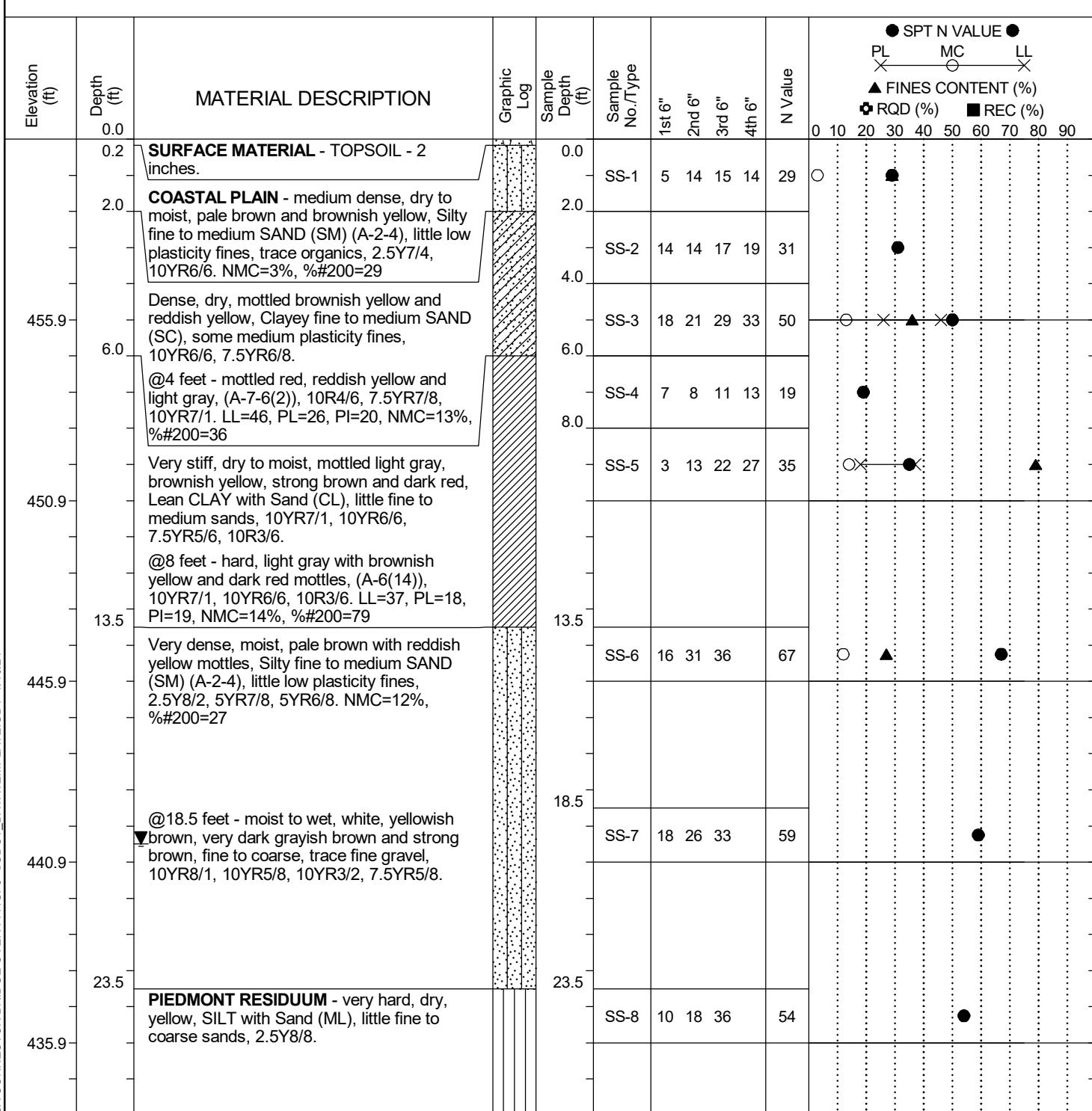
Soil Test Log

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 6C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+68.45	Offset:	35.5	Alignment:	Proposed	
Elev.:	455.6 ft	Latitude:	34.191002104	Longitude:	-80.98384144	Date Started:	11/13/2023	
Total Depth:	100 ft	Soil Depth:	100 ft	Core Depth:	N/A ft	Date Completed:	11/13/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y <input checked="" type="checkbox"/>	N <input type="checkbox"/>	Liner Used:	Y <input checked="" type="checkbox"/>
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	18.2 ft



SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

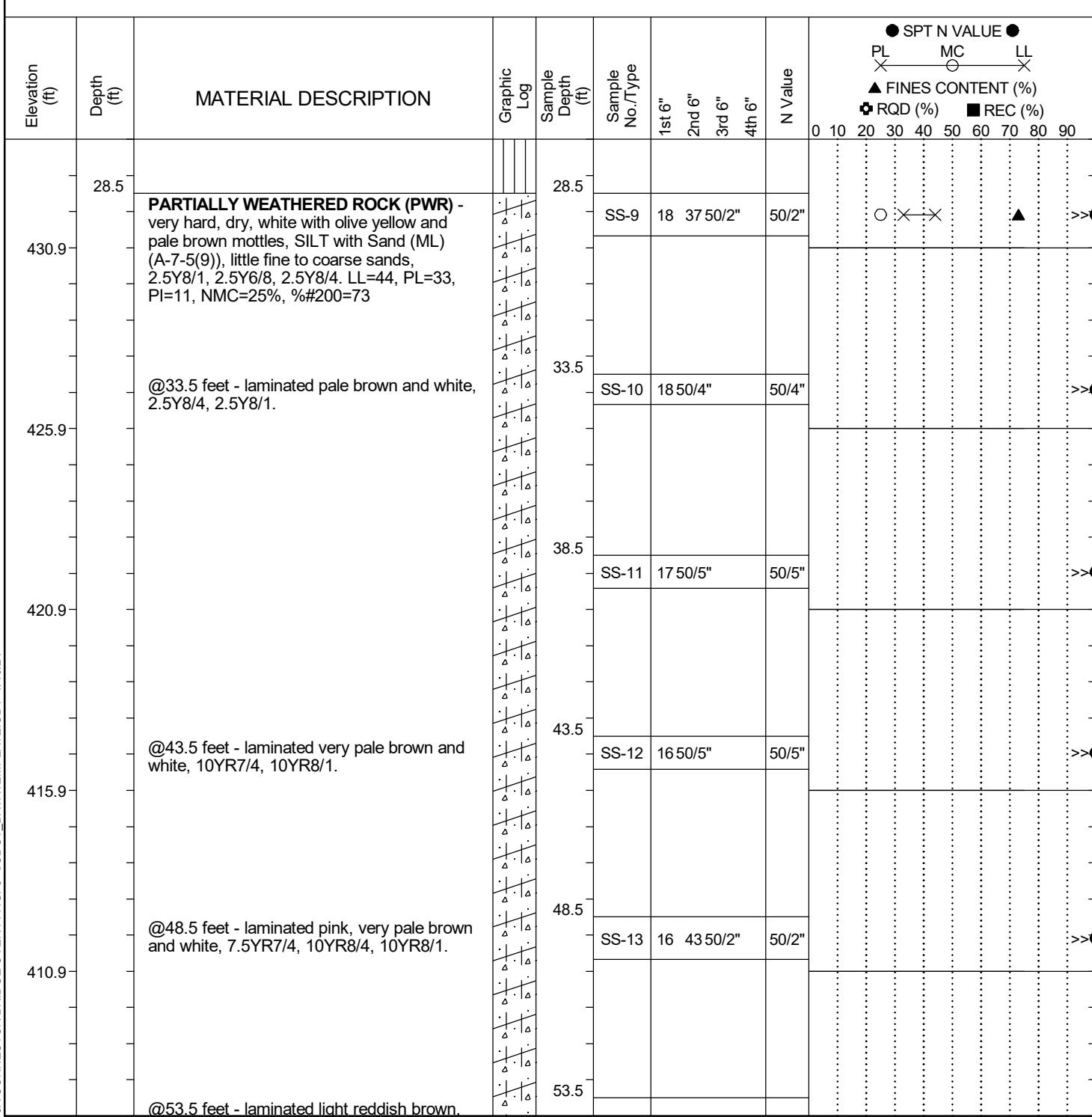
Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 7C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks	Boring Location:	147+14.80	Offset:	-48.9	Alignment:	Proposed	
Elev.:	460.9 ft	Latitude:	34.191177457	Longitude:	-80.98409601	Date Started:	10/18/2023	
Total Depth:	98.7 ft	Soil Depth:	98.7 ft	Core Depth:	N/A ft	Date Completed:	10/18/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	19.5 ft



LEGEND

Continued Next Page

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 7C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+14.80	Offset:	-48.9	Alignment:	Proposed
Elev.:	460.9 ft		Latitude:	34.191177457	Longitude:	-80.98409601	Date Started:	10/18/2023
Total Depth:	98.7 ft	Soil Depth:	98.7 ft	Core Depth:	N/A ft	Date Completed:	10/18/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic		Energy Ratio:	91.6%
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	19.5 ft

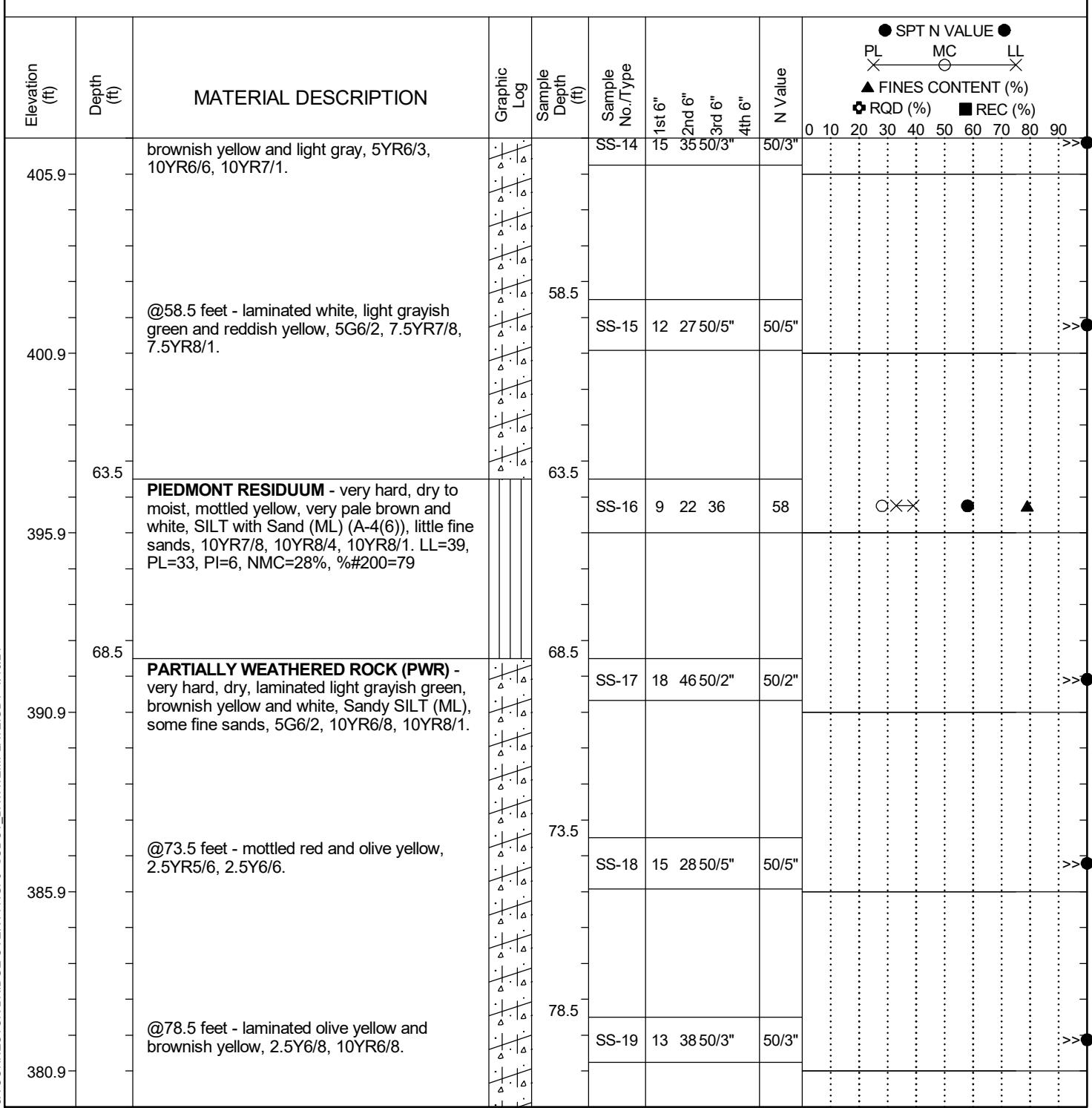


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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 7C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+14.80	Offset:	-48.9	Alignment:	Proposed
Elev.:	460.9 ft		Latitude:	34.191177457	Longitude:	-80.98409601	Date Started:	10/18/2023
Total Depth:	98.7 ft	Soil Depth:	98.7 ft	Core Depth:	N/A ft	Date Completed:	10/18/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:		
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	19.5 ft



LEGEND

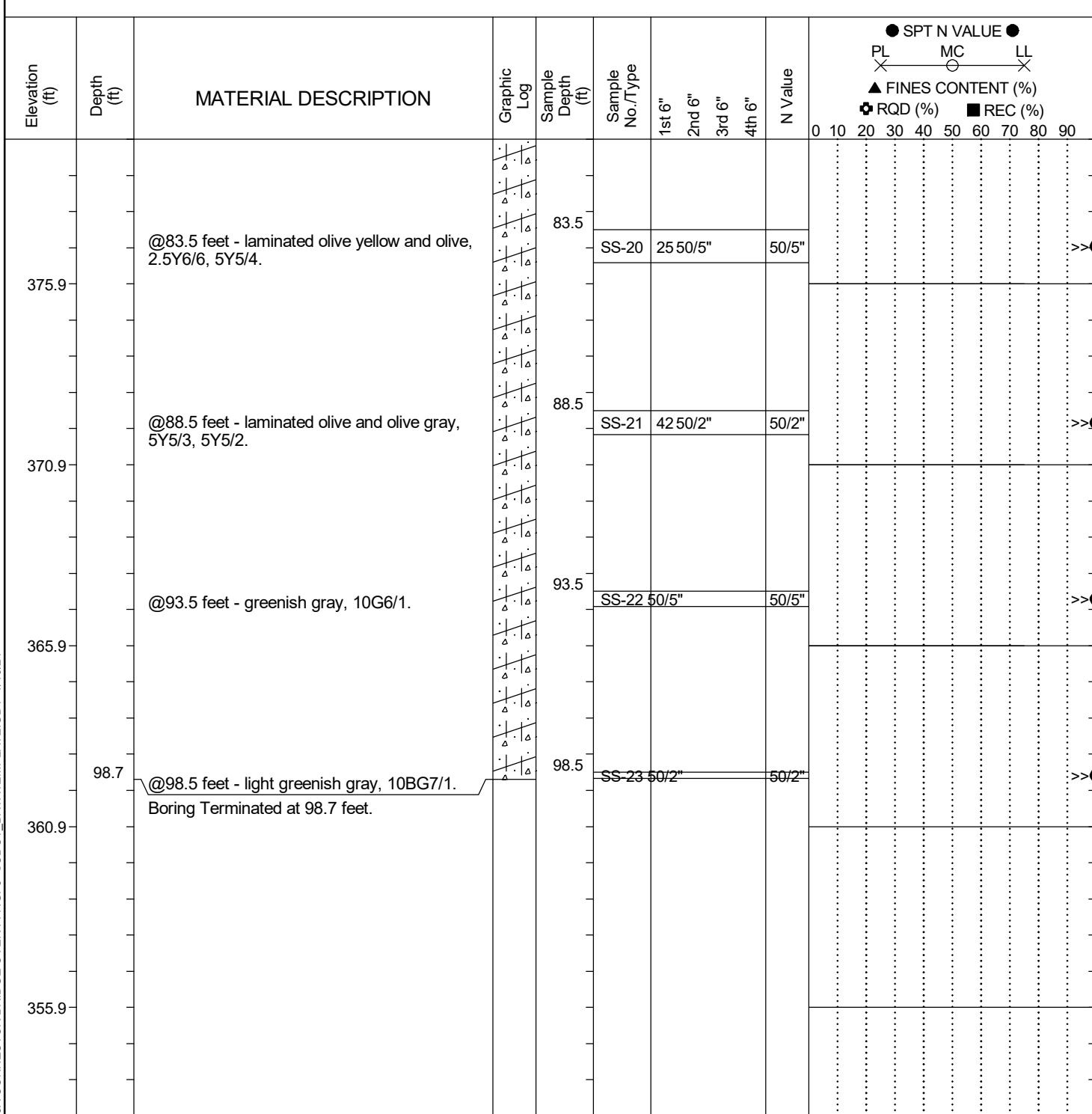
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



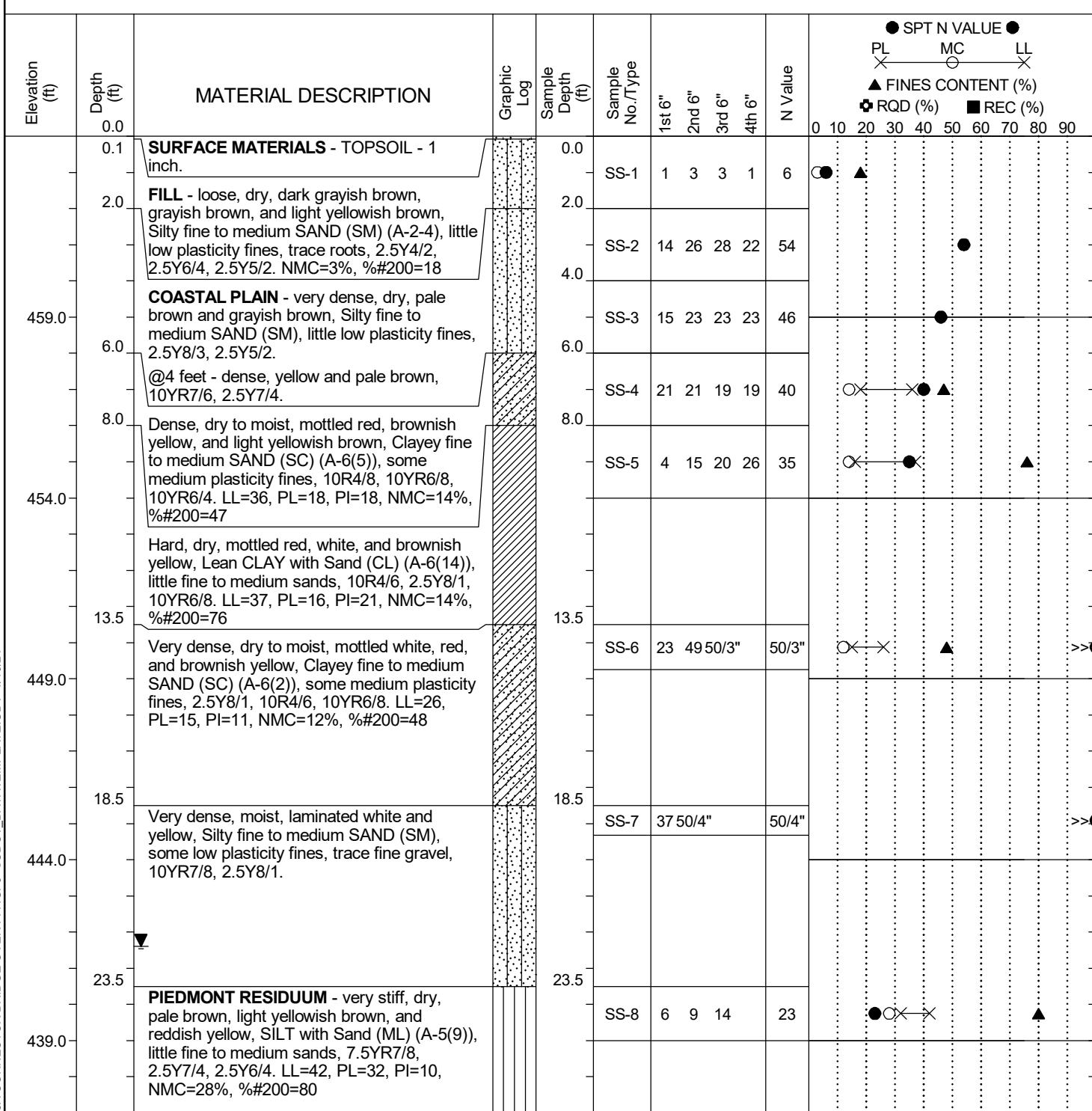
Soil Test Log

Project ID:	P042443 (S&ME 23610178A)		County:	Richland		Boring No.:	IB- 7C
Site Description:	I-77 Exit 26 Phase I					Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+14.80	Offset:	-48.9	Alignment:
Elev.:	460.9 ft	Latitude:	34.191177457	Longitude:	-80.98409601	Date Started:	10/18/2023
Total Depth:	98.7 ft	Soil Depth:	98.7 ft	Core Depth:	N/A ft	Date Completed:	10/18/2023
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR



SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 8C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+17.23		Offset:	7.7	Alignment:
Elev.:	464.0 ft		Latitude:	34.19103167		Longitude:	-80.98403094	Date Started:
Total Depth:	99.2 ft		Soil Depth:	99.2 ft		Core Depth:	N/A ft	Date Completed:
Bore Hole Diameter (in):	4		Sampler Configuration		Liner Required:	Y	(N)	Liner Used:
Drill Machine:	CME-550X		Drill Method:	RW		Hammer Type:	Automatic	Energy Ratio:
Core Size:	N/A		Driller:	L. Shrader		Groundwater:	TOB	N/A
							24HR	22.4 ft

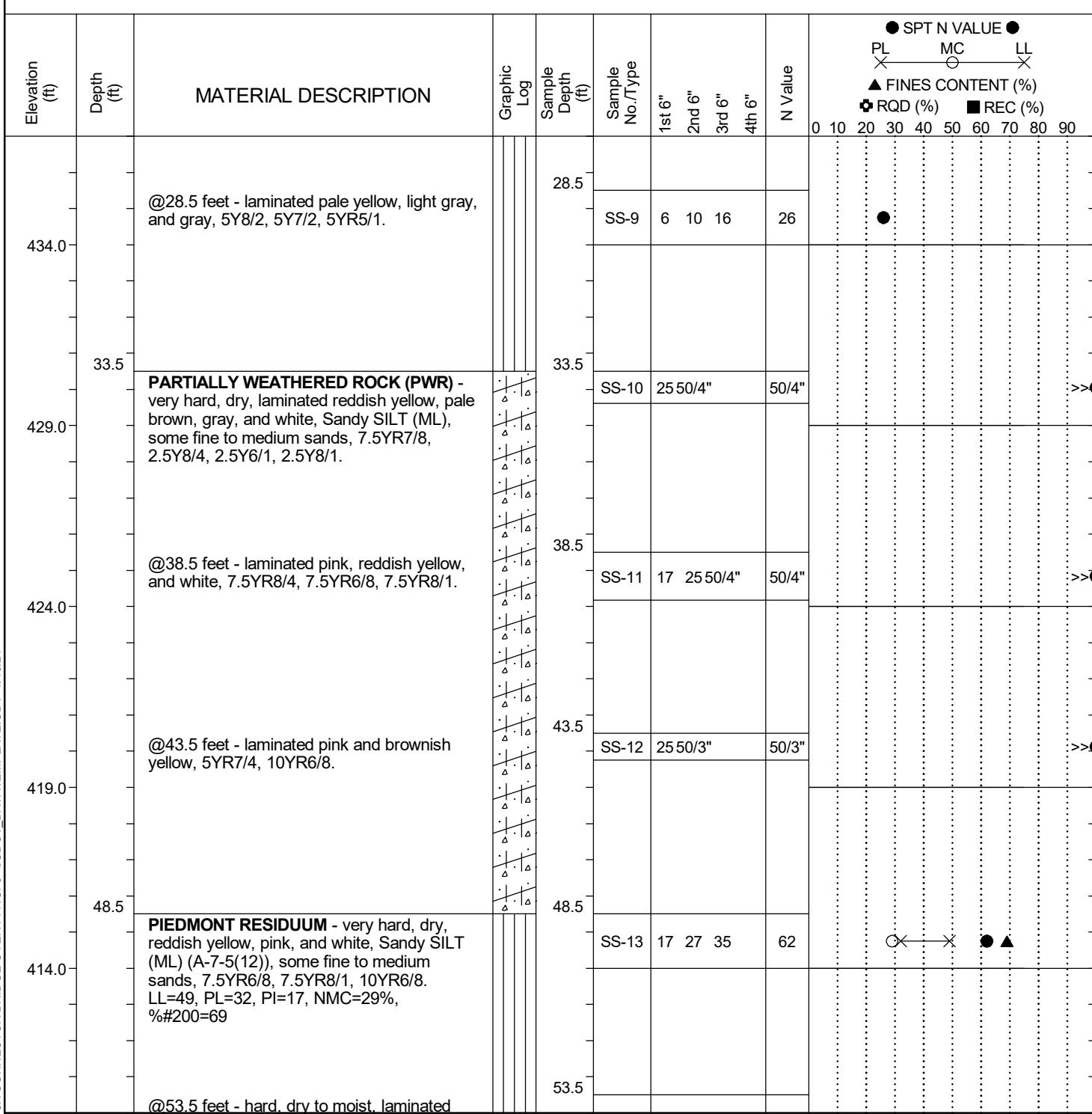


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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	CU - Cuttings	HSA - Hollow Stem Auger	RW - Rotary Wash	CFA - Continuous Flight Augers	RC - Rock Core	DC - Driving Casing
UD - Undisturbed Sample							
AWG - Rock Core, 1-1/8"		CT - Continuous Tube					

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 8C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+17.23		Offset:	7.7	Alignment:
Elev.:	464.0 ft		Latitude:	34.19103167		Longitude:	-80.98403094	Date Started:
Total Depth:	99.2 ft		Soil Depth:	99.2 ft		Core Depth:	N/A ft	Date Completed:
Bore Hole Diameter (in):	4		Sampler Configuration		Liner Required:	Y	(N)	Liner Used:
Drill Machine:	CME-550X		Drill Method:	RW		Hammer Type:	Automatic	Energy Ratio:
Core Size:	N/A		Driller:	L. Shrader		Groundwater:	TOB	N/A
							24HR	22.4 ft

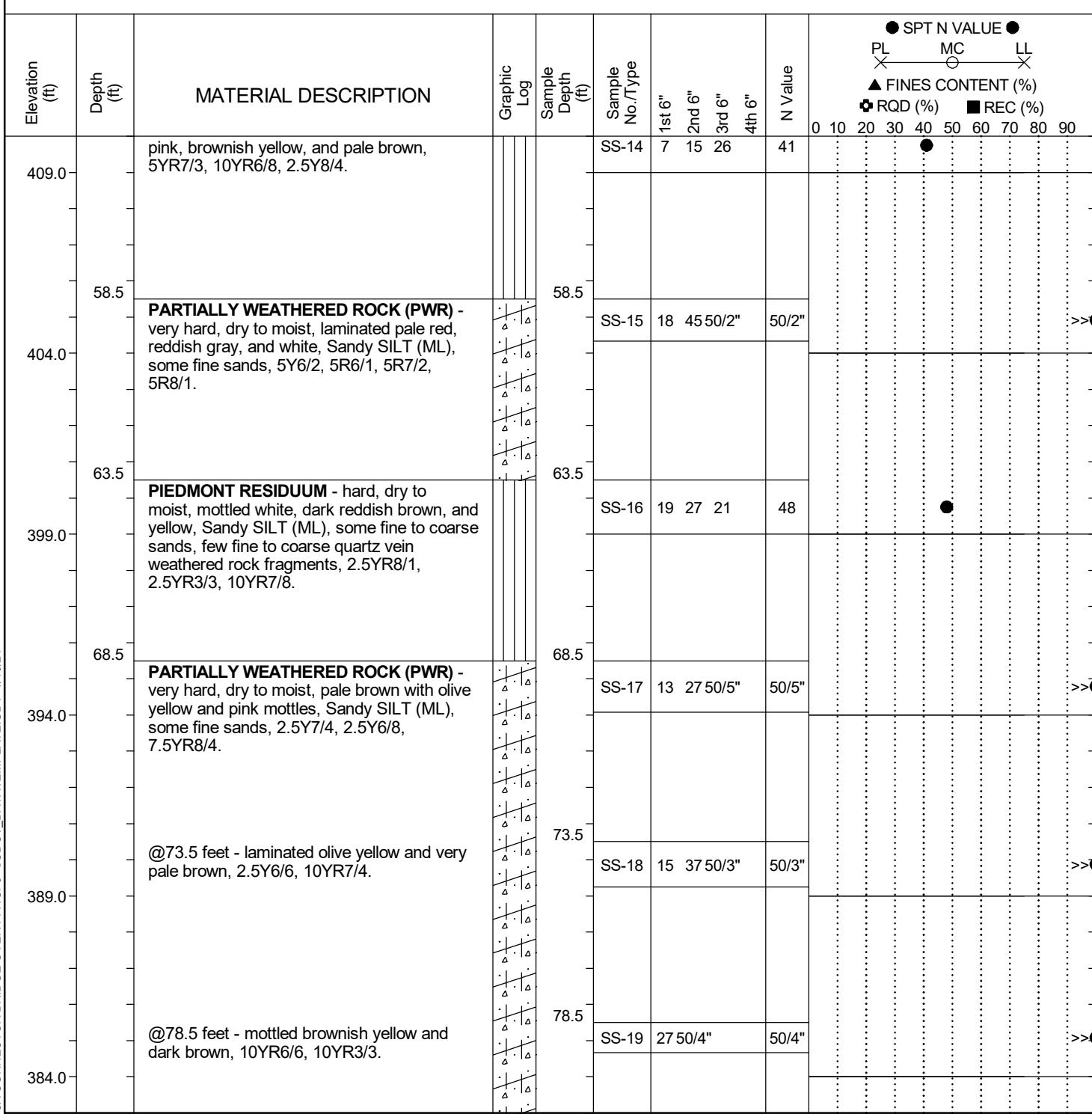


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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	UD - Undisturbed Sample	CU - Cuttings	HSA - Hollow Stem Auger	RW - Rotary Wash	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube			DC - Driving Casing			

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 8C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+17.23	Offset:	7.7	Alignment:	Proposed
Elev.:	464.0 ft		Latitude:	34.19103167	Longitude:	-80.98403094	Date Started:	10/19/23
Total Depth:	99.2 ft	Soil Depth:	99.2 ft	Core Depth:	N/A ft	Date Completed:		10/19/2023
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:		91.6%
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	22.4 ft



LEGEND

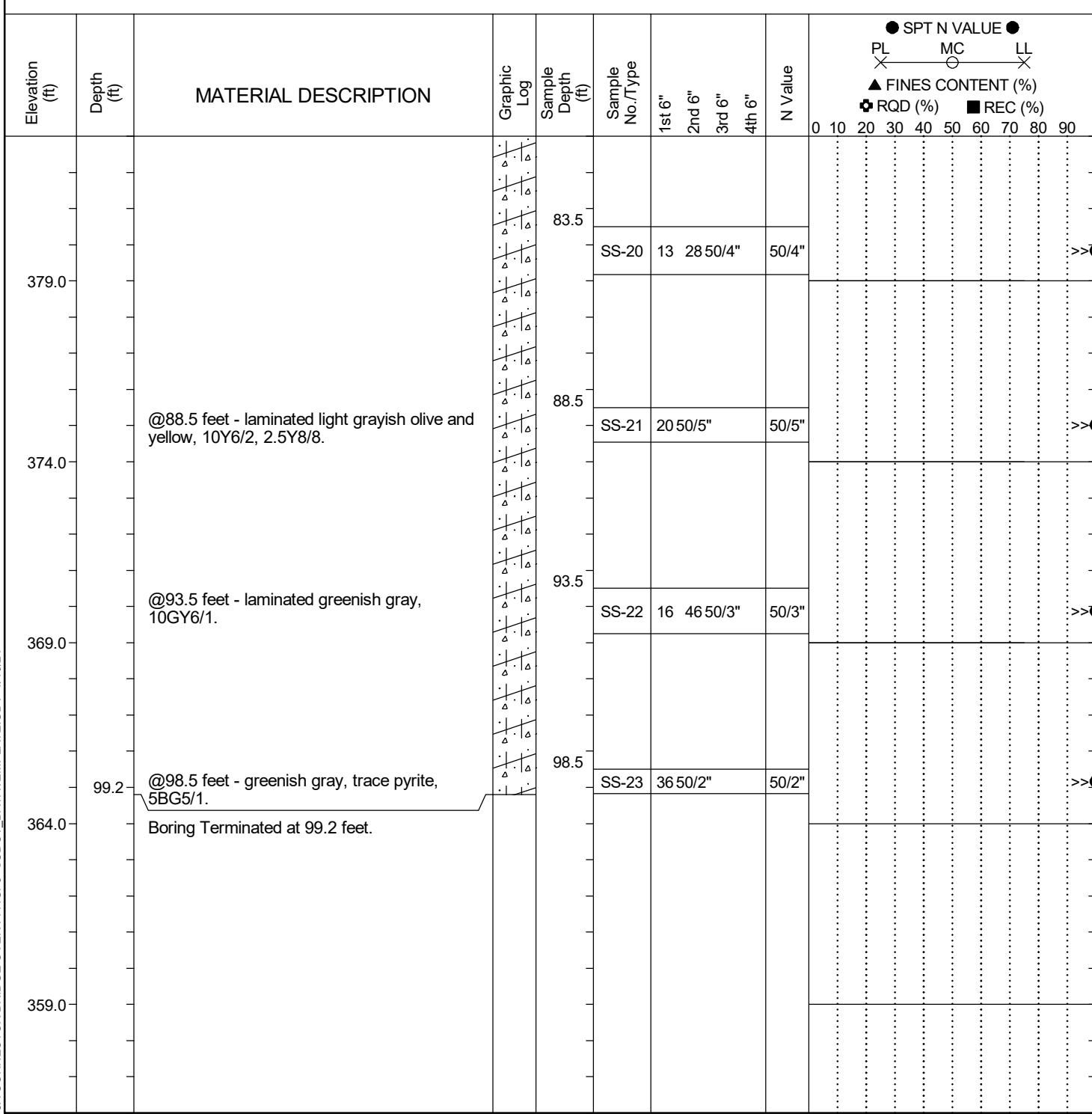
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



Soil Test Log

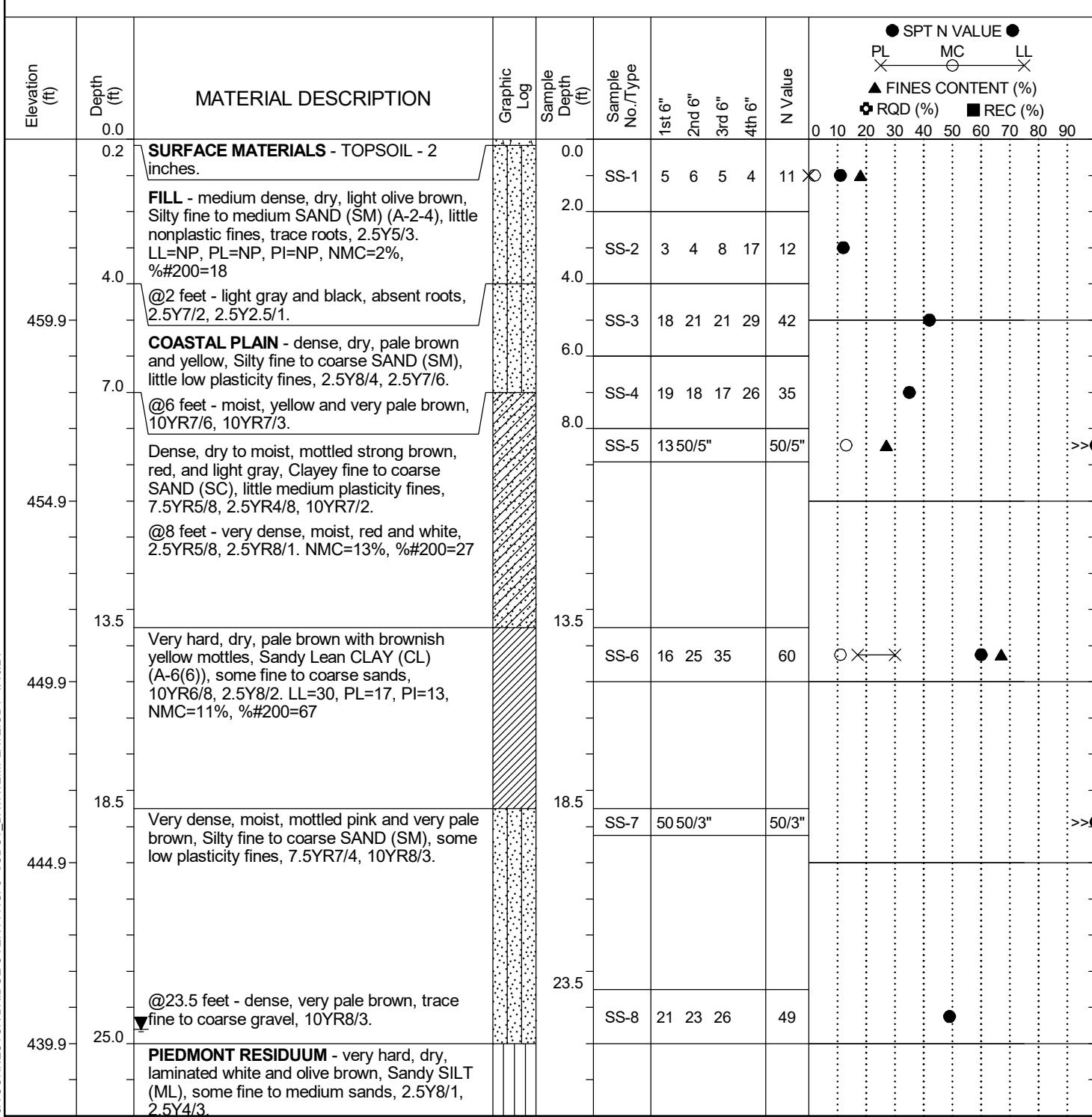
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Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+17.23	Offset:	7.7	Alignment:	Proposed
Elev.:	464.0 ft		Latitude:	34.19103167	Longitude:	-80.98403094	Date Started:	10/19/23
Total Depth:	99.2 ft	Soil Depth:	99.2 ft	Core Depth:	N/A ft	Date Completed:		10/19/2023
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:		91.6%
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	22.4 ft



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland			Boring No.:	IB- 9C	
Site Description:	I-77 Exit 26 Phase I							Route:	Connector Rd	
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+19.17		Offset:	57.5		Alignment:	Proposed
Elev.:	464.9 ft		Latitude:	34.190903077		Longitude:	-80.98397419		Date Started:	10/23/2023
Total Depth:	99.3 ft		Soil Depth:	99.3 ft		Core Depth:	N/A ft		Date Completed:	10/24/2023
Bore Hole Diameter (in):	4		Sampler Configuration		Liner Required:		Y	N	Liner Used:	Y N
Drill Machine:	CME-550X		Drill Method:	RW		Hammer Type:	Automatic		Energy Ratio:	91.6%
Core Size:	N/A		Driller:	L. Shrader		Groundwater:	TOB	N/A	24HR	24.6 ft

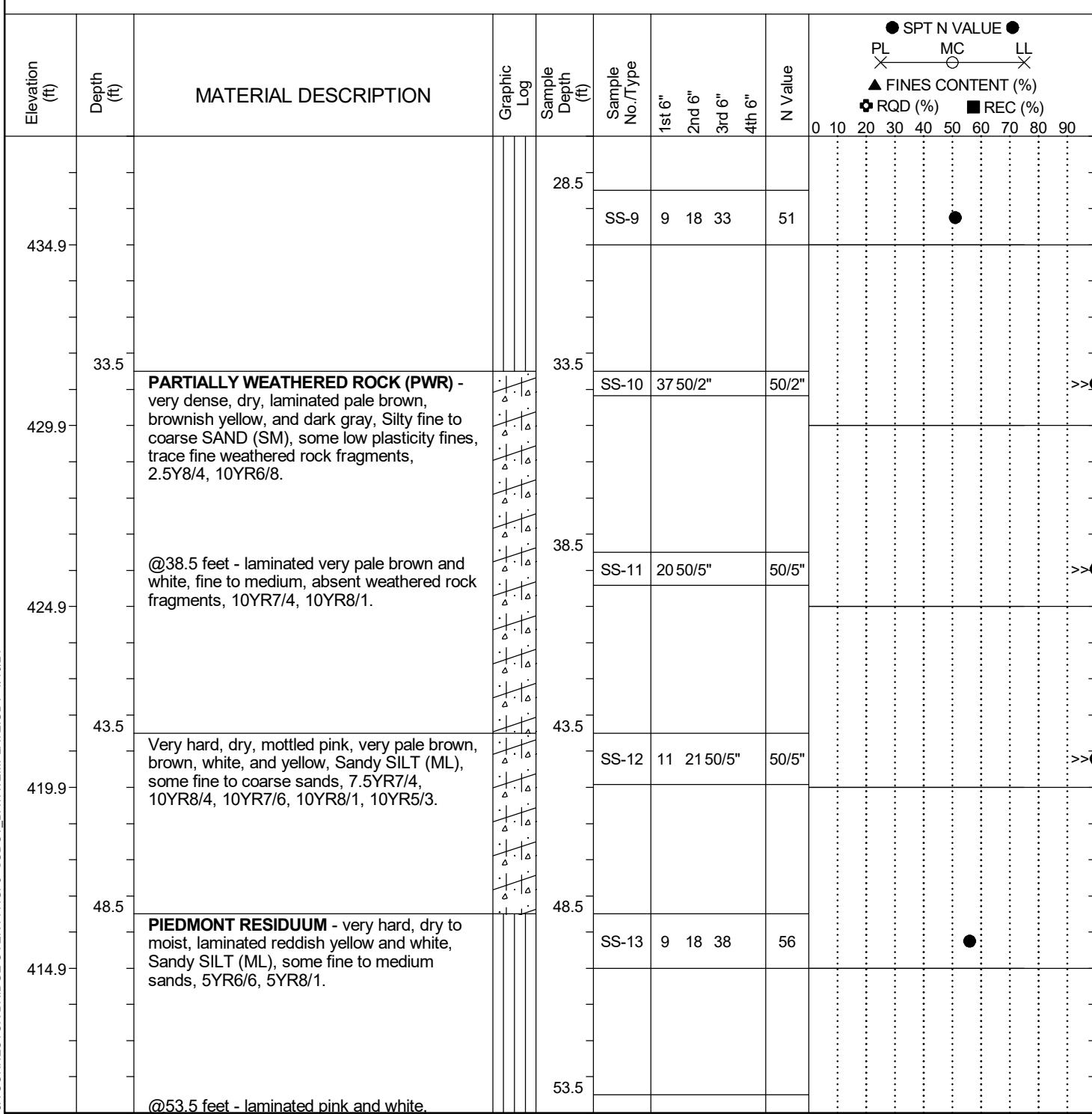


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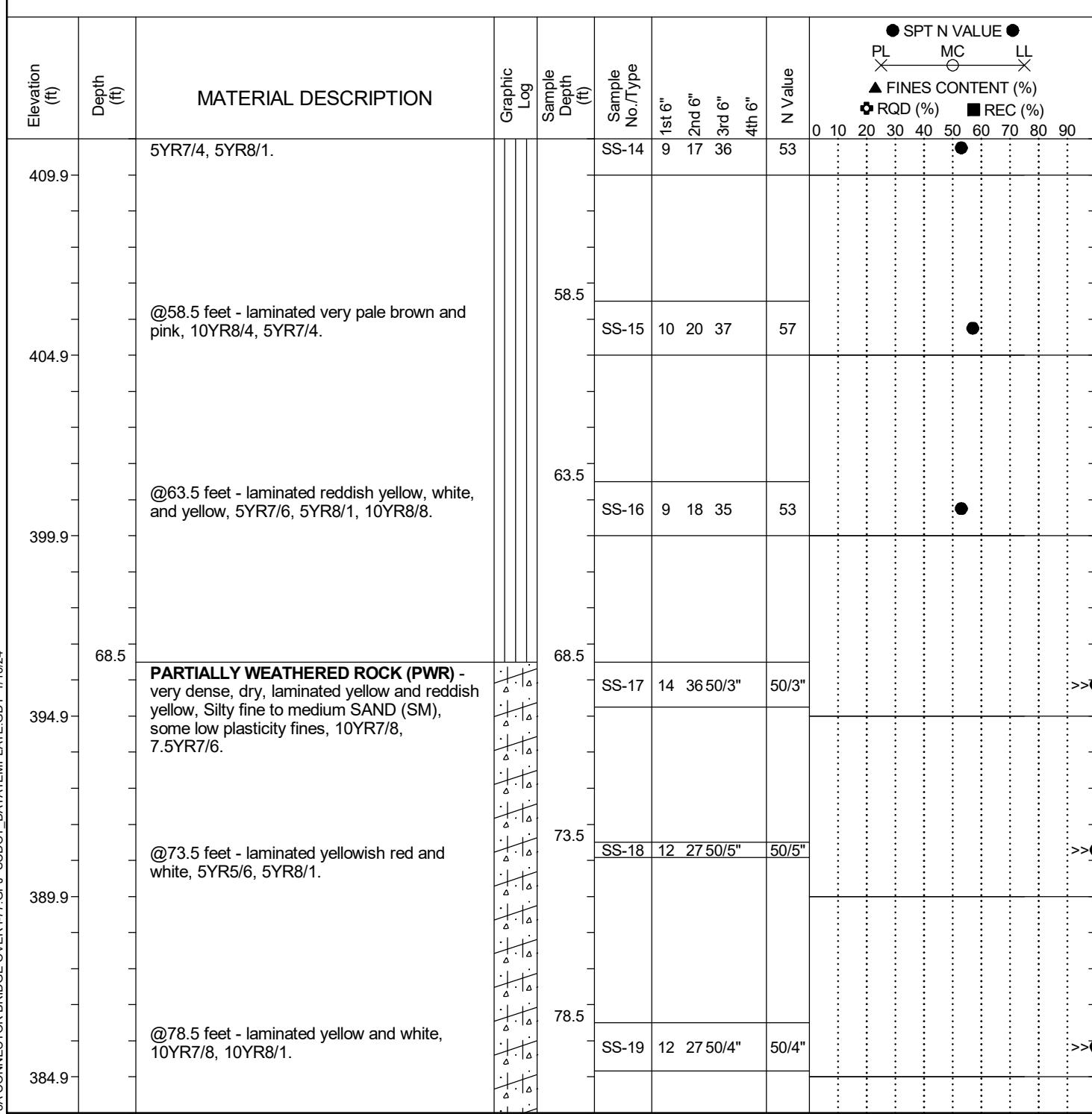
SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	CU - Cuttings	HSA - Hollow Stem Auger	RW - Rotary Wash	CFA - Continuous Flight Augers	RC - Rock Core	AWG - Rock Core, 1-1/8"
UD - Undisturbed Sample	CT - Continuous Tube	DC - Driving Casing					
AWG - Rock Core, 1-1/8"							

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 9C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+19.17	Offset:	57.5	Alignment:	Proposed
Elev.:	464.9 ft	Latitude:	34.190903077	Longitude:	-80.98397419	Date Started:	10/23/2023	
Total Depth:	99.3 ft	Soil Depth:	99.3 ft	Core Depth:	N/A ft	Date Completed:	10/24/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y <input checked="" type="checkbox"/>	N <input type="checkbox"/>	Liner Used:	Y <input checked="" type="checkbox"/>
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	24.6 ft



SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 9C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+19.17	Offset:	57.5	Alignment:	Proposed
Elev.:	464.9 ft		Latitude:	34.190903077	Longitude:	-80.98397419	Date Started:	10/23/2023
Total Depth:	99.3 ft	Soil Depth:	99.3 ft	Core Depth:	N/A ft	Date Completed:	10/24/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	24.6 ft

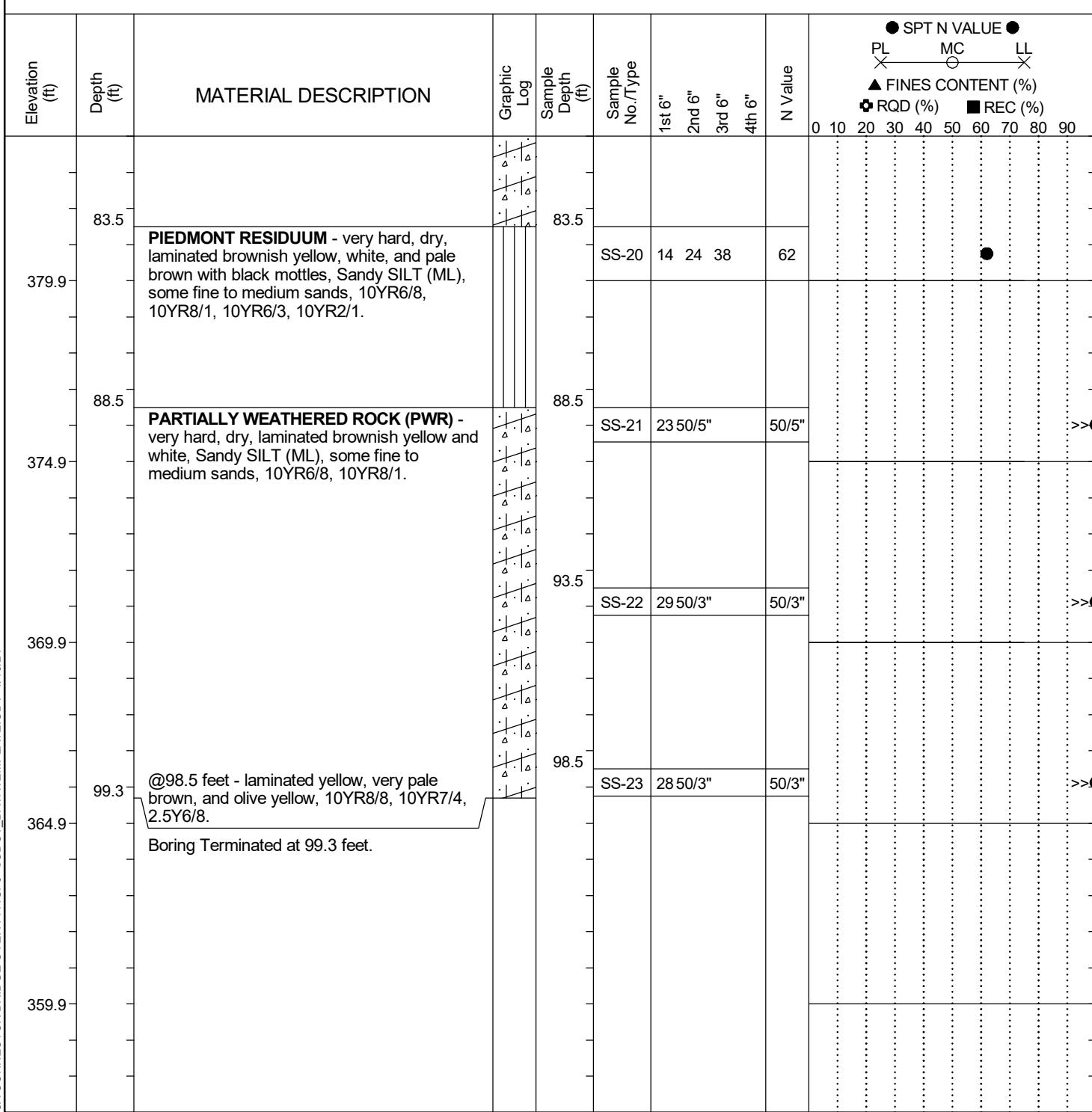


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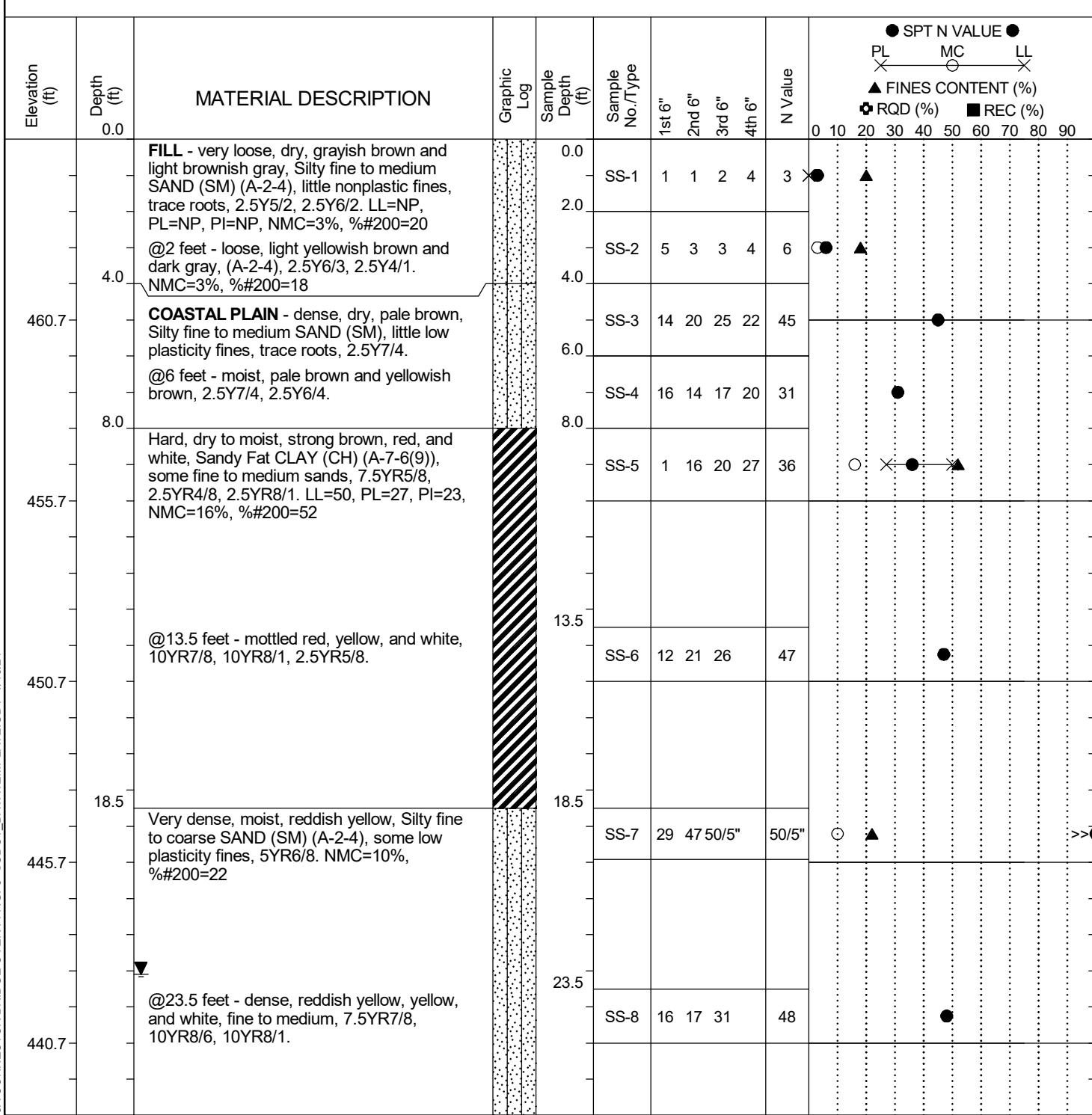
SAMPLER TYPE			DRILLING METHOD		
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UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB- 9C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+19.17	Offset:	57.5	Alignment:	Proposed
Elev.:	464.9 ft		Latitude:	34.190903077	Longitude:	-80.98397419	Date Started:	10/23/2023
Total Depth:	99.3 ft	Soil Depth:	99.3 ft	Core Depth:	N/A ft	Date Completed:	10/24/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic		Energy Ratio:	91.6%
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	24.6 ft

**LEGEND**

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB-10C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+20.10	Offset:	102.7	Alignment:	Proposed
Elev.:	465.7 ft		Latitude:	34.190785679	Longitude:	-80.98392534	Date Started:	10/24/2023
Total Depth:	99.3 ft	Soil Depth:	99.3 ft	Core Depth:	N/A ft	Date Completed:	10/25/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	23.1 ft

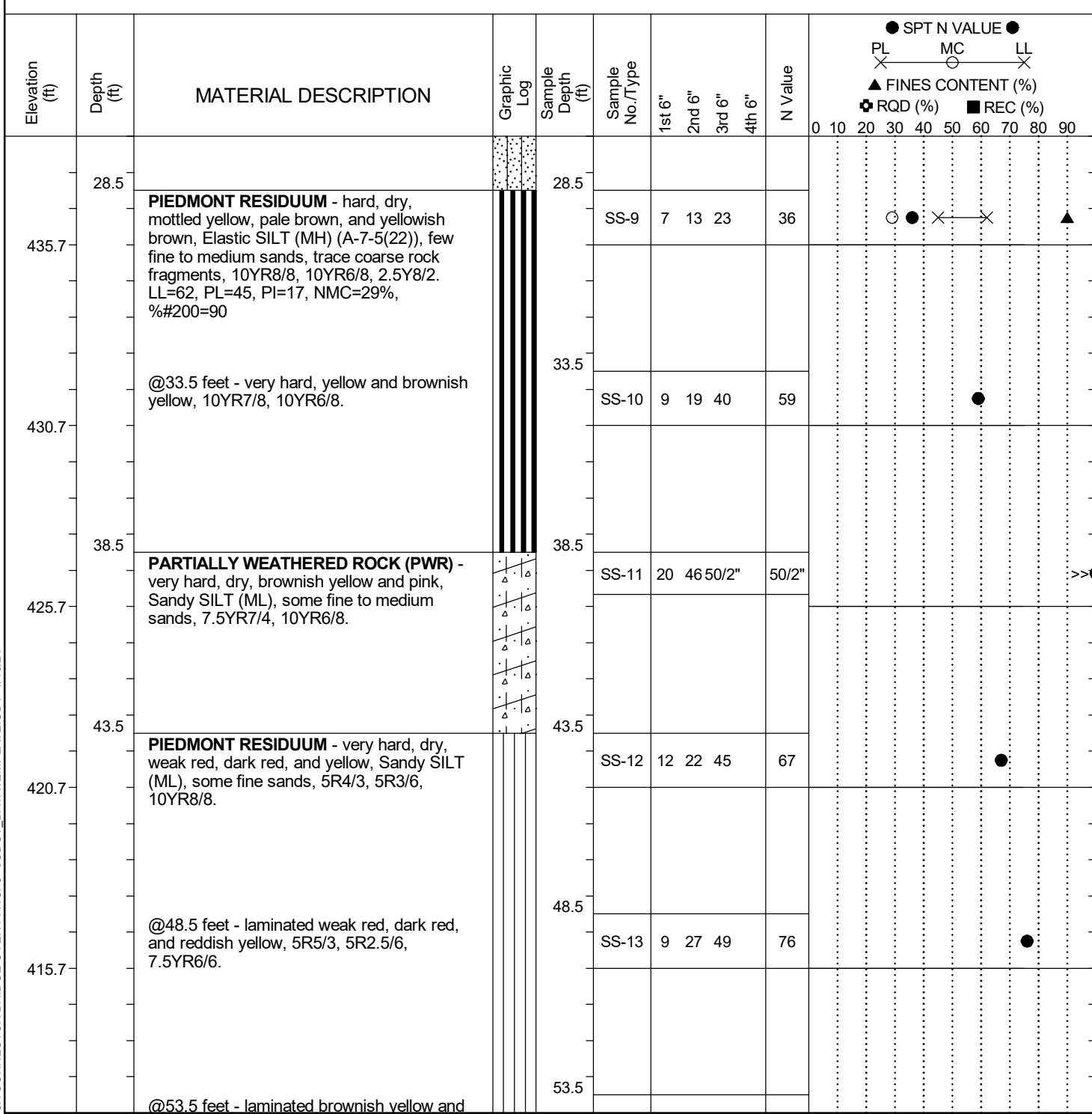


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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB-10C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+20.10	Offset:	102.7	Alignment:	Proposed
Elev.:	465.7 ft		Latitude:	34.190785679	Longitude:	-80.98392534	Date Started:	10/24/2023
Total Depth:	99.3 ft	Soil Depth:	99.3 ft	Core Depth:	N/A ft	Date Completed:	10/25/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	23.1 ft

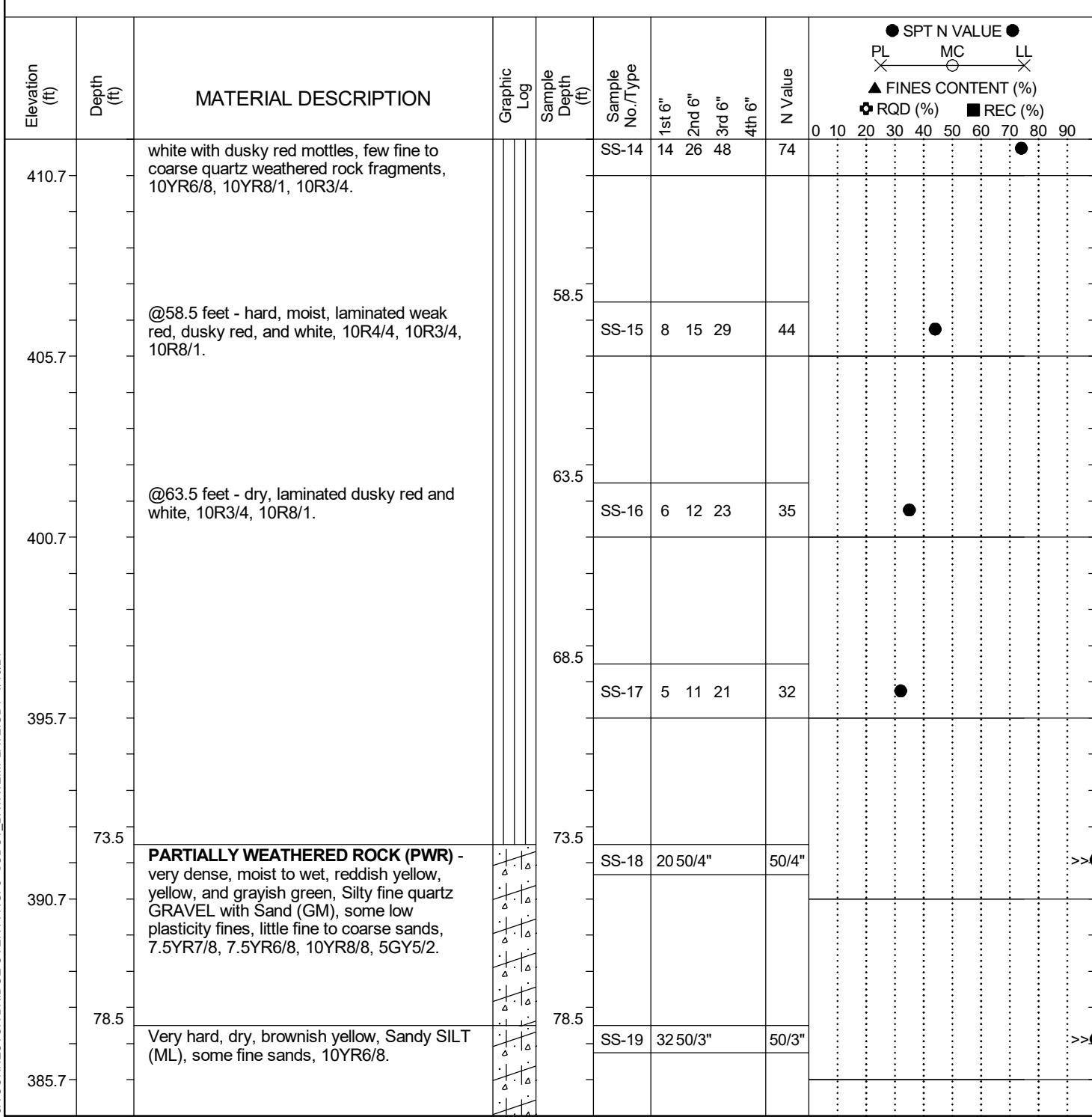


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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash				
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core				
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing					

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB-10C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+20.10	Offset:	102.7	Alignment:	Proposed
Elev.:	465.7 ft		Latitude:	34.190785679	Longitude:	-80.98392534	Date Started:	10/24/2023
Total Depth:	99.3 ft	Soil Depth:	99.3 ft	Core Depth:	N/A ft	Date Completed:	10/25/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	23.1 ft

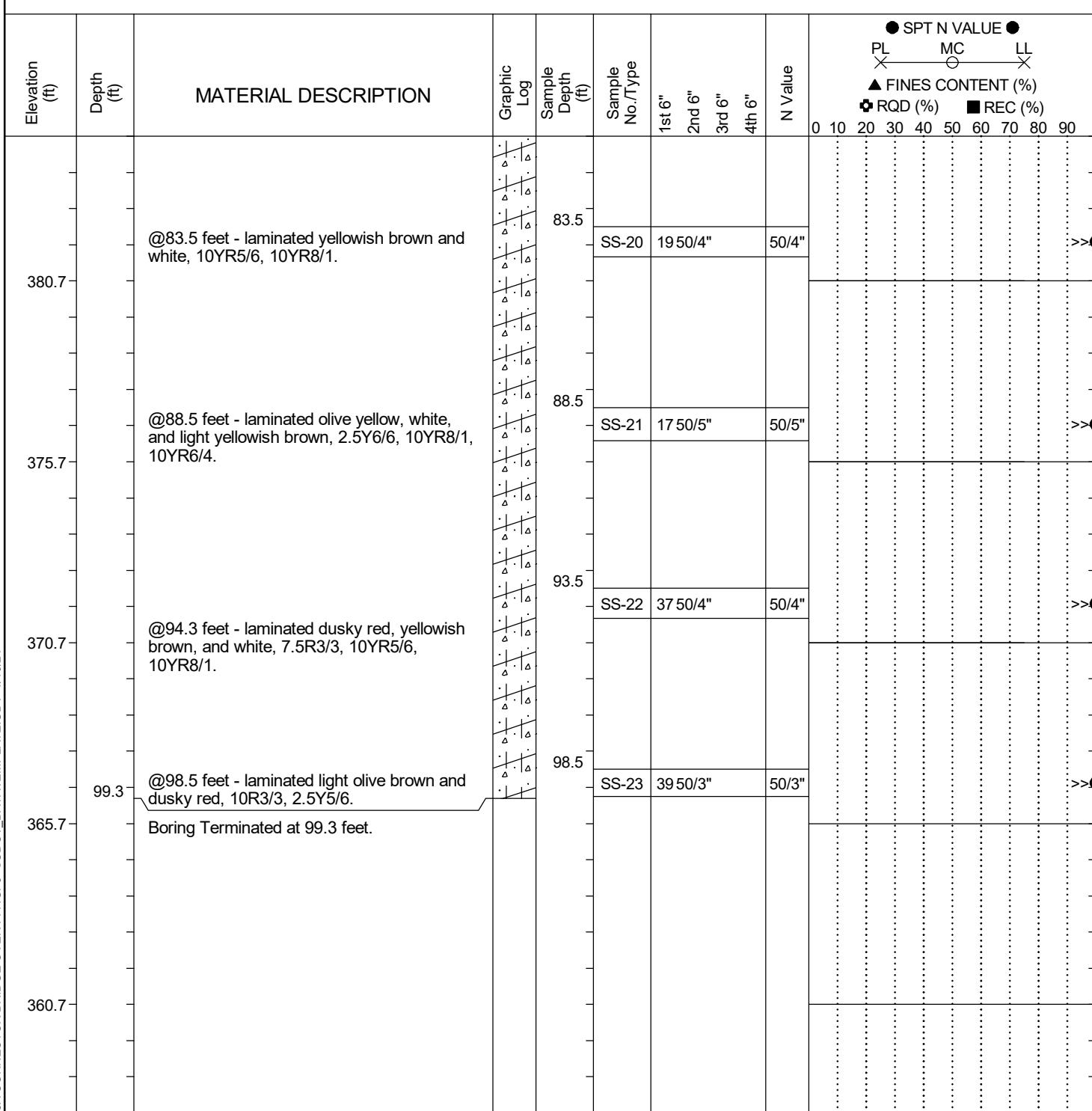


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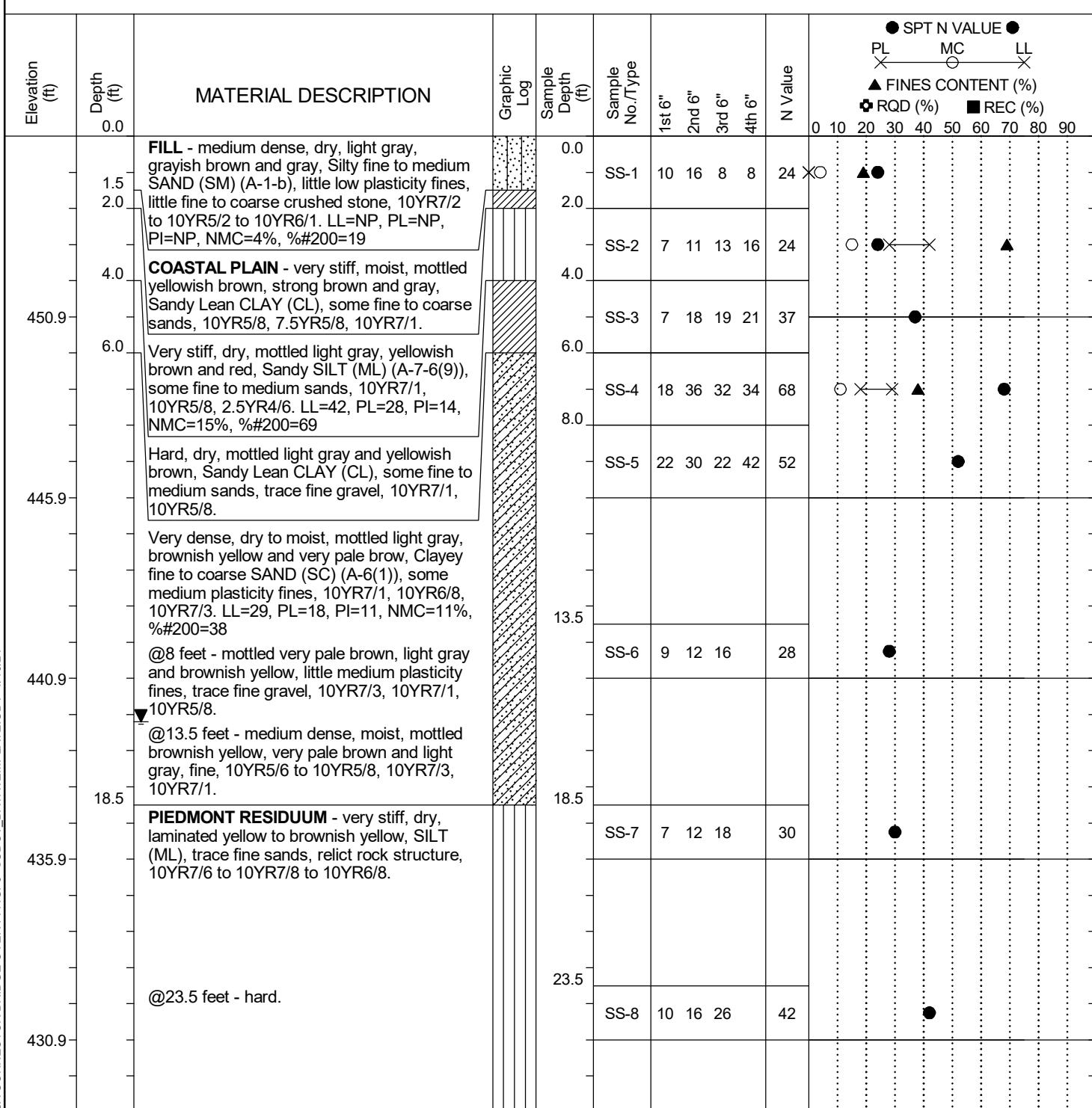
SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)		County:	Richland		Boring No.:	IB-10C	
Site Description:	I-77 Exit 26 Phase I					Route:	Connector Rd	
Eng./Geo.:	E. Eastabrooks		Boring Location:	147+20.10	Offset:	102.7	Alignment:	Proposed
Elev.:	465.7 ft	Latitude:	34.190785679	Longitude:	-80.98392534	Date Started:	10/24/2023	
Total Depth:	99.3 ft	Soil Depth:	99.3 ft	Core Depth:	N/A ft	Date Completed:	10/25/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	23.1 ft

**LEGEND**

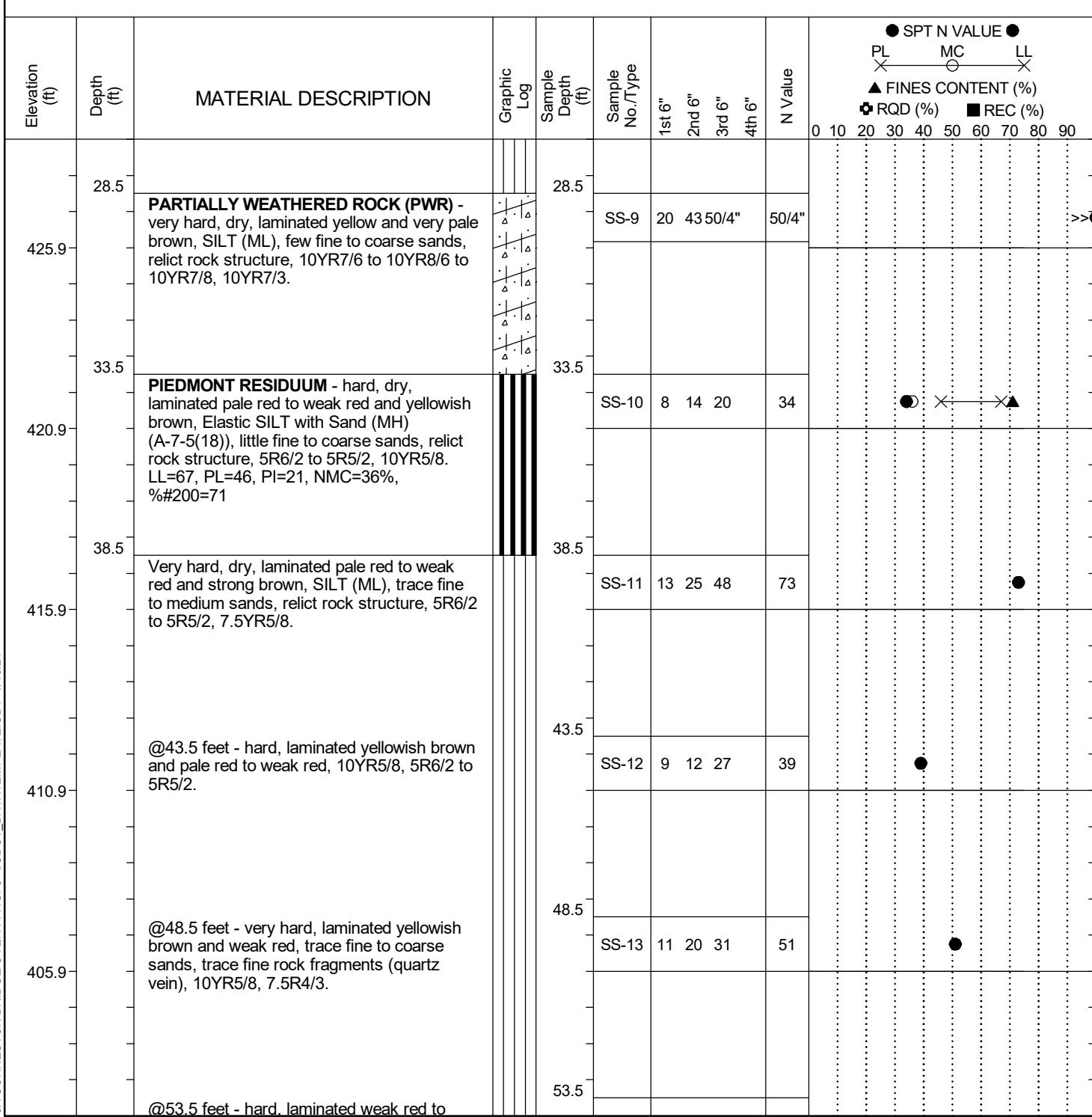
SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB-11C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+67.94	Offset:	113.3	Alignment:	Proposed	
Elev.:	455.9 ft	Latitude:	34.190798359	Longitude:	-80.98376403	Date Started:	11/7/2023	
Total Depth:	99.9 ft	Soil Depth:	99.9 ft	Core Depth:	N/A ft	Date Completed:	11/7/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	16.2 ft



SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash				
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core				
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing					

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB-11C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+67.94	Offset:	113.3	Alignment:	Proposed	
Elev.:	455.9 ft	Latitude:	34.190798359	Longitude:	-80.98376403	Date Started:	11/7/2023	
Total Depth:	99.9 ft	Soil Depth:	99.9 ft	Core Depth:	N/A ft	Date Completed:	11/7/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	16.2 ft

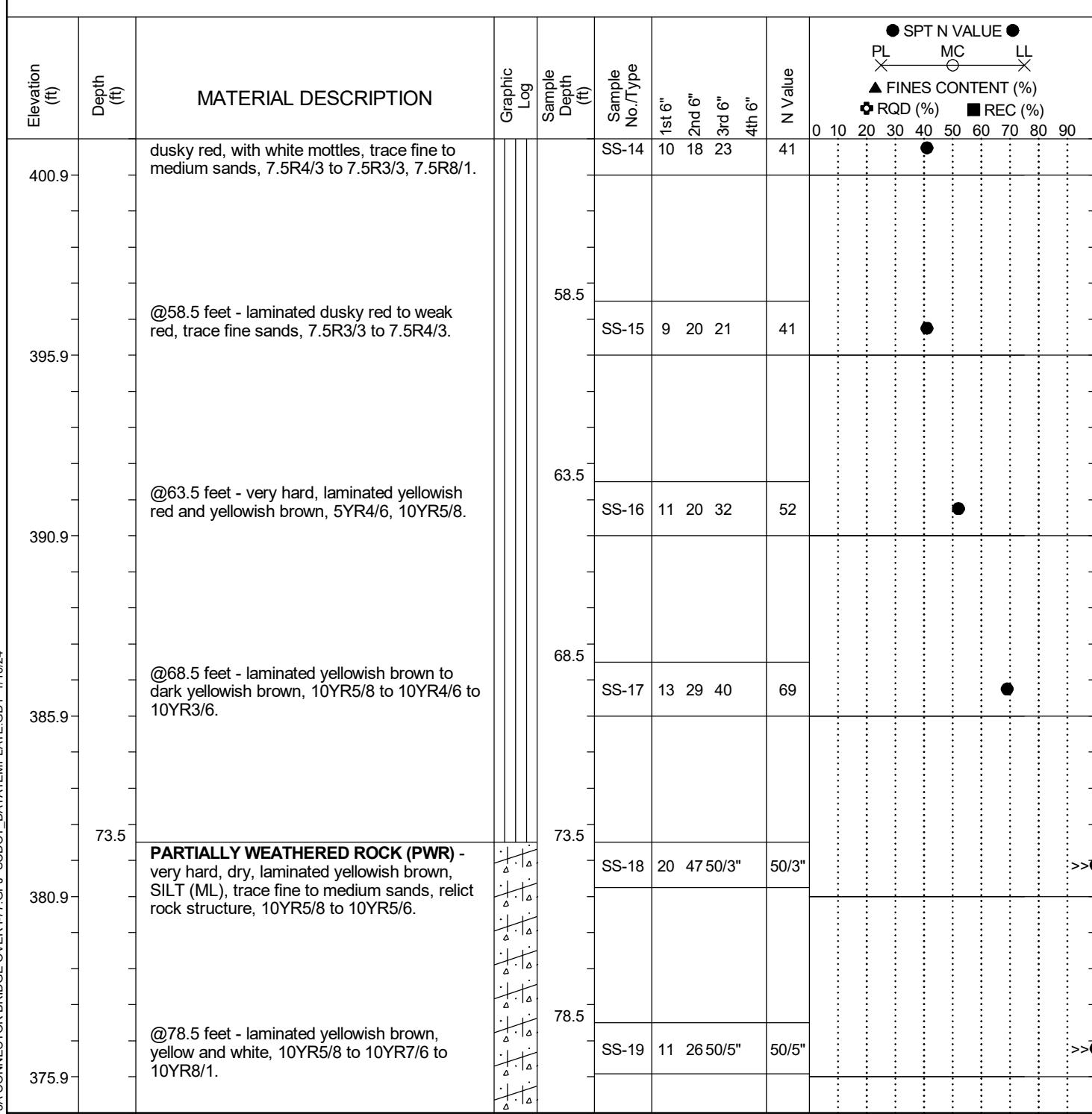


LEGEND

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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	IB-11C
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+67.94	Offset:	113.3	Alignment:	Proposed	
Elev.:	455.9 ft	Latitude:	34.190798359	Longitude:	-80.98376403	Date Started:	11/7/2023	
Total Depth:	99.9 ft	Soil Depth:	99.9 ft	Core Depth:	N/A ft	Date Completed:	11/7/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	16.2 ft



LEGEND

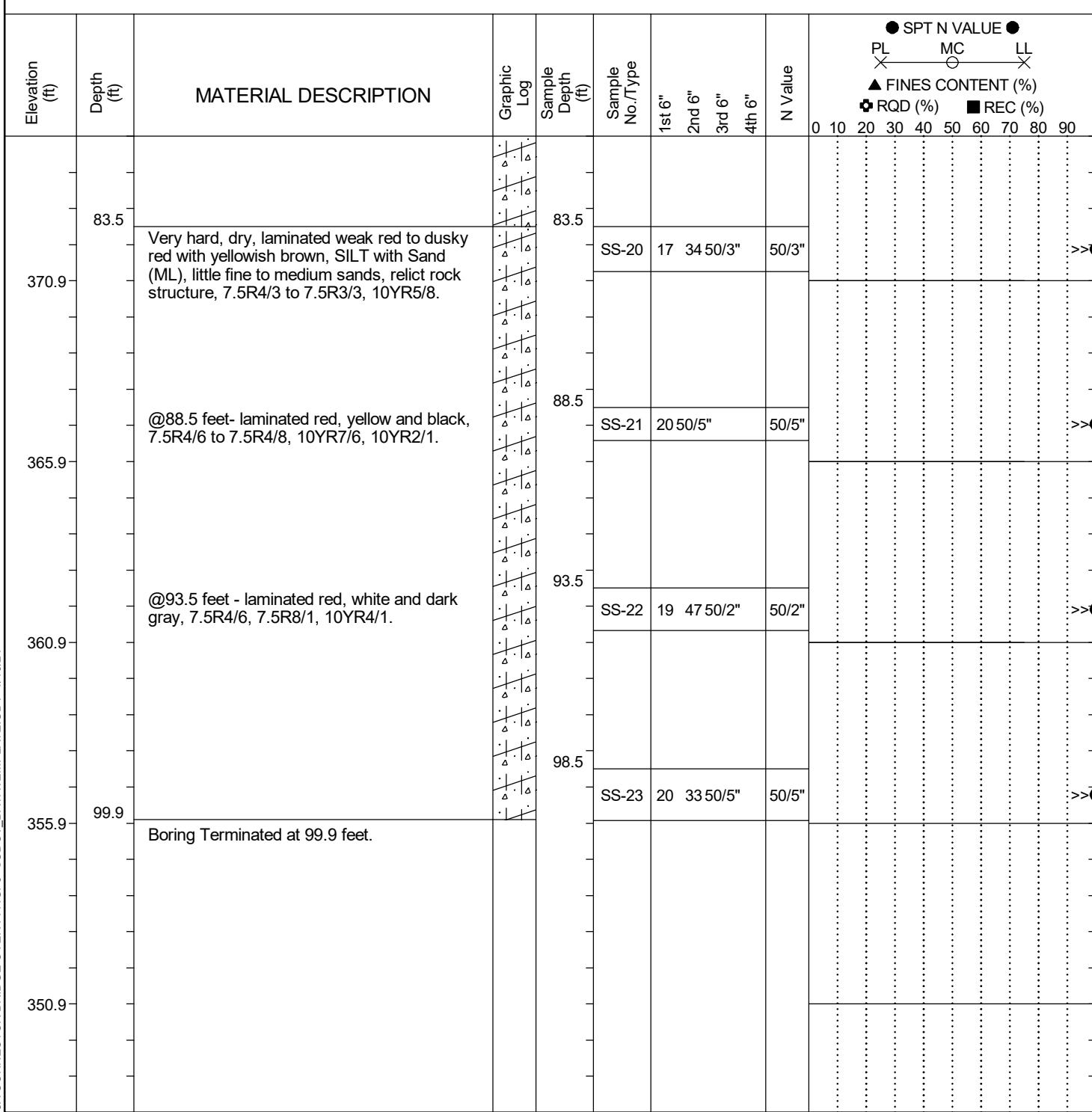
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



Soil Test Log

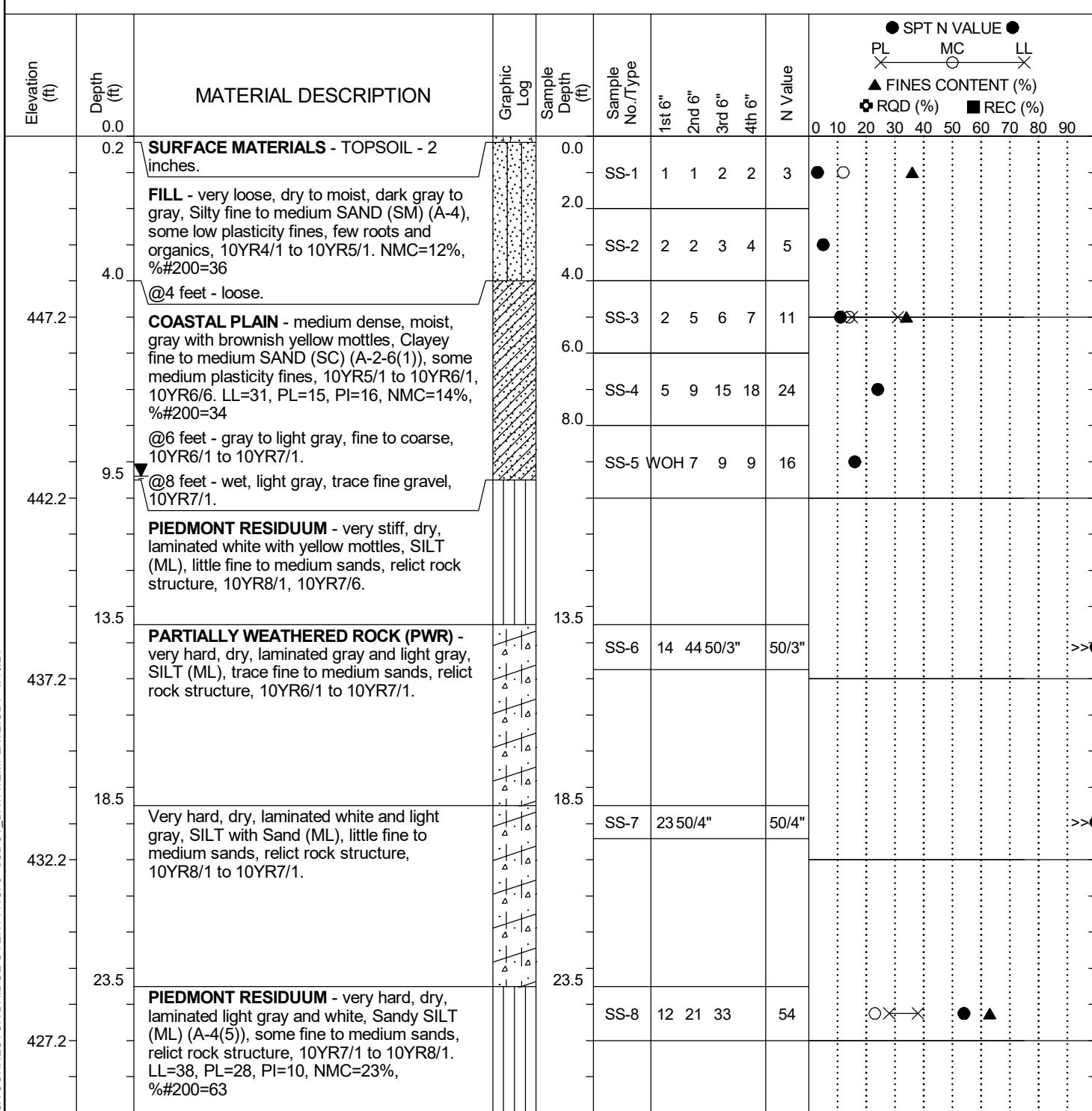
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Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	147+67.94	Offset:	113.3	Alignment:	Proposed	
Elev.:	455.9 ft	Latitude:	34.190798359	Longitude:	-80.98376403	Date Started:	11/7/2023	
Total Depth:	99.9 ft	Soil Depth:	99.9 ft	Core Depth:	N/A ft	Date Completed:	11/7/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	16.2 ft



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	W- 1
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+06.74	Offset:	-91.4	Alignment:	Proposed	
Elev.:	452.2 ft	Latitude:	34.191535214	Longitude:	-80.98322066	Date Started:	10/17/2023	
Total Depth:	40 ft	Soil Depth:	40 ft	Core Depth:	N/A ft	Date Completed:	10/17/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	9.4 ft



LEGEND

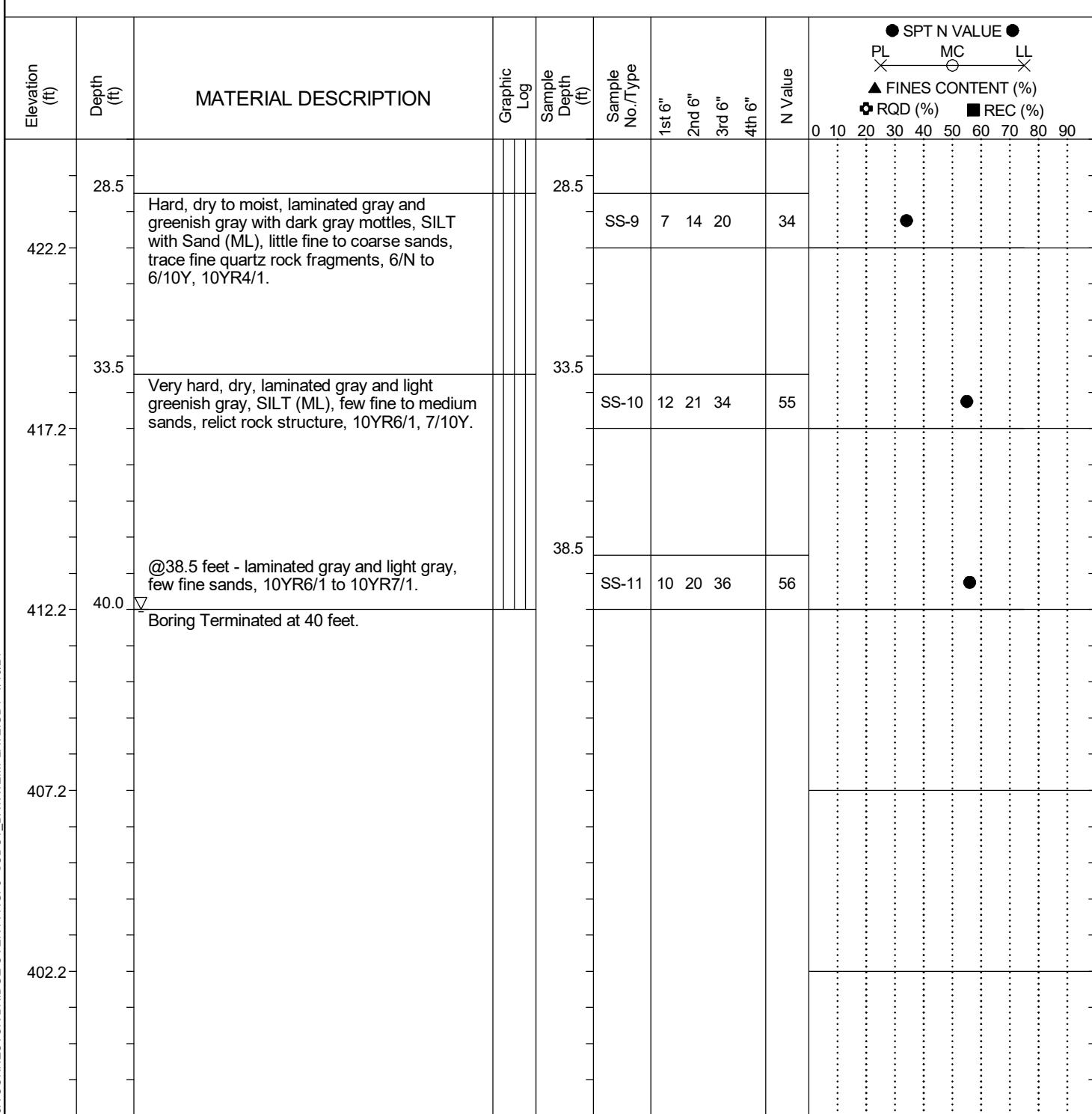
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



Soil Test Log

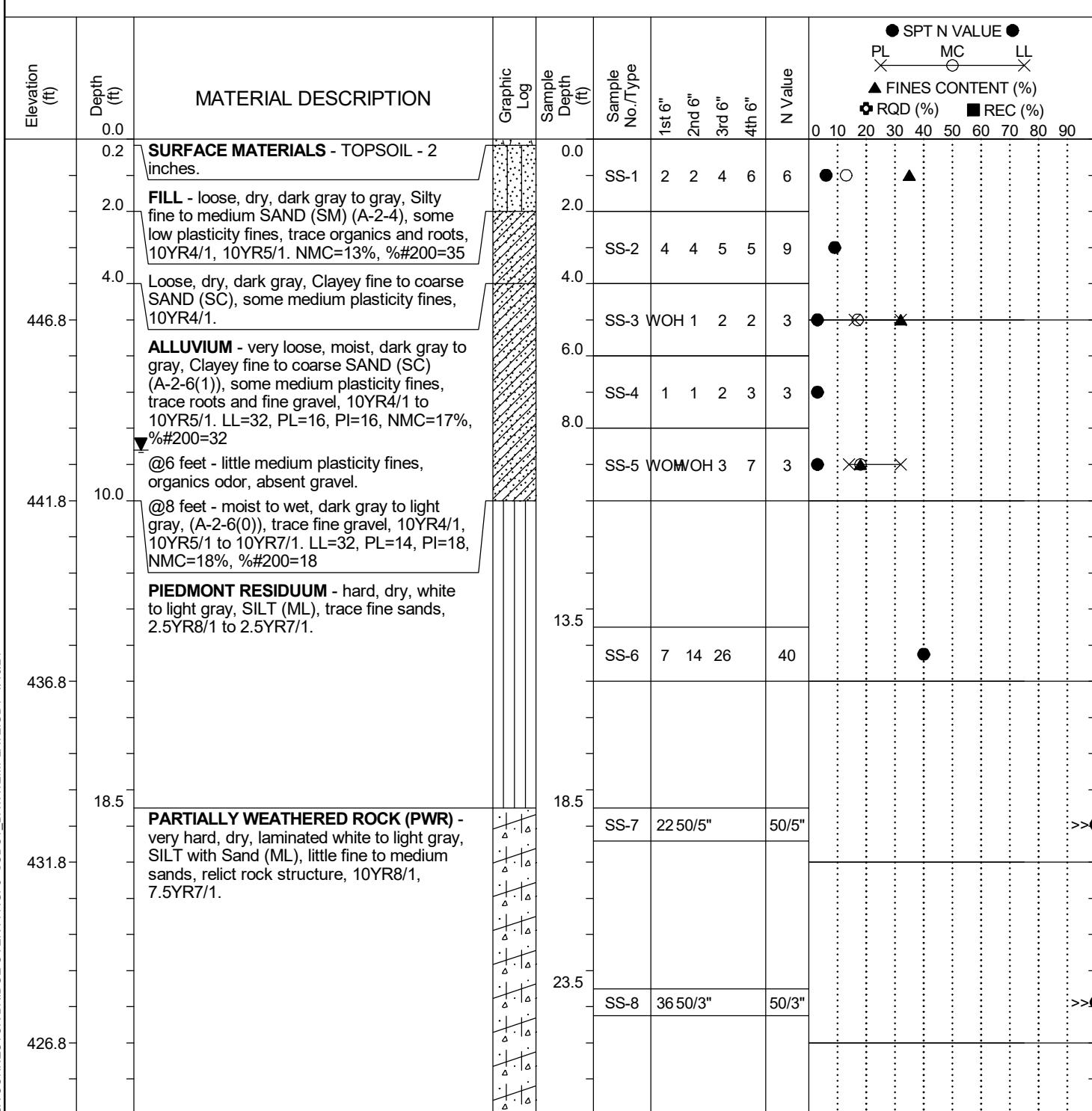
Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	W- 1
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+06.74	Offset:	-91.4	Alignment:	Proposed	
Elev.:	452.2 ft	Latitude:	34.191535214	Longitude:	-80.98322066	Date Started:	10/17/2023	
Total Depth:	40 ft	Soil Depth:	40 ft	Core Depth:	N/A ft	Date Completed:	10/17/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	9.4 ft



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)		County:	Richland		Boring No.:	W- 2
Site Description:	I-77 Exit 26 Phase I					Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+14.60	Offset:	-128.8	Alignment:	Proposed
Elev.:	451.8 ft	Latitude:	34.191639599	Longitude:	-80.98323392	Date Started:	10/17/2023
Total Depth:	39.9 ft	Soil Depth:	39.9 ft	Core Depth:	N/A ft	Date Completed:	10/17/2023
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR



LEGEND

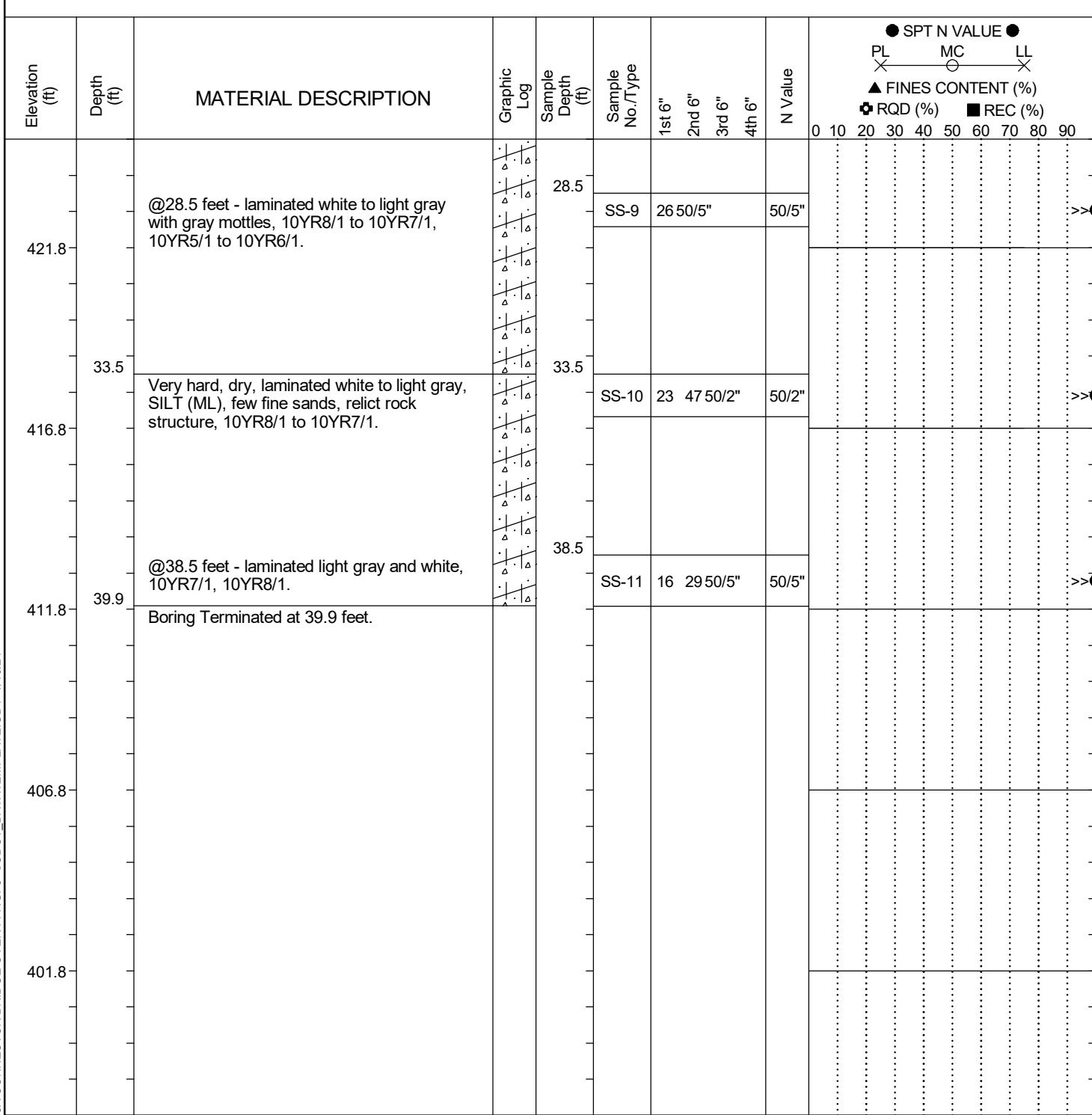
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SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	



Soil Test Log

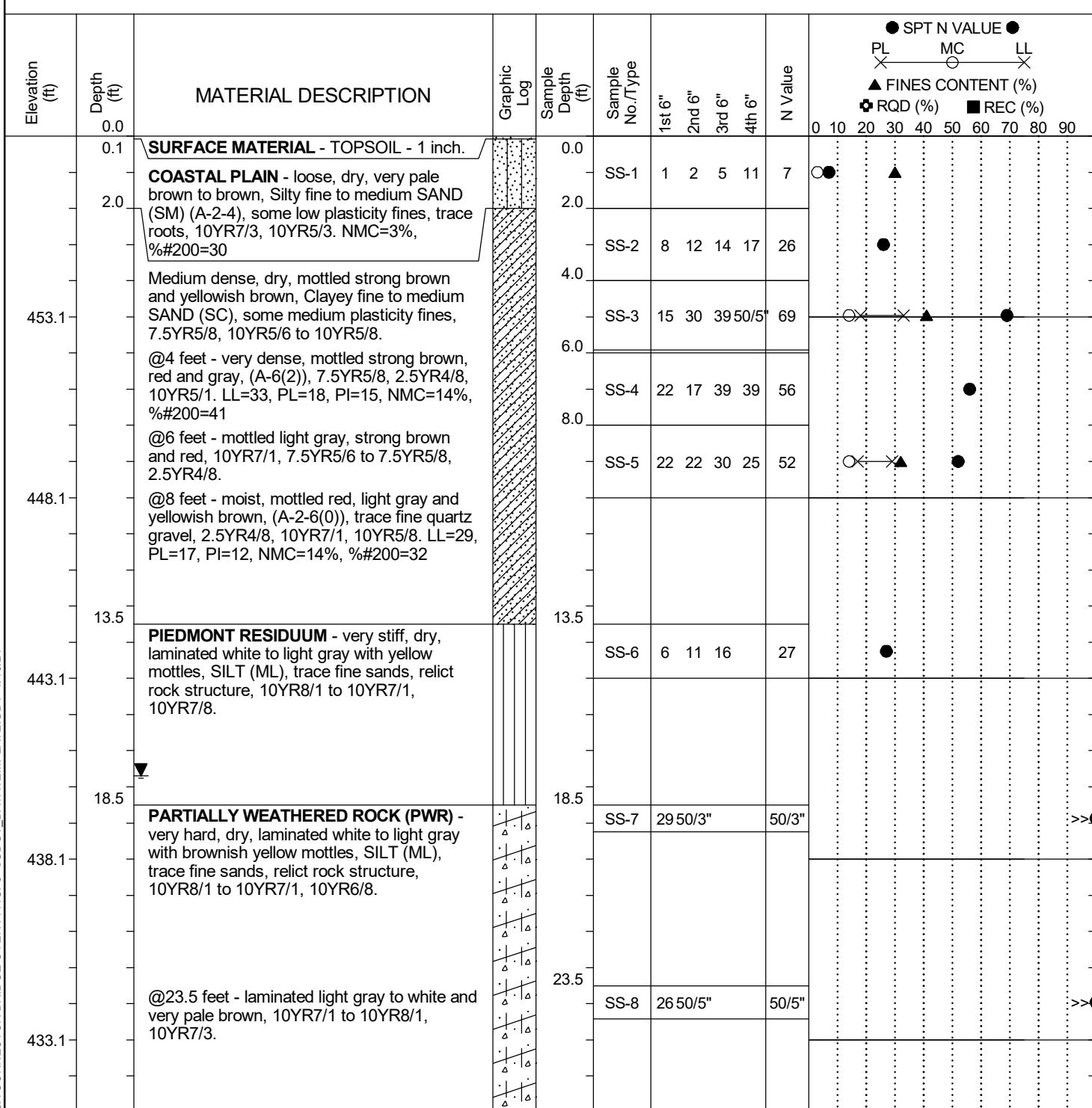
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Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+14.60	Offset:	-128.8	Alignment:	Proposed	
Elev.:	451.8 ft	Latitude:	34.191639599	Longitude:	-80.98323392	Date Started:	10/17/2023	
Total Depth:	39.9 ft	Soil Depth:	39.9 ft	Core Depth:	N/A ft	Date Completed:	10/17/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	8.6 ft



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	W- 3
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+11.80	Offset:	91.4	Alignment:	Proposed	
Elev.:	458.1 ft	Latitude:	34.191061525	Longitude:	-80.98301895	Date Started:	10/23/2023	
Total Depth:	39.4 ft	Soil Depth:	39.4 ft	Core Depth:	N/A ft	Date Completed:	10/23/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	17.7 ft



LEGEND

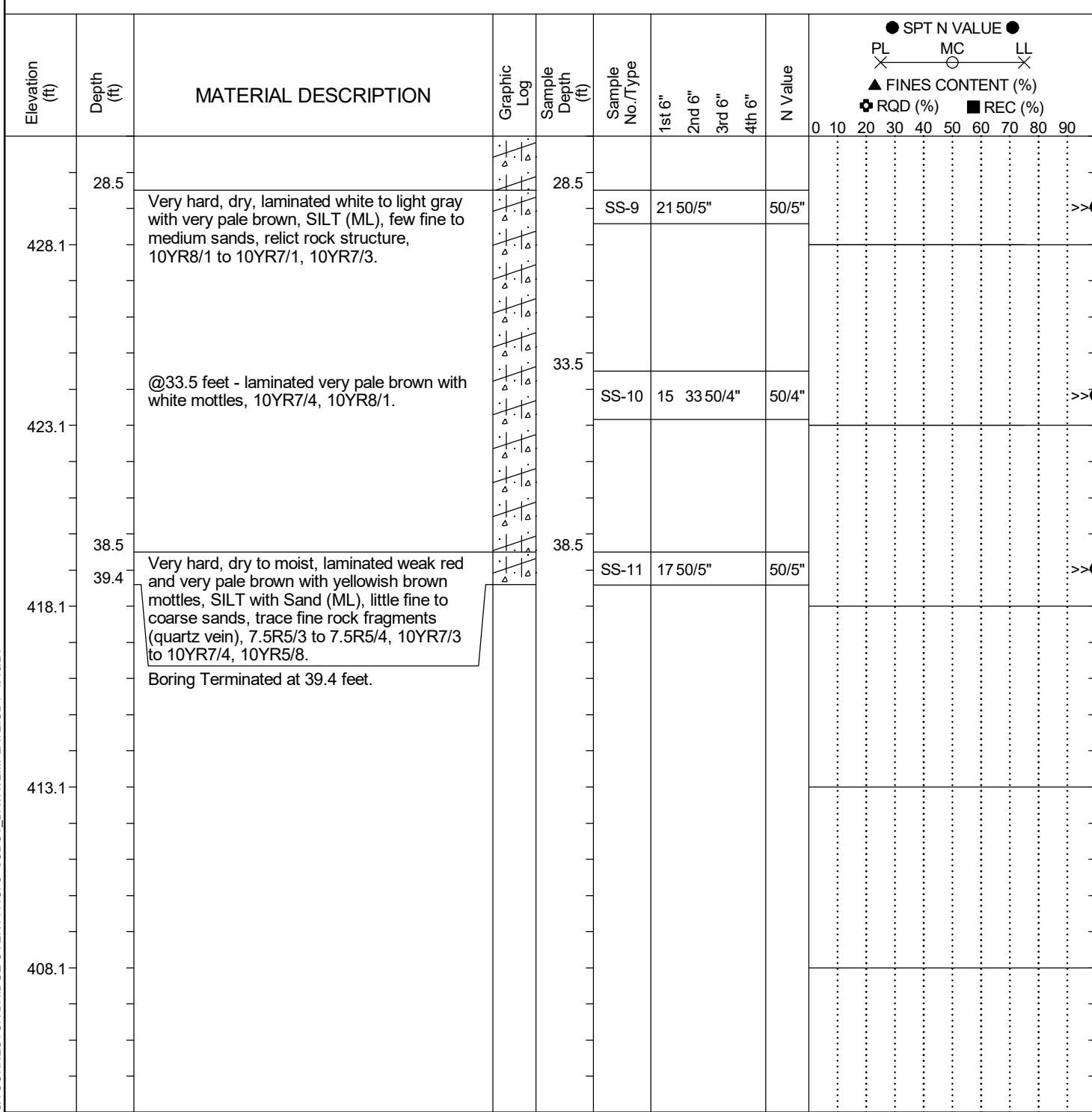
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



Soil Test Log

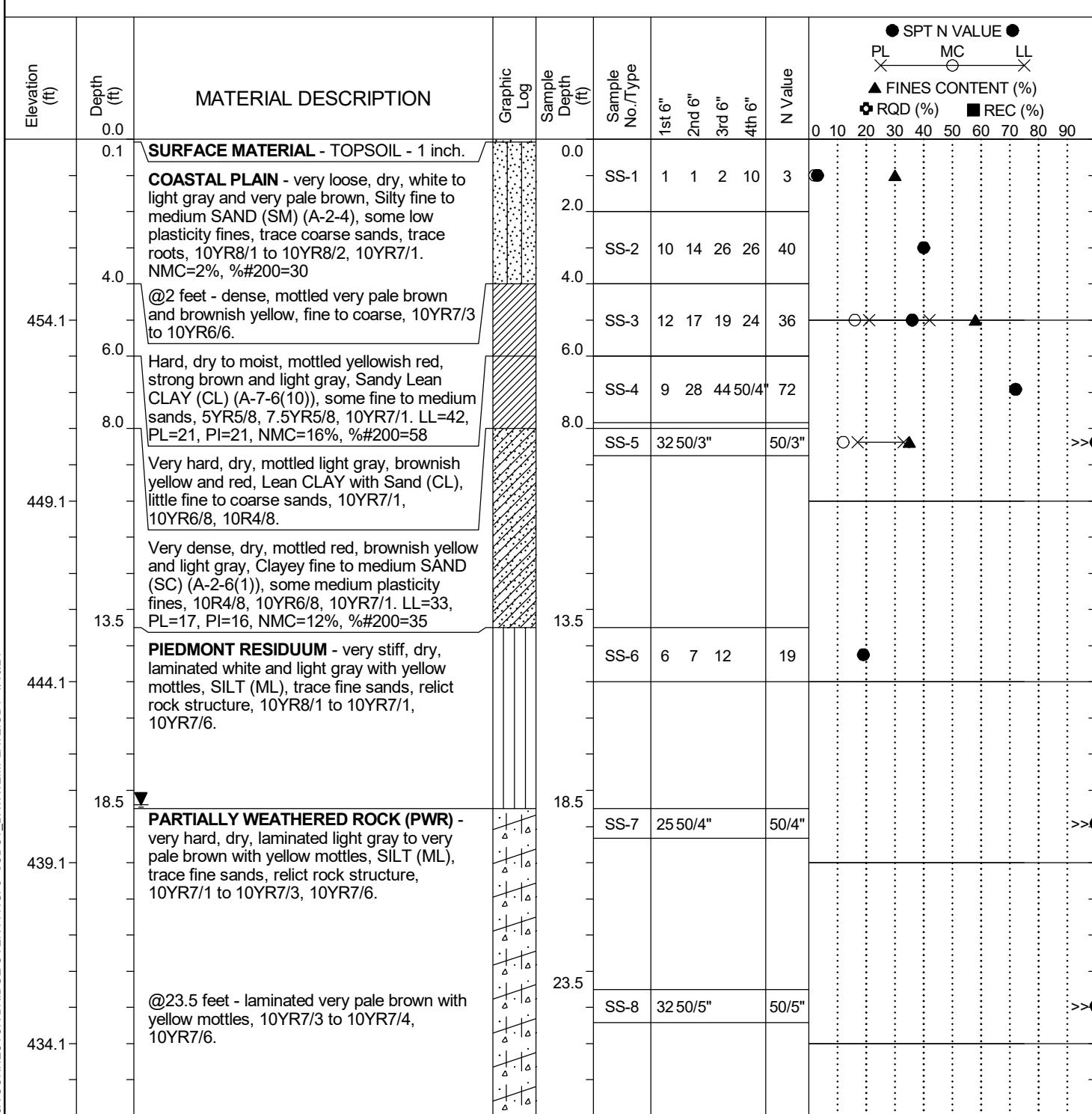
Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	W- 3
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+11.80	Offset:	91.4	Alignment:	Proposed	
Elev.:	458.1 ft	Latitude:	34.191061525	Longitude:	-80.98301895	Date Started:	10/23/2023	
Total Depth:	39.4 ft	Soil Depth:	39.4 ft	Core Depth:	N/A ft	Date Completed:	10/23/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y <input checked="" type="checkbox"/>	N <input type="checkbox"/>	Liner Used:	Y <input checked="" type="checkbox"/>
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	17.7 ft



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	W- 4
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+07.59	Offset:	118.7	Alignment:	Proposed	
Elev.:	459.1 ft	Latitude:	34.190986537	Longitude:	-80.98300442	Date Started:	10/20/2023	
Total Depth:	39.8 ft	Soil Depth:	39.8 ft	Core Depth:	N/A ft	Date Completed:	10/20/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	18.4 ft



LEGEND

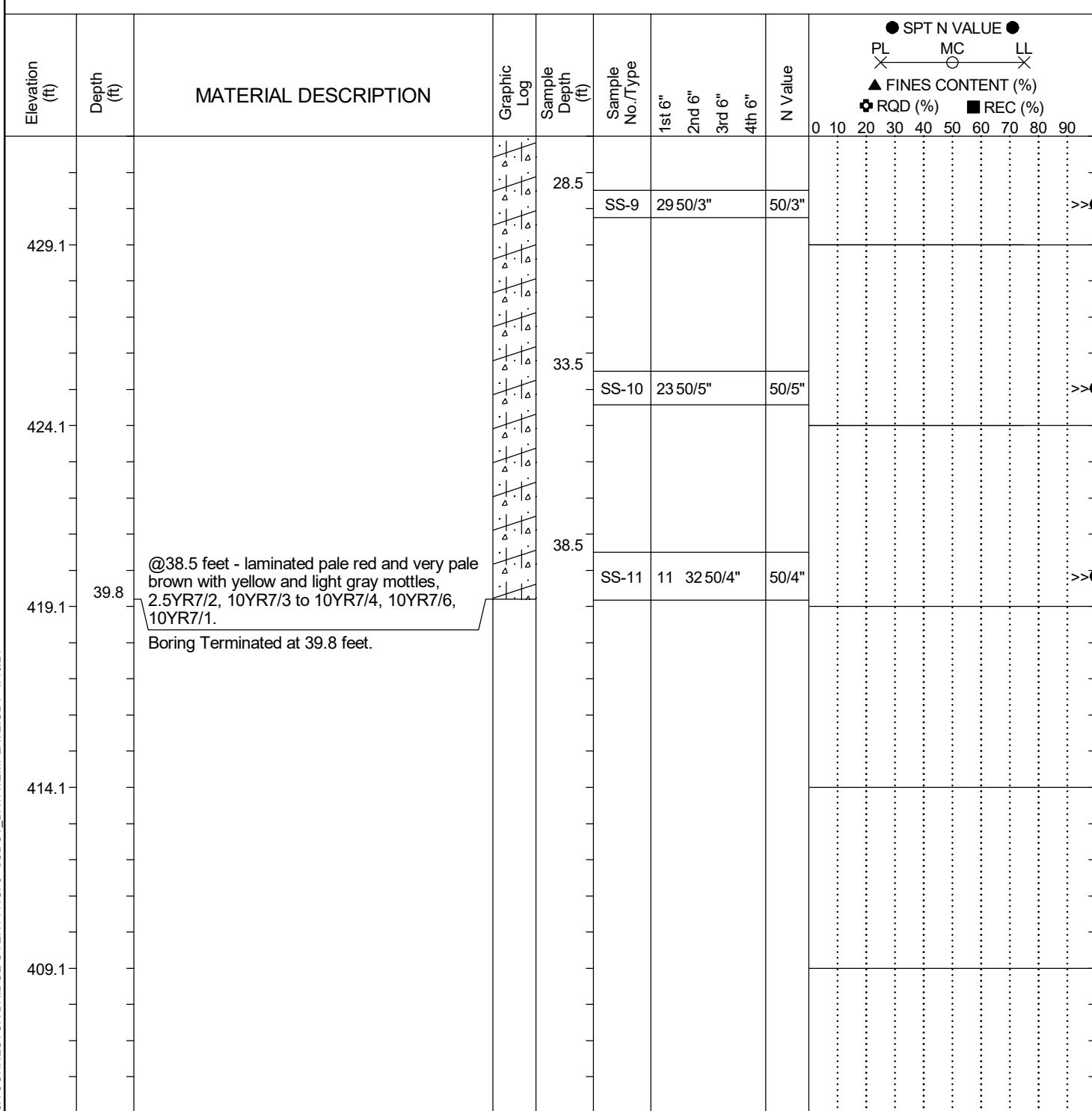
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



Soil Test Log

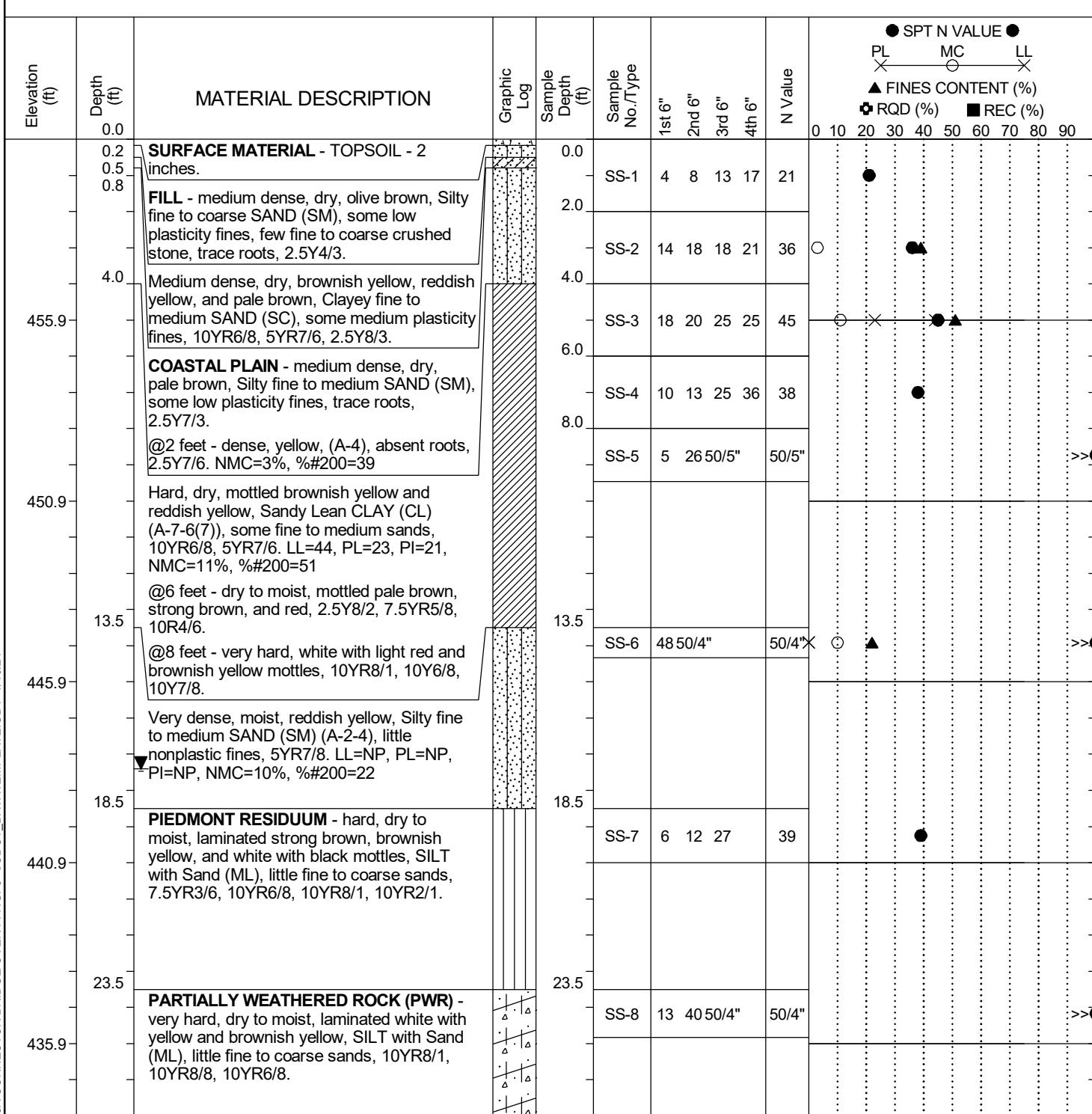
Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	W- 4
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	Z. Zelaya	Boring Location:	150+07.59	Offset:	118.7	Alignment:	Proposed	
Elev.:	459.1 ft	Latitude:	34.190986537	Longitude:	-80.98300442	Date Started:	10/20/2023	
Total Depth:	39.8 ft	Soil Depth:	39.8 ft	Core Depth:	N/A ft	Date Completed:	10/20/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	87.6%	
Core Size:	N/A	Driller:	S. Eubanks	Groundwater:	TOB	N/A	24HR	18.4 ft



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	W- 5
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	146+04.18	Offset:	-108.7	Alignment:	Proposed
Elev.:	460.9 ft		Latitude:	34.191240555	Longitude:	-80.984504934	Date Started:	10/4/2023
Total Depth:	40 ft	Soil Depth:	40 ft	Core Depth:	N/A ft	Date Completed:	10/4/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic		Energy Ratio:	91.6%
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	17.4 ft



LEGEND

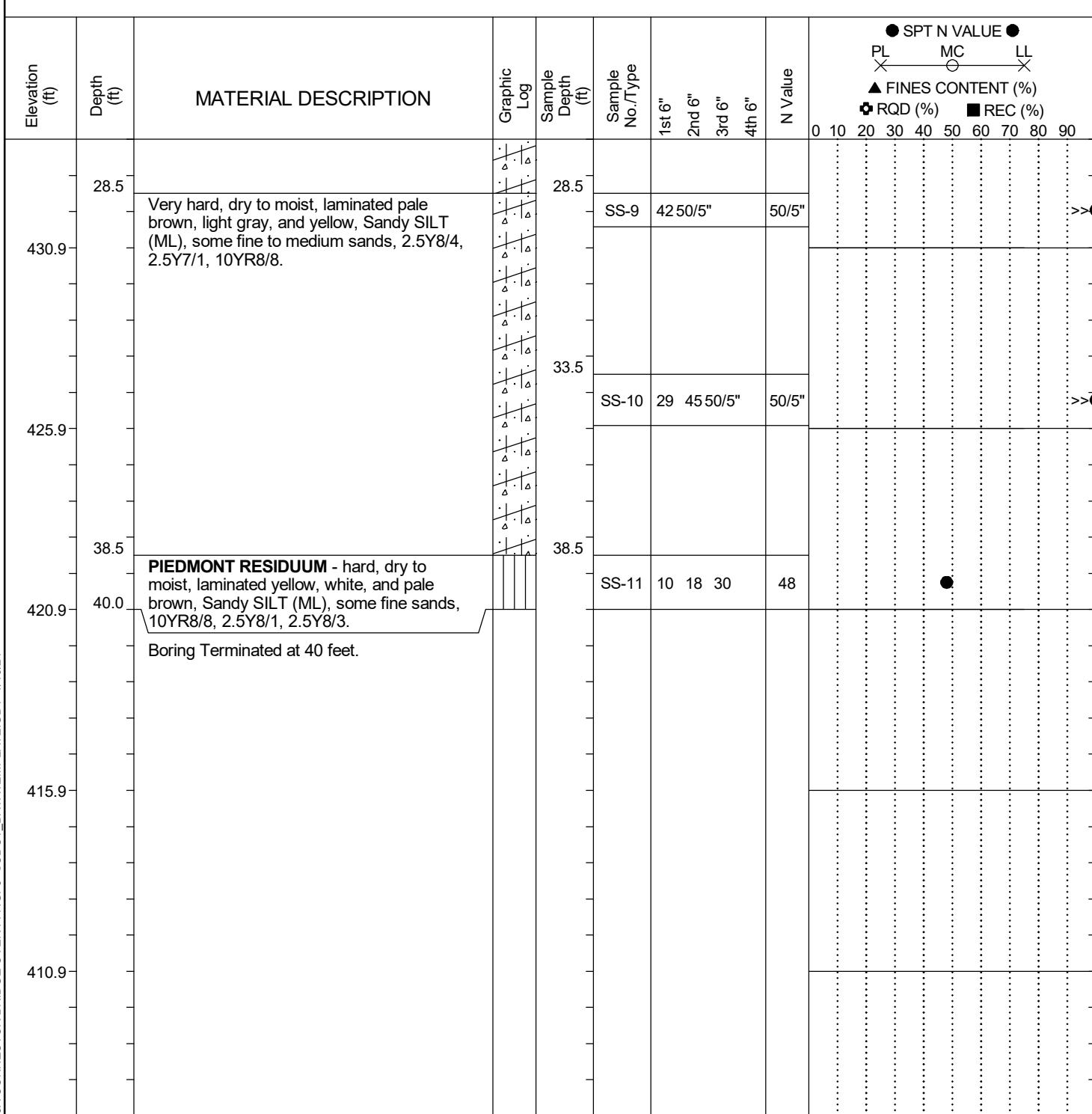
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



Soil Test Log

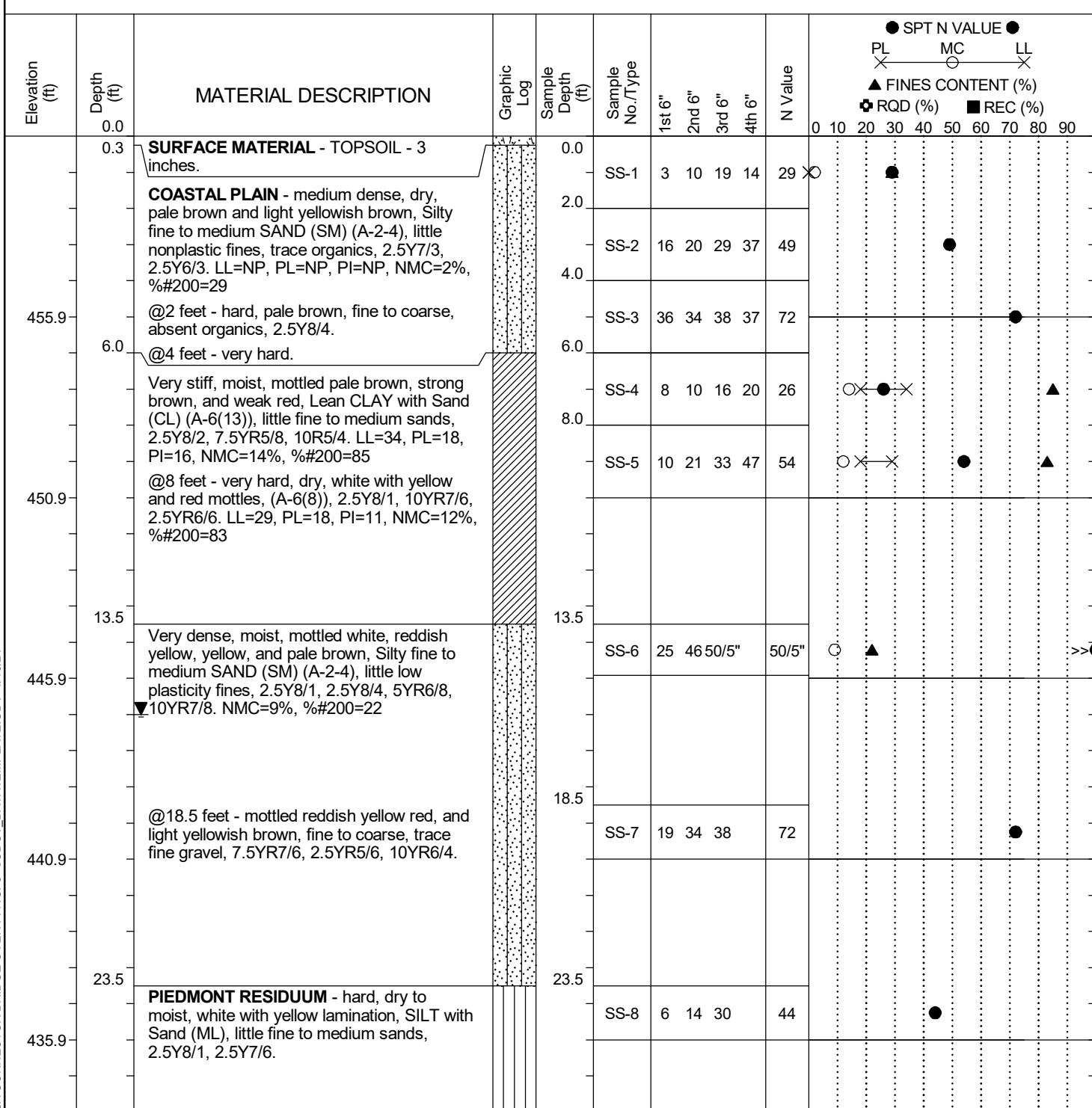
Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	W- 5
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks	Boring Location:	146+04.18	Offset:	-108.7	Alignment:	Proposed	
Elev.:	460.9 ft	Latitude:	34.191240555	Longitude:	-80.984504934	Date Started:	10/4/2023	
Total Depth:	40 ft	Soil Depth:	40 ft	Core Depth:	N/A ft	Date Completed:	10/4/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	17.4 ft



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	W- 6
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	146+02.27	Offset:	-75.6	Alignment:	Proposed
Elev.:	460.9 ft		Latitude:	34.191152368	Longitude:	-80.984477309	Date Started:	10/4/2023
Total Depth:	39.4 ft	Soil Depth:	39.4 ft	Core Depth:	N/A ft	Date Completed:	10/4/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic		Energy Ratio:	91.6%
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	16 ft



LEGEND

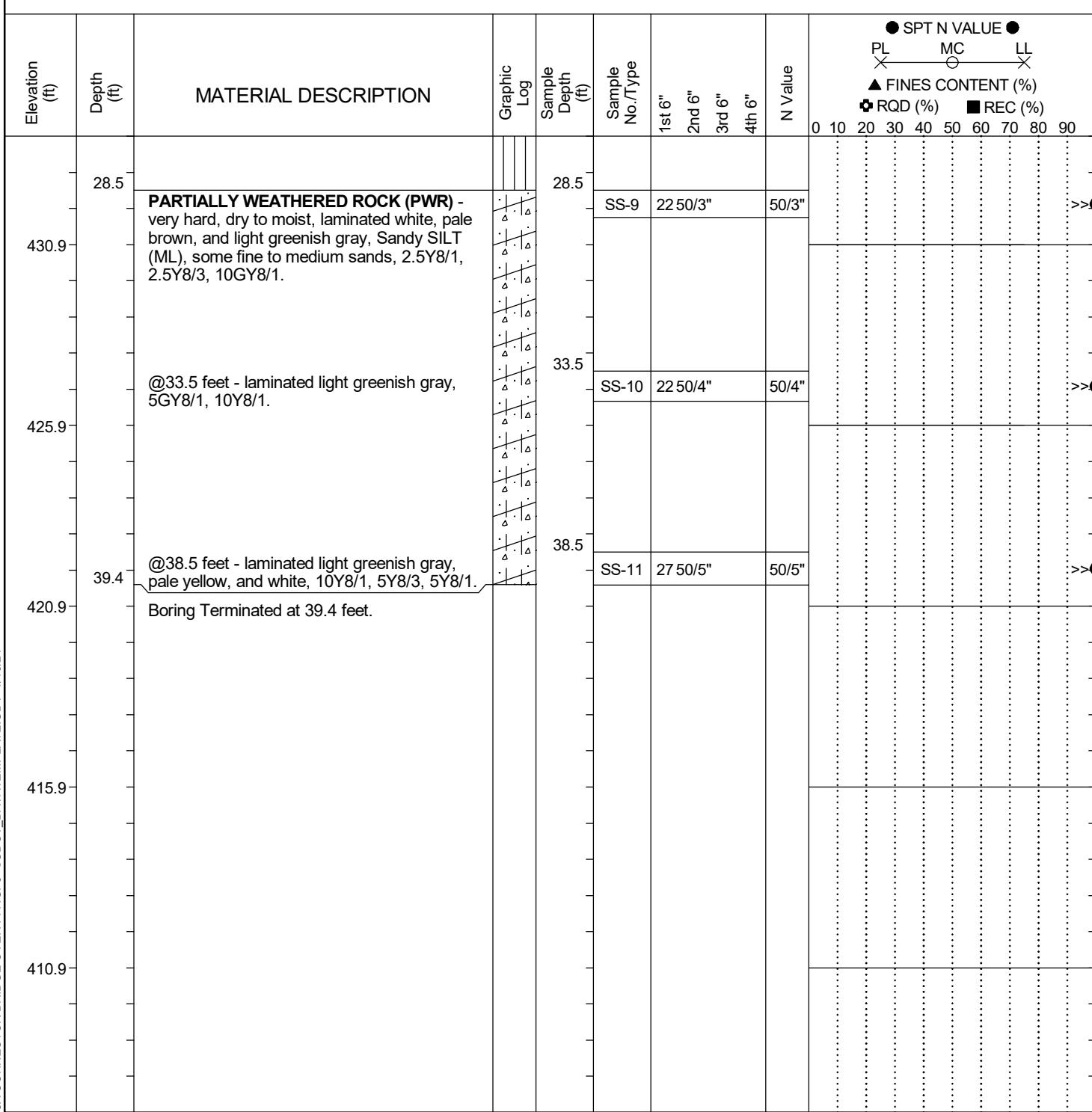
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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"			HSA - Hollow Stem Auger	RW - Rotary Wash		
UD - Undisturbed Sample	CU - Cuttings			CFA - Continuous Flight Augers	RC - Rock Core		
AWG - Rock Core, 1-1/8"	CT - Continuous Tube			DC - Driving Casing			



Soil Test Log

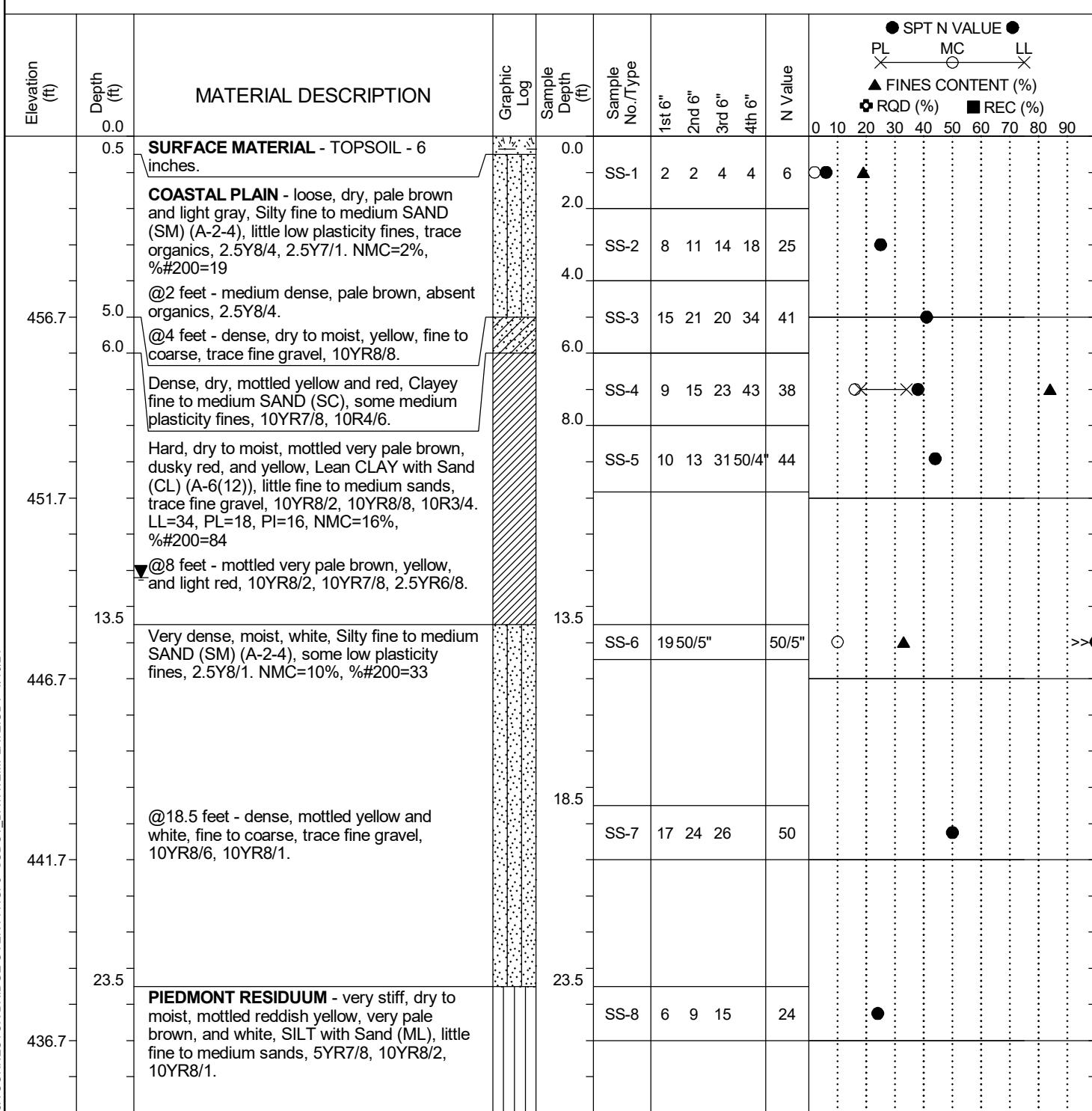
Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	W- 6
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	146+02.27	Offset:	-75.6	Alignment:	Proposed
Elev.:	460.9 ft		Latitude:	34.191152368	Longitude:	-80.984477309	Date Started:	10/4/2023
Total Depth:	39.4 ft	Soil Depth:	39.4 ft	Core Depth:	N/A ft	Date Completed:		10/4/2023
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y <input checked="" type="checkbox"/>	N <input type="checkbox"/>	Liner Used:	Y <input checked="" type="checkbox"/>
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:		91.6%
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	16 ft



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	W- 7		
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd		
Eng./Geo.:	E. Eastabrooks		Boring Location:	145+99.87		Offset:	101.9	Alignment:	Proposed	
Elev.:	461.7 ft		Latitude:	34.190686194		Longitude:	-80.984304447		Date Started:	10/3/2023
Total Depth:	40 ft		Soil Depth:	40 ft		Core Depth:	N/A ft	Date Completed:	10/3/2023	
Bore Hole Diameter (in):	4		Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y	(N)
Drill Machine:	CME-550X		Drill Method:	RW		Hammer Type:	Automatic		Energy Ratio:	91.6%
Core Size:	N/A		Driller:	L. Shrader		Groundwater:	TOB	N/A	24HR	12.2 ft



LEGEND

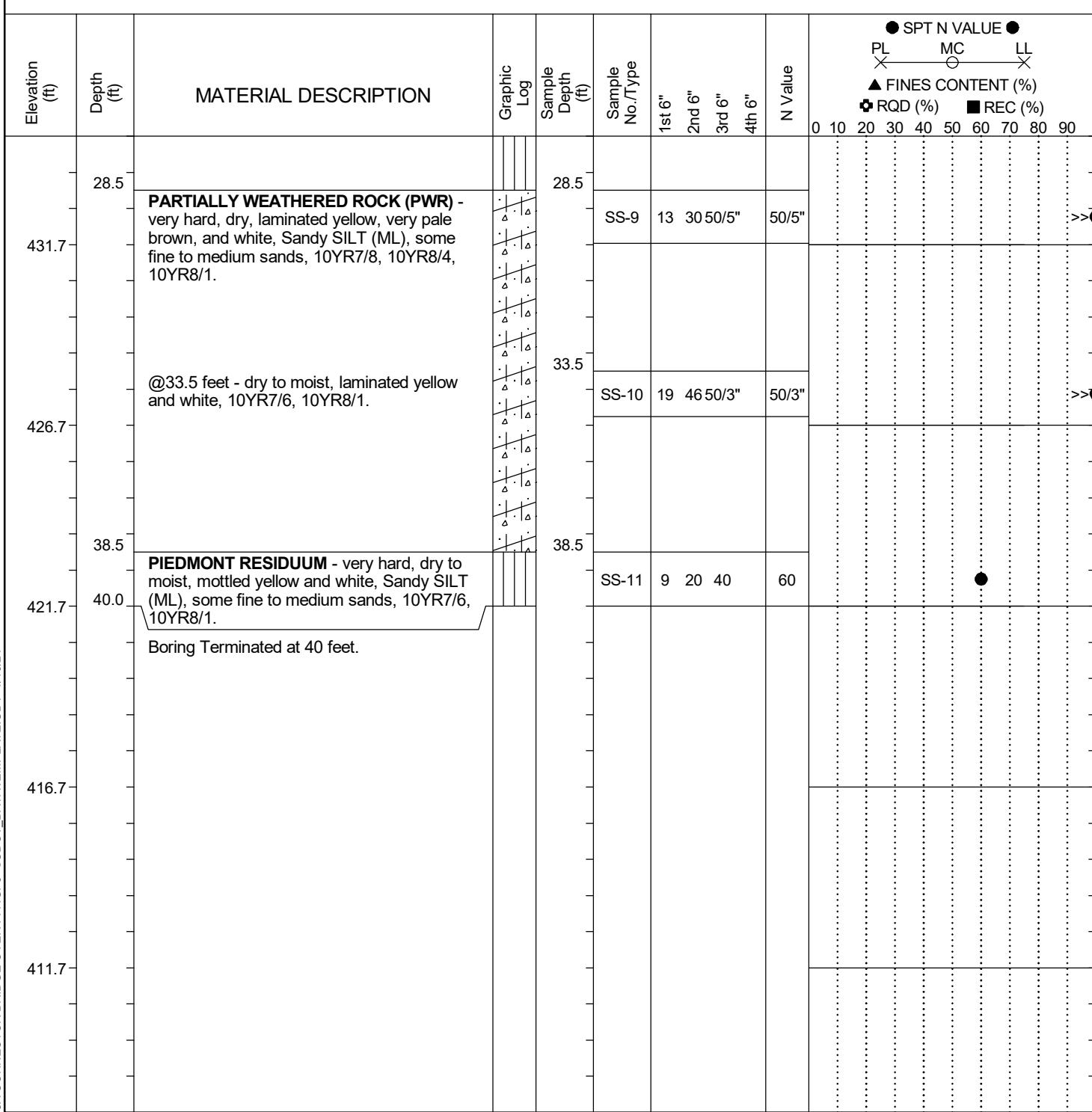
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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	CU - Cuttings	HSA - Hollow Stem Auger	RW - Rotary Wash			
UD - Undisturbed Sample		CT - Continuous Tube	CFA - Continuous Flight Augers	RC - Rock Core			
AWG - Rock Core, 1-1/8"			DC - Driving Casing				



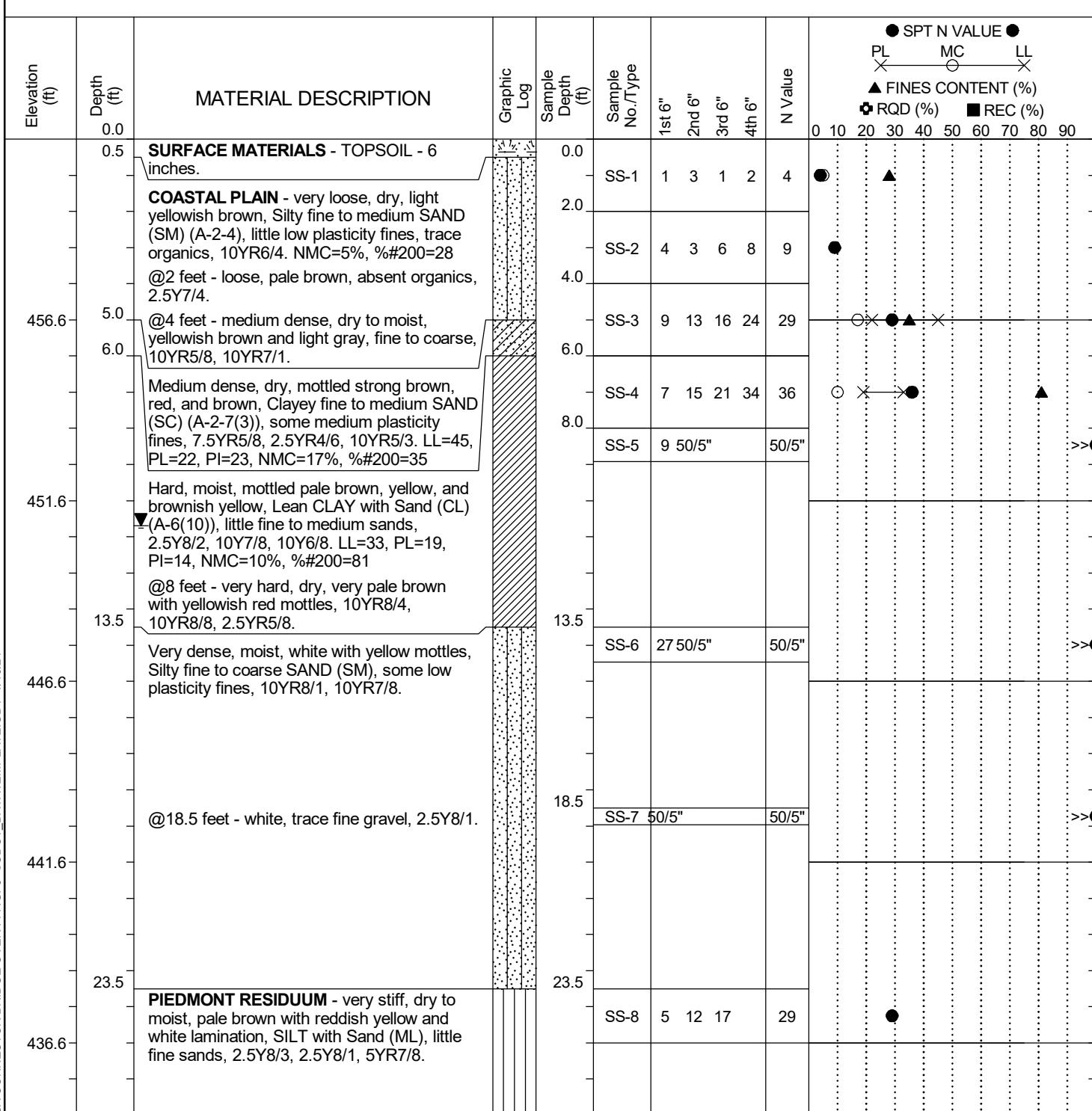
Soil Test Log

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	W- 7
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	145+99.87	Offset:	101.9	Alignment:	Proposed
Elev.:	461.7 ft	Latitude:	34.190686194	Longitude:	-80.984304447	Date Started:	10/3/2023	
Total Depth:	40 ft	Soil Depth:	40 ft	Core Depth:	N/A ft	Date Completed:	10/3/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y <input checked="" type="checkbox"/>	N <input type="checkbox"/>	Liner Used:	Y <input checked="" type="checkbox"/>
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	91.6%	
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	12.2 ft



SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	W- 8
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	146+00.33	Offset:	118.6	Alignment:	Proposed
Elev.:	461.6 ft		Latitude:	34.190642943	Longitude:	-80.984286044	Date Started:	10/3/2023
Total Depth:	39.8 ft	Soil Depth:	39.8 ft	Core Depth:	N/A ft	Date Completed:	10/3/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic		Energy Ratio:	91.6%
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	10.7 ft



LEGEND

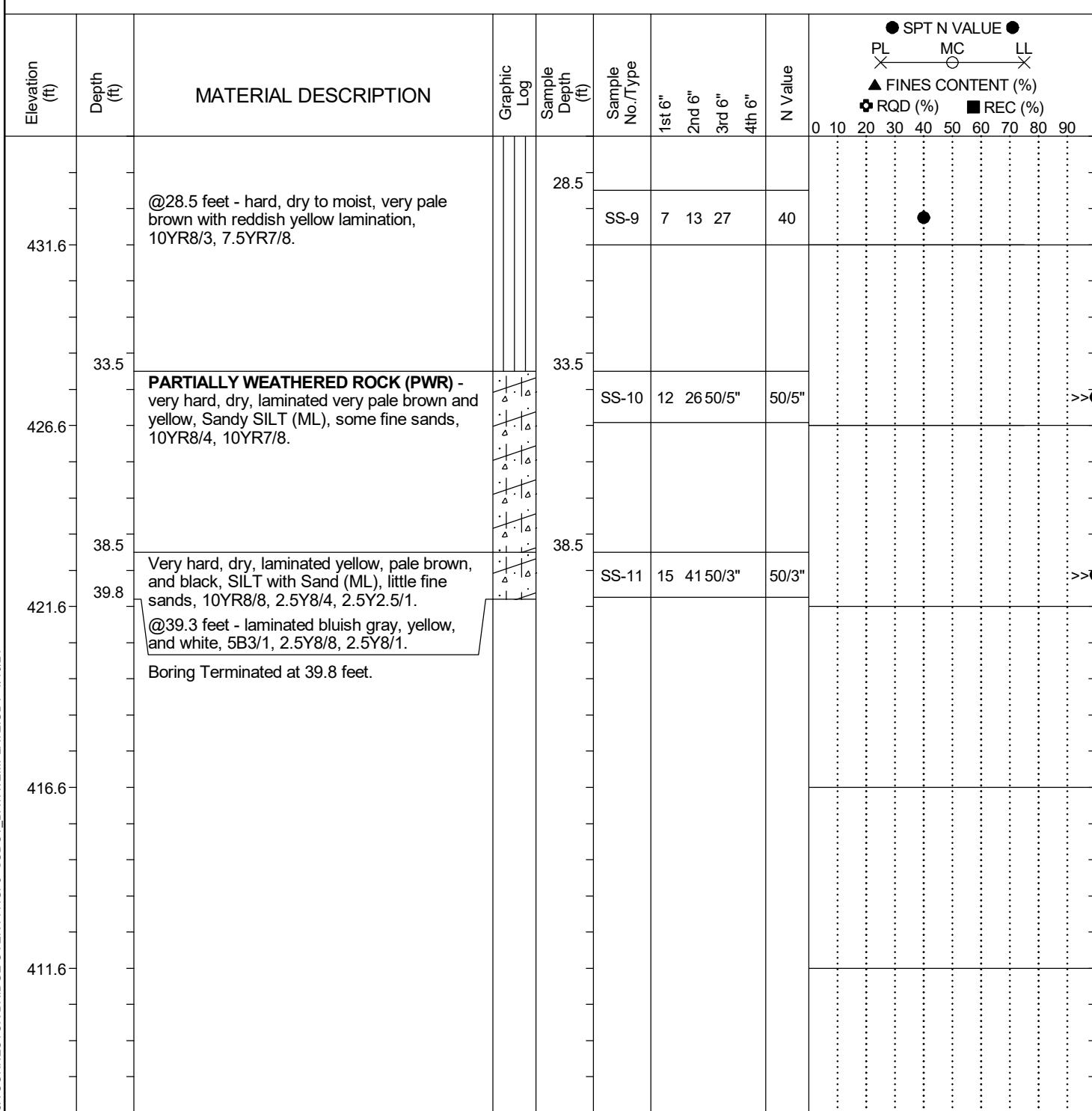
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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash				
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core				
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing					



Soil Test Log

Project ID:	P042443 (S&ME 23610178A)			County:	Richland		Boring No.:	W- 8
Site Description:	I-77 Exit 26 Phase I						Route:	Connector Rd
Eng./Geo.:	E. Eastabrooks		Boring Location:	146+00.33	Offset:	118.6	Alignment:	Proposed
Elev.:	461.6 ft		Latitude:	34.190642943	Longitude:	-80.984286044	Date Started:	10/3/2023
Total Depth:	39.8 ft	Soil Depth:	39.8 ft	Core Depth:	N/A ft	Date Completed:	10/3/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y	(N)	Liner Used:	Y
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic		Energy Ratio:	91.6%
Core Size:	N/A	Driller:	L. Shrader	Groundwater:	TOB	N/A	24HR	10.7 ft



Appendix IV– Downhole Shear Wave Velocity Test Results



Shear Wave Velocity Calculations

I-77 Exit 26 Phase I
Blythewood, South Carolina

Sounding ID: EB-1C

S&ME Project Number: **23610178A**

Casing Stickup: **2.50** Feet
Source Offset: 8.00 Feet

Date: 30-Oct-23
Rig: CME-550X

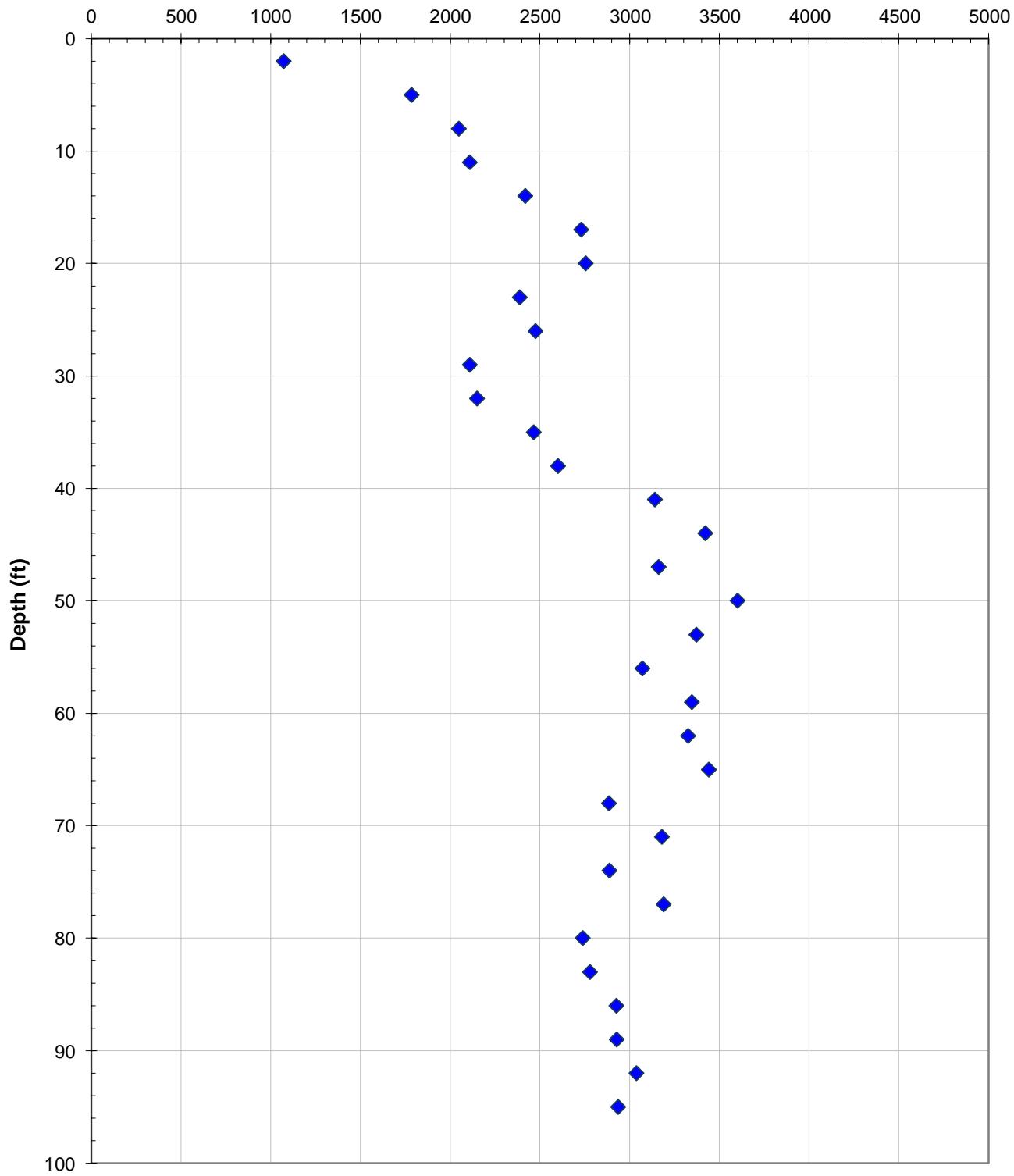
Test Depth (feet)	Geophone Depth (feet)	Waveform Ray Path (feet)	Incremental Distance (feet)	S-WAVE				d_i/v_{si}	Poissons
				Characteristic Arrival Time (seconds)	Incremental Time Interval (seconds)	Interval Velocity (ft/s)	Interval Depth (feet)		
0.50	0.50	8.02	8.02	0.0090					
3.50	3.50	8.73	0.72	0.0097	0.0007	1072.3	2.00	0.00187	0.24
6.50	6.50	10.31	1.58	0.0105	0.0009	1784.1	5.00	0.00168	0.10
9.50	9.50	12.42	2.11	0.0116	0.0010	2047.8	8.00	0.00146	0.07
12.50	12.50	14.84	2.42	0.0127	0.0011	2109.2	11.00	0.00142	0.28
15.50	15.50	17.44	2.60	0.0138	0.0011	2418.9	14.00	0.00124	0.28
18.50	18.50	20.16	2.71	0.0148	0.0010	2730.1	17.00	0.00110	0.16
21.50	21.50	22.94	2.78	0.0158	0.0010	2755.0	20.00	0.00109	0.11
24.50	24.50	25.77	2.83	0.0170	0.0012	2388.4	23.00	0.00126	0.33
27.50	27.50	28.64	2.87	0.0182	0.0012	2475.2	26.00	0.00121	0.33
30.50	30.50	31.53	2.89	0.0195	0.0014	2108.7	29.00	0.00142	0.43
33.50	33.50	34.44	2.91	0.0209	0.0014	2149.5	32.00	0.00140	0.44
36.50	36.50	37.37	2.92	0.0221	0.0012	2465.6	35.00	0.00122	0.43
39.50	39.50	40.30	2.94	0.0232	0.0011	2600.8	38.00	0.00115	0.43
42.50	42.50	43.25	2.94	0.0241	0.0009	3141.0	41.00	0.00096	0.39
45.50	45.50	46.20	2.95	0.0250	0.0009	3421.6	44.00	0.00088	0.38
48.50	48.50	49.16	2.96	0.0259	0.0009	3160.8	47.00	0.00095	0.36
51.50	51.50	52.12	2.96	0.0268	0.0008	3601.0	50.00	0.00083	0.20
54.50	54.50	55.08	2.97	0.0276	0.0009	3370.8	53.00	0.00089	0.26
57.50	57.50	58.05	2.97	0.0286	0.0010	3070.6	56.00	0.00098	0.37
60.50	60.50	61.03	2.97	0.0295	0.0009	3345.9	59.00	0.00090	0.37
63.50	63.50	64.00	2.98	0.0304	0.0009	3325.1	62.00	0.00090	0.33
66.50	66.50	66.98	2.98	0.0312	0.0009	3441.3	65.00	0.00087	0.26
69.50	69.50	69.96	2.98	0.0323	0.0010	2884.1	68.00	0.00104	0.30
72.50	72.50	72.94	2.98	0.0332	0.0009	3180.2	71.00	0.00094	0.26
75.50	75.50	75.92	2.98	0.0342	0.0010	2887.2	74.00	0.00104	0.35
78.50	78.50	78.91	2.98	0.0352	0.0009	3189.1	77.00	0.00094	0.35
81.50	81.50	81.89	2.99	0.0363	0.0011	2738.6	80.00	0.00110	0.41
84.50	84.50	84.88	2.99	0.0373	0.0011	2778.7	83.00	0.00108	0.42
87.50	87.50	87.86	2.99	0.0384	0.0010	2926.6	86.00	0.00103	0.42
90.50	90.50	90.85	2.99	0.0394	0.0010	2927.4	89.00	0.00102	0.43
93.50	93.50	93.84	2.99	0.0404	0.0010	3037.3	92.00	0.00099	0.43
96.50	96.50	96.83	2.99	0.0414	0.0010	2935.6	95.00	0.00102	0.43



Shear Wave Velocity Profile EB-1C

I-77 Exit 26 Phase-I
Blythewood, South Carolina
S&ME Project: 23610178A

Shear Wave Velocity, Vs (ft/sec)



Appendix V – SPT Hammer Energy Measurements



Report of SPT Energy Measurements
S&ME CME-550X ATV
(Serial No. 290593)
Blythewood, South Carolina

PREPARED FOR:

**North Carolina Department of Transportation
Geotechnical Engineering Unit
1589 Mail Service Center
Raleigh, North Carolina 27699**

PREPARED BY:

**S&ME, Inc.
8848 Red Oak Boulevard, Suite A
Charlotte, North Carolina 28217**

December 27, 2023



December 27, 2023

North Carolina Department of Transportation
Geotechnical Engineering Unit
1589 Mail Service Center
Raleigh, North Carolina 27699

Attention: Mr. Greg Bodenheimer, P.E.

Cc: Ms. Cheryl A. Youngblood, L.G.
Ms. Christina M. Bruinsma, L.G.

Reference: **Report of SPT Energy Measurements**
S&ME CME-550X ATV (Serial No. 290593)
Blythewood, South Carolina
NC PE Firm License No. F-0176

Dear Mr. Bodenheimer:

We have completed the Standard Penetration Test (SPT) energy measurements on the automatic hammer used with our CME-550X ATV-mounted drill rig (Serial No. 290593). This service was performed by Mr. Joseph Williamson, P.E. of our firm on November 17, 2023, in general accordance with ASTM D4633 and the most recent revision of the North Carolina Department of Transportation (NCDOT) Geotechnical Engineering Unit's requirements. Review of the data quality and analyses was performed by Mr. Williamson. A copy of the Certificate of Proficiency issued by Pile Dynamics based on the Dynamic Measurement and Analysis Proficiency Test for Mr. Williamson is included in Appendix I. The testing procedures, equipment used during testing, and detailed results are presented in this report.

1.0 Dynamic Testing Methodology

Testing was performed using a model PAX (Serial No. 3726L) Pile Driving Analyzer™ (PDA) manufactured by Pile Dynamics, Inc. The PDA was used to record and interpret data from two piezoresistive accelerometers (Serial Nos. K4664 and K4665) bolted to a 2.0-foot long AWJ drill rod (Serial No. 203) internally instrumented with two strain transducers. Calibration sheets for the accelerometers and the instrumented rod are included in Appendix II. The instrumented AWJ drill rod has a cross-sectional area of 1.22 square inches and an outside diameter of approximately 1 $\frac{3}{4}$ inches. Therefore, we calculate the inside diameter to be approximately 1 $\frac{1}{4}$ inches at the gauge location. The accelerometers and strain gauges, which are diametrically opposed near the middle of the instrumented rod, monitor acceleration and strain for each hammer blow. The analyzer converts the data to velocities and forces and computes the maximum transferred hammer energies with the "EFV" method described in ASTM D4633. Preliminary results are recorded and displayed in real time for each blow.



2.0 Testing and Observations

S&ME personnel were on site November 17, 2023, to observe and perform high-strain dynamic testing during SPT sampling on the CME-550X ATV-mounted drill rig operated by Larry Shrader of S&ME. The measurements were taken during drilling of a test hole adjacent to a previous soil test boring at an S&ME project site in Blythewood, South Carolina. SPT energy measurements were recorded during four sampling intervals that generally met the NCDOT testing requirements. Two of the samples do not specifically meet the required N-value or rod length interval. However, analysis of the test data indicates the data from these samples generally agrees with the two samples that do meet the testing requirements. Preliminary test results were shared with Mr. Bodenheimer on December 19, 2023 for review. Mr. Bodenheimer agreed that, collectively the four samples provide an appropriate evaluation of the hammer energy transfer. The information presented in the tables below summarizes the equipment and tooling used during the SPT energy measurements. The SPT Energy Evaluation Form and the Soil Test Boring Log from the adjacent boring are included in Appendix III.

Table 2-1: Drill Rig Information

Manufacturer	CME
Model	550X
Serial Number	290593
Operator	L. Shrader
Carrier	ATV

Table 2-2: Hammer Information

Model / Type	CME / Auto
Serial Number	290593
Typical Drop Height (inches)	30
Typical Ram Weight (pounds)	140
Ram Serial Number	N/A



Table 2-3: Drilling and Instrumented Rod Information

Instrumented Rod Type	AWJ (Serial No. 203)
OD (inches) ¹	1 ³ / ₄
ID (inches) ²	1 ¹ / ₄
Cross-Sectional Area (in ²) ³	1.22
Total Instrumented Rod Length (feet) ¹	2.0
Length Below Gages (feet) ¹	0.7
Typical Rod Lengths (feet)	5
Split-Spoon Length (feet) ¹	2.85

3.0 Dynamic Testing Results

The total rod length from the instrumentation to the tip of the split-spoon sampler was determined by adding 3.55 ft to the drill rod length at each sample depth. The SPT Energy Measurement Data Summary tables in Appendix IV present the test data from every hammer blow at each sampling interval, along with representative force and velocity traces for each test interval. Per ASTM D4633, only the blows from the final foot of each sample interval (i.e. the blows that determine the N-value) are considered when computing the average measurement values of each test interval.

The reported blow counts obtained by the drill rig personnel, a summary of the test data, and average computed hammer energy and transfer ratio values are provided in Table 3-1. Based on the test data, the automatic hammer on the CME-550X operated at an average rate of about 59 blows per minute (bpm) during dynamic testing. The measured average transferred hammer energy (EFV) of the four sample intervals tested ranged from 316 to 326 ft-lbs, which corresponds to Energy Transfer Ratio (ETR) values of 90.3 to 93.2%, respectively. Plots and tables of the following are also included in the Appendix and present the test data with depth for each test interval:

- Penetration vs. BLC⁴
- Penetration vs. FMX⁵
- Penetration vs. EFV⁶
- Penetration vs. CSX⁷
- Penetration vs. VMX⁸
- Penetration vs. ETR⁹
- ETR vs. Rod Length
- Average ETR vs. Rod Length

¹ Measured with engineer's tape measure.

² Calculated using measured OD and Area from instrument rod calibration record.

³ From instrument rod calibration record.

⁴ BLC - Blow Count per 6-in. increment

⁵ FMX - Maximum Compressive Force

⁶ EFV - Maximum Transferred Energy

⁷ CSX - Maximum Compressive Stress

⁸ VMX - Maximum Velocity

⁹ ETR - Energy Transfer Ratio - Ratio of Calculated Energy to Theoretical Energy of 140 lb hammer falling 30 inches



Table 3-1: Summary of Dynamic Testing Results

Data Set ID	Sample Depth (ft)	Drill Rod Length (ft)	Instrumentation to Sampler Tip Length (ft)	Blows per 6" Increment / N-value	Soil Sample Description (Piedmont Residual)	Avg. BPM	Avg. EFV (ft-lbs)	Avg. ETR (%)
1	48.5 – 50.0	50.0	53.55	6-8-13 / 21	SANDY SILT	58.6	316	90.3
2	53.5 – 55.0	55.0	58.55	6-11-17 / 28	SANDY SILT	58.7	326	93.2
3	56.0 – 57.5	57.5	60.55	7-9-17 / 26	SANDY SILT	58.6	320	91.3
4	58.5 – 60.0	60.0	63.55	15-27-44 / 71	SANDY SILT	58.8	320	91.4
Overall Average						58.7	321	91.6

The overall average transferred hammer energy for the automatic hammer on the CME-550X ATV-mounted drill rig (SN 290593) was 321 foot-pounds, with an average ETR of 91.6%.

4.0 Limitations of Report

This report has been prepared in accordance with generally accepted geotechnical engineering practice for specific application to this project. The conclusions contained in this report were based on the applicable standards of our profession in this geographic area at the time this report was prepared. No other warranty, express or implied, is made.



5.0 Closing

S&ME appreciates the opportunity to provide this report to the North Carolina Department of Transportation, Geotechnical Engineering Unit. Please let us know if you have any questions concerning this report.

Sincerely,

S&ME, Inc.

A handwritten signature in black ink, appearing to read "GJ".

Joseph R. Williamson, P.E.
Project Manager
N.C. Registration No. 42168

Gregory J. Canivan, P.E.
Technical Principal

Appendices:

- Appendix I - Certificates of Proficiency
- Appendix II - Instrumented Rod and Accelerometer Calibration Sheets
- Appendix III - SPT Energy Evaluation Form (Field Log)
- Appendix IV - CME-550X ATV (SN 290593) SPT Energy Measurements Summary Plots and Tables

Appendices

Appendix I- Certificate of Proficiency



This documents that

**Joseph Williamson
S&ME, Inc.**



has on March 16, 2022 achieved the rank of

MASTER

on the Dynamic Measurement and Analysis Proficiency Test.

The individual identified on this document demonstrated to the degree granted above an understanding of theory, data quality evaluation, interpretation and signal matching for high strain dynamic testing of deep foundations. ***It is recommended that individuals at the Master level seek to attain Expert level through additional study within eight years of the date of this document***

The ability of the individual named to provide appropriate knowledge and advice on a specific project is not implied or warranted by the Pile Driving Contractors Association or Pile Dynamics, Inc. The Pile Driving Contractors Association or Pile Dynamics, Inc. assumes no liability for foundation testing and analysis work performed by the bearer of this certificate. This certificate can be verified at www.PDAproficiencytest.com.

A handwritten signature in blue ink that reads "Frank T. Peters".

Frank T. Peters, Executive Director
Pile Driving Contractors Association



A handwritten signature in blue ink that reads "Garland Likins".

Garland Likins, Senior Partner
Pile Dynamics, Inc.

No. 3251

Appendix II - Calibration Sheets

Accelerometer Calibration Certificate

Pile Dynamics, Inc.



Calibrated by Pile Dynamics, Inc.
Calibration performed on 17Aug2023

Serial No: K4664 Temperature: 77.6 °F

Model: PR Humidity: 51%

Calibrated on: Channel 3 on 8G 5161 LE

PDA CALIBRATION FACTOR

376.6 mv/5000g
(75.3 μ v/g)
 $R^2: 0.999955$ [Chip programmed]

Operator: William Johnson

Ref Acc 1: 72505!
1035 g's/volt

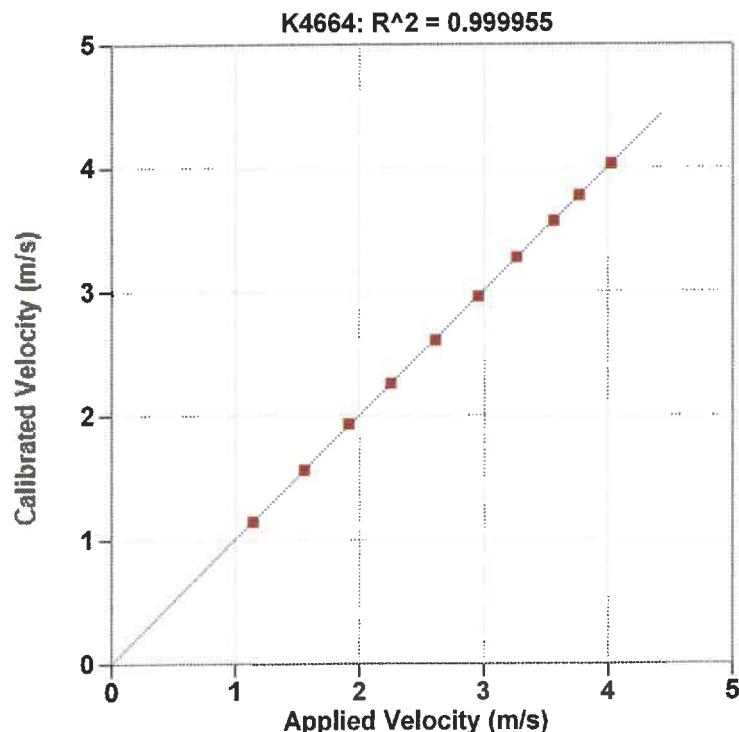
Cal on: 24Mar2022

Ref Acc 2: 72517!
1049 g's/volt

Cal on: 24Mar2022

Signed

Reference accelerometer calibrations are traceable to
the United States National Institute of Standards and
Technology (NIST).



Reference Velocity	S/N K4664 Velocity
m/s	m/s
1.146	1.143
1.560	1.559
1.915	1.932
2.255	2.258
2.612	2.606
2.962	2.958
3.270	3.273
3.569	3.566
3.772	3.773
4.030	4.027

Maximum Acceleration: 879 g's

Accelerometer Calibration Certificate

Pile Dynamics, Inc.



Calibrated by Pile Dynamics, Inc.
Calibration performed on 17Aug2023

Serial No: K4665 Temperature: 77.6 °F PDA CALIBRATION FACTOR

Model: PR Humidity: 51% 375.3 mv/5000g
(75.1 μ v/g)
R²: 0.999957 [Chip programmed]

Calibrated on: Channel 3 on 8G 5161 LE

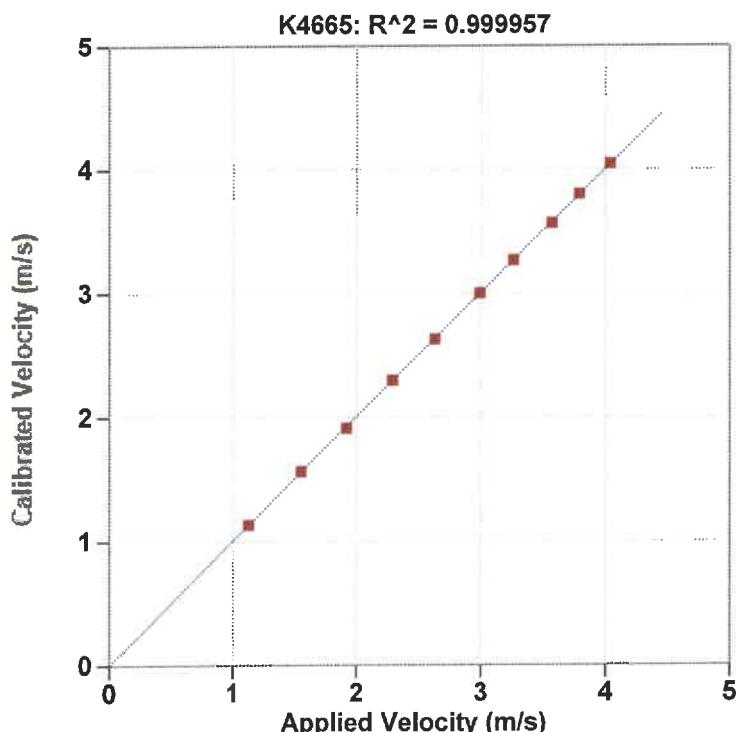
Ref Acc 1: 72505!
1035 g's/volt Cal on: 24Mar2022

Ref Acc 2: 72517!
1049 g's/volt Cal on: 24Mar2022

Operator: William Johnson


Signed

Reference accelerometer calibrations are traceable to
the United States National Institute of Standards and
Technology (NIST).



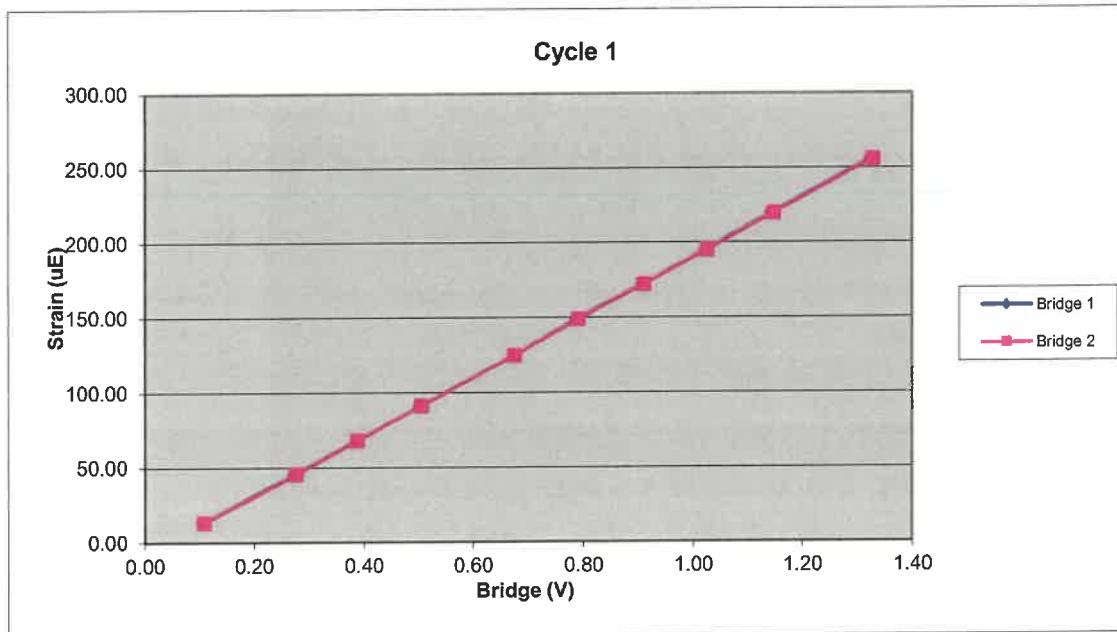
Reference Velocity	S/N K4665 Velocity
m/s	m/s
1.129	1.131
1.555	1.560
1.922	1.910
2.291	2.295
2.633	2.627
2.994	2.999
3.262	3.264
3.573	3.564
3.791	3.797
4.038	4.041

Maximum Acceleration: 880 g's

203AWJ		Cycle 1		
Sample	Force (lb)	Strain (μE)	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	819.88	13.18	0.11	0.11
3	2100.72	45.33	0.27	0.28
4	2947.11	68.12	0.39	0.39
5	3827.72	90.98	0.50	0.51
6	5122.01	124.83	0.67	0.68
7	5996.48	148.92	0.79	0.79
8	6896.87	172.25	0.91	0.91
9	7771.24	195.27	1.02	1.03
10	8694.53	219.87	1.15	1.15
11	10075.00	255.83	1.33	1.33

Bridge 1	Bridge 2
Force Calibration (lb/V)	7576.32
Offset	14.17
Correlation	0.999999
Strain Calibration ($\mu\text{E}/\text{V}$)	199.46
Offset	-9.00
Correlation	0.999979
Force Calibration (lb/V)	7575.14
Offset	2.97
Correlation	0.999999
Strain Calibration ($\mu\text{E}/\text{V}$)	199.43
Offset	-9.29
Correlation	0.999982

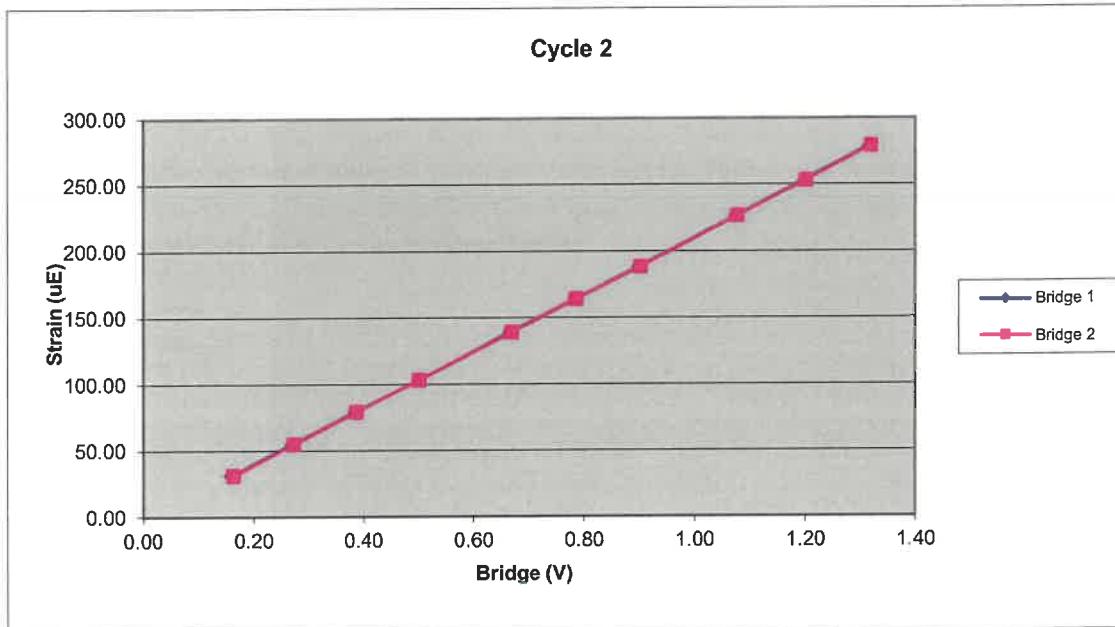
Force Strain Calibration
EA (Kips)
37982.46
Offset
356.04
Correlation
0.999980



203AWJ		Cycle 2		
Sample	Force (lb)	Strain (μE)	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	1217.00	30.72	0.16	0.16
3	2060.56	54.45	0.27	0.27
4	2939.22	78.94	0.39	0.39
5	3811.73	102.81	0.50	0.50
6	5082.83	138.71	0.67	0.67
7	5976.20	163.65	0.78	0.79
8	6861.10	187.95	0.90	0.90
9	8194.67	226.13	1.08	1.08
10	9130.84	252.84	1.20	1.20
11	10039.52	278.74	1.32	1.32

Bridge 1		Bridge 2	
Force Calibration (lb/V)	7616.13	Force Calibration (lb/V)	7615.56
Offset	1.43	Offset	-11.88
Correlation	0.999999	Correlation	0.999997
Strain Calibration ($\mu\text{E}/\text{V}$)	213.80	Strain Calibration ($\mu\text{E}/\text{V}$)	213.79
Offset	-3.74	Offset	-4.12
Correlation	0.999987	Correlation	0.999990

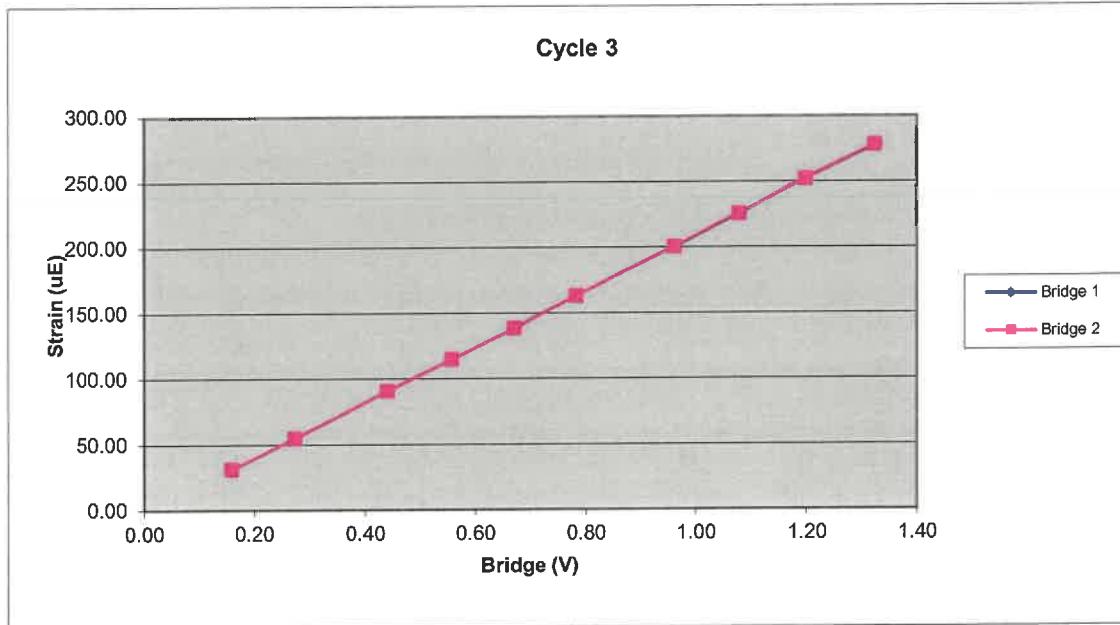
Force Strain Calibration	
EA (Kips)	35621.25
Offset	134.95
Correlation	0.999985



203AWJ		Cycle 3		
Sample	Force (lb)	Strain (μE)	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	1216.12	31.38	0.16	0.16
3	2078.01	54.75	0.27	0.27
4	3348.13	90.71	0.44	0.44
5	4248.62	114.98	0.56	0.56
6	5110.90	138.68	0.67	0.67
7	5966.16	163.47	0.78	0.78
8	7338.73	200.80	0.96	0.96
9	8226.55	225.96	1.08	1.08
10	9144.10	252.26	1.20	1.20
11	10093.62	278.03	1.32	1.32

Bridge 1		Bridge 2	
Force Calibration (lb/V)	7621.84	Force Calibration (lb/V)	7635.13
Offset	-0.64	Offset	-3.95
Correlation	0.999999	Correlation	0.999999
Strain Calibration ($\mu\text{E}/\text{V}$)	212.12	Strain Calibration ($\mu\text{E}/\text{V}$)	212.49
Offset	-2.91	Offset	-3.01
Correlation	0.999979	Correlation	0.999985

Force Strain Calibration	
EA (Kips)	35930.12
Offset	104.27
Correlation	0.999985



Bridge Excitation (V) 5
Shunt Resistor (ohm) 60.4k

Calibration Factors	203AWJ		
Bridge 1 (μ E/V)	208.46	Bridge 2 (μ E/V)	208.57
EA Factor (Kips)	36511.28	Area (in ²)	1.22

Calibrated by: Sean Bang
Calibrated Date: 8/24/2023

Pile Dynamics Inc
30725 Aurora Rd
Solon, OH 44139

Traceable to N.I.S.T.

Appendix III – Field Log



SPT Energy Evaluation Form

Project: I-77 EXIST ZG PHASE I
 Project No.: 23610178A
 Boring No.: TEST ITOLE A

Date: 11/17/23
 Weather: CLEAR 70°
 Drill Rod Type: 5' LONG AW3

On-site Personnel

Drilling Company: SIME
 Rig Operator: L. SARADER
 Engr/Geologist: N/A
 Client Rep.: N/A
 Analyzer Oper.: J. WILLIAMSON

Rig/Hammer Info

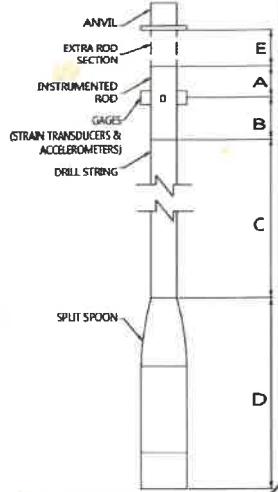
Drill Rig Make/Model: CME-550X
 Carrier Type: ATV
 Rig Serial No.: 290593 (R-49)
 Hammer Type/Model: AUTO / CME
 Hammer Serial No.:
 Hammer Drop System: CHAIN DRIVE
 Lubrication Condition: PER MANUFACTURER REC.

Manufacturer Recommended

Operation Rate (bpm): 50-55
 Typical Drop Height (in.): 30
 Typical Hammer Weight (lbs): 140
 Anvil Dimension (in.): 12
 Drilling Method: 2.5 ft HSA
 Drop Height in Tolerance (y/n) Y

Rod Info

(A) + (B) Instr. Rod Length: 7.0 ft
 (B) Instr. Rod Length below Gages: 0.7 ft
 (D) Spoon Length: 2.85 ft
 (E) Rod Length Above Instr. Rod (if applicable): 0 ft
 (B)+(C)+(D) (LE) - Length Below Gauges (C) + 3.55 ft
 Instr. Rod S/N: 203 AW3
 Instr. Rod Outside Dia.: 1.75 in.
 Instr. Rod Area: 1.22 in²
 PDA Make/Model: PDI / PAY
 PDA Serial No.: 3733L
 Calib. Pulse Test (y/n): Y



Gage Info

Gage		Serial No.	Calibration No.
Accel.	A3	K 4664	376.4
	A4	K 4665	375.3
Strain	F3	C03 AW3-1	208.46
	F4	C03 AW3-2	208.57

Date of Test	Test Depth Increment (ft to ft)	Test Time Start / Stop (military)	Length of Drill String (ft) (C)	(LE) Length below Gages (ft) (B) + (C) + (D)	Avg. Meas. Hammer Rate (BPM)	SPT Blow Counts						AASHTO / USCS Classification
						Total Blows by PDA	6"	12"	18"	N-Value	Extra Blows	
11/17/23	385-40.0	11:01	39	42.55			25	26	50+	100+		
	435-45	11:19	45	48.55		97	14	35	50.63	100+		
	485-50.0	11:34	50	53.55		27	6	8	13	21	0	
	53.5-55.0	11:48	55	58.55		34	6	11	17	28	0	
	56.0-57.5	12:05	57	60.55		33	7	9	17	26	0	
	585-60.0	12:18	60	63.55		86	15	27	44	71	0	

Notes: FZ SPIKING ON FIRST SAMPLE, SWAPPED OUT PICTAIL. ALSO SEVERAL BAD ISLOWS RECORDS B, PDA
 " LAST SAMPLE.

NOTE: (1) Note any unusual hammer operating conditions that affect the hammer performance, or changes in operating conditions (e.g. veritcality, weather, or lubrication between trials). (2) Note any changes in rod diameter along drill string and record locations of short rod sections.

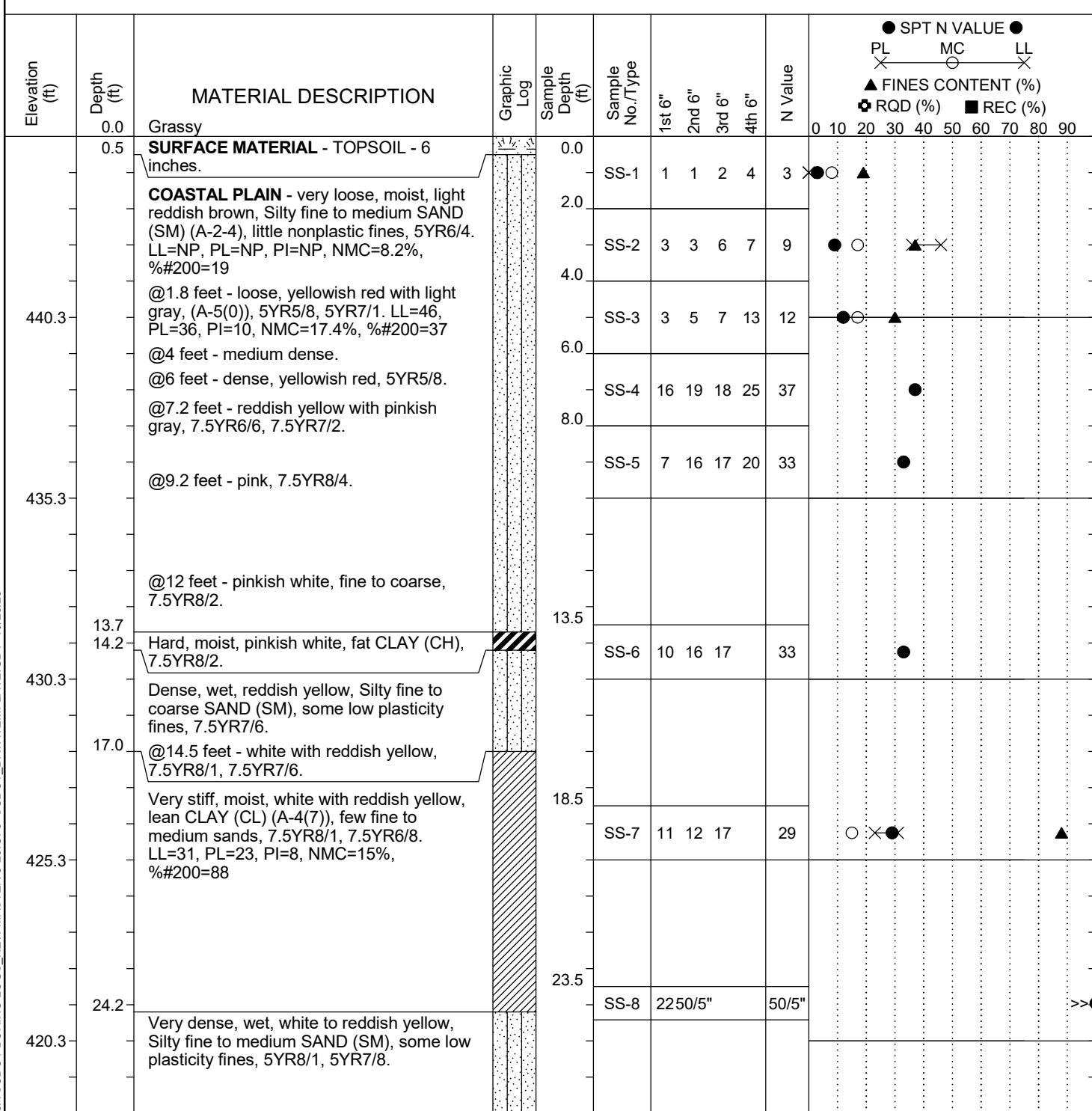
Joseph Wilson

11/17/23

Prepared By (print/signature)

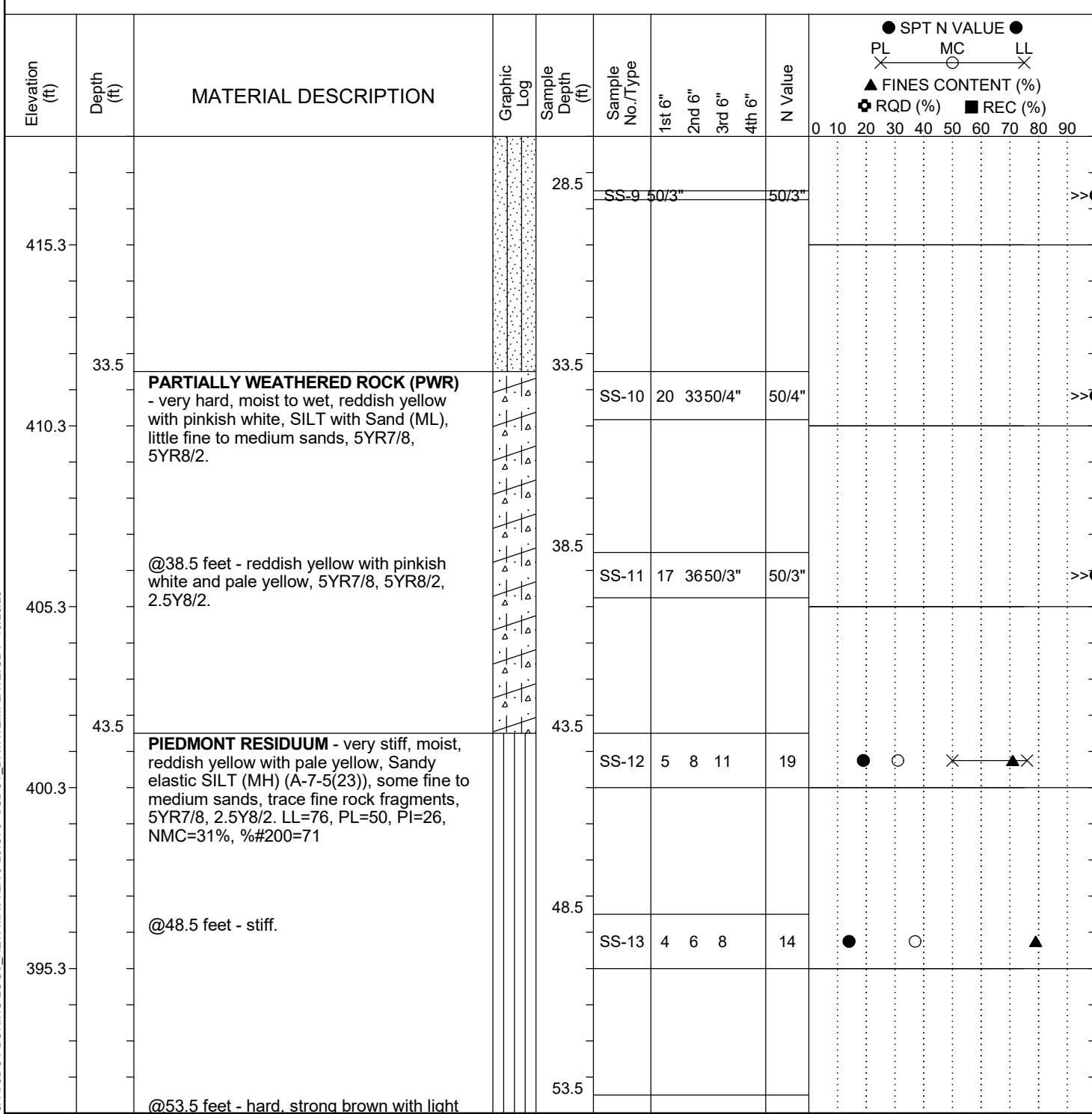
Date

Project ID:	23610178A			County:	Richland			Boring No.:	EB-1W
Site Description:	I-77 Exit 26 Phase I							Route:	US-21
Eng./Geo.:	S. Melecosky		Boring Location:			Offset:			Alignment: Proposed
Elev.:	445.3 ft		Latitude:	34.18986277		Longitude:	-80.97066934		Date Started: 7/19/2023
Total Depth:	89.6 ft		Soil Depth:	71.6 ft		Core Depth:	18 ft		Date Completed: 7/21/2023
Bore Hole Diameter (in):	4		Sampler Configuration		Liner Required:		Y (N)	Liner Used:	
Drill Machine:	CME-550X		Drill Method:	RW/RC		Hammer Type:	Automatic		Energy Ratio: 81.6%
Core Size:	NQ		Driller:	S. Gowan		Groundwater:	TOB	NA	24HR NA

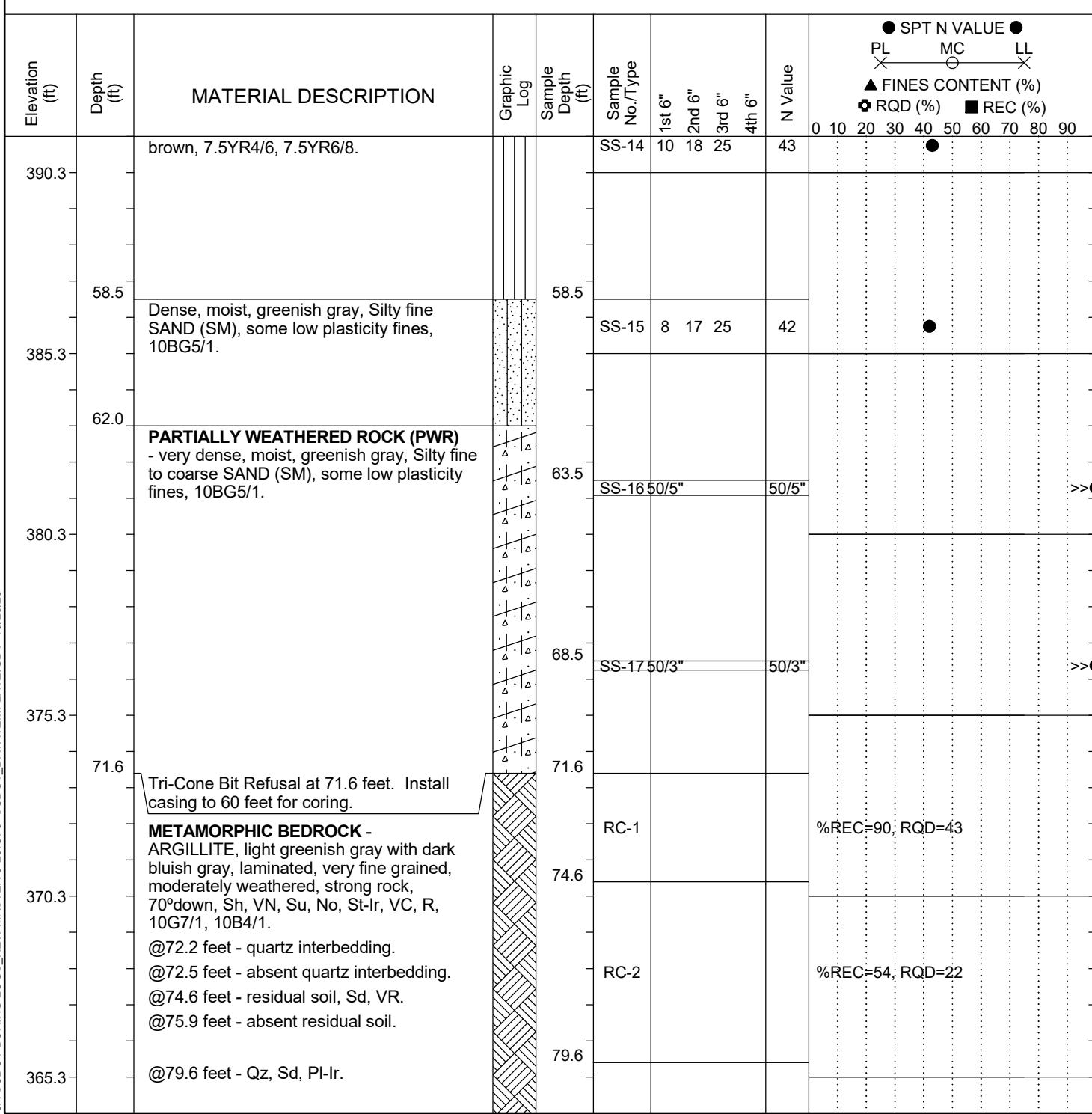


SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	23610178A			County:	Richland		Boring No.:	EB-1W
Site Description:	I-77 Exit 26 Phase I						Route:	US-21
Eng./Geo.:	S. Melecosky		Boring Location:			Offset:		
Elev.:	445.3 ft		Latitude:	34.18986277		Longitude:	-80.97066934	
Total Depth:	89.6 ft		Soil Depth:	71.6 ft		Core Depth:	18 ft	
Bore Hole Diameter (in):	4		Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)
Drill Machine:	CME-550X	Drill Method:	RW/RC	Hammer Type:	Automatic	Energy Ratio:	81.6%	
Core Size:	NQ	Driller:	S. Gowan	Groundwater:	TOB	NA	24HR	NA



Project ID:	23610178A			County:	Richland		Boring No.:	EB-1W
Site Description:	I-77 Exit 26 Phase I						Route:	US-21
Eng./Geo.:	S. Melecosky		Boring Location:			Offset:		
Elev.:	445.3 ft		Latitude:	34.18986277		Longitude:	-80.97066934	
Total Depth:	89.6 ft		Soil Depth:	71.6 ft		Core Depth:	18 ft	
Bore Hole Diameter (in):	4		Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)
Drill Machine:	CME-550X	Drill Method:	RW/RC	Hammer Type:	Automatic	Energy Ratio:	81.6%	
Core Size:	NQ	Driller:	S. Gowan	Groundwater:	TOB	NA	24HR	NA

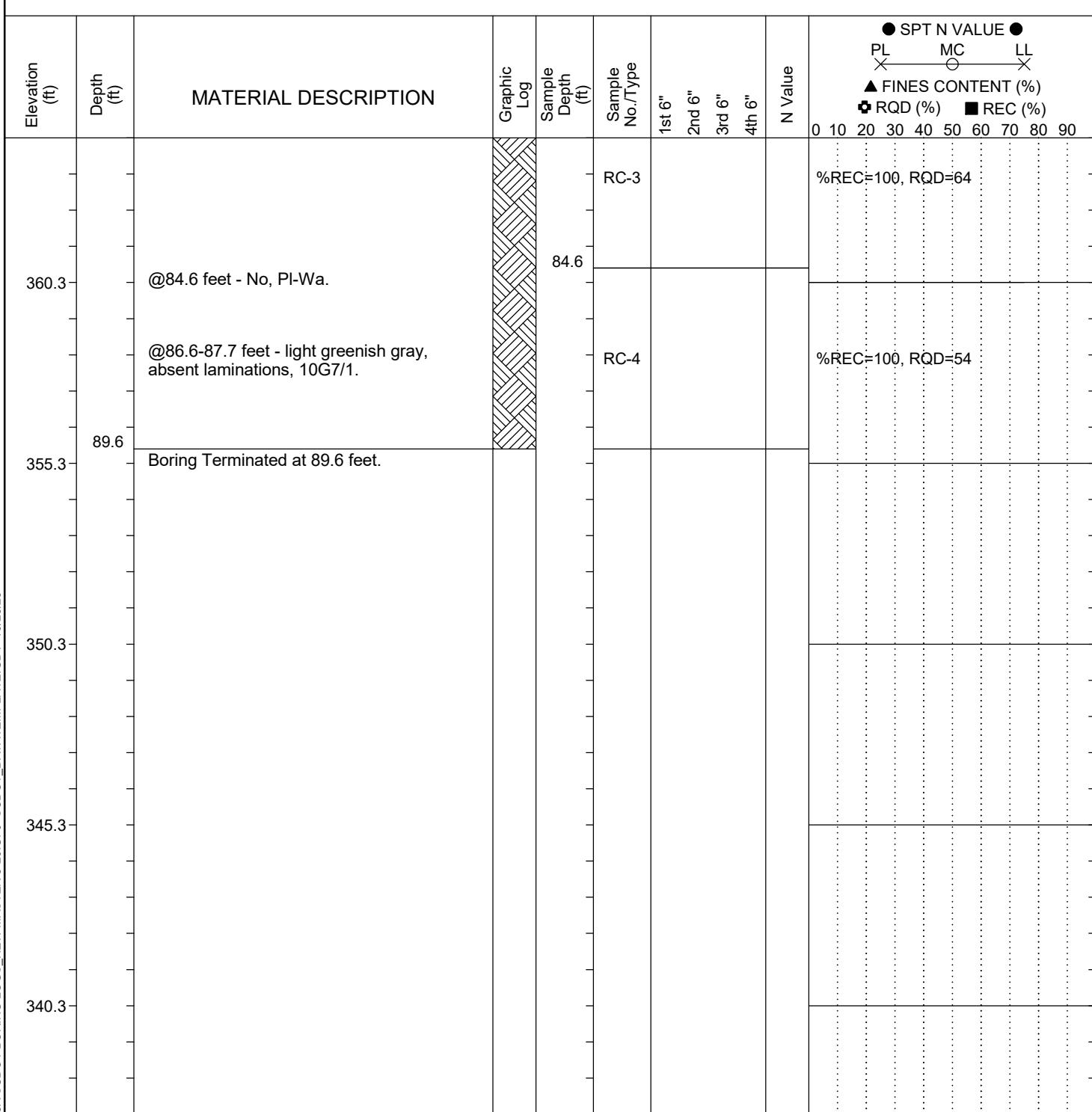


LEGEND

Continued Next Page

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	23610178A			County:	Richland		Boring No.:	EB-1W
Site Description:	I-77 Exit 26 Phase I						Route:	US-21
Eng./Geo.:	S. Melecosky		Boring Location:			Offset:		
Elev.:	445.3 ft		Latitude:	34.18986277		Longitude:	-80.97066934	
Total Depth:	89.6 ft		Soil Depth:	71.6 ft		Core Depth:	18 ft	
Bore Hole Diameter (in):	4		Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)
Drill Machine:	CME-550X	Drill Method:	RW/RC	Hammer Type:	Automatic	Energy Ratio:		81.6%
Core Size:	NQ	Driller:	S. Gowan	Groundwater:	TOB	NA	24HR	NA



LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Appendix IV – SPT Energy Measurement Plots and Tables



Pile Dynamics, Inc. - PDIPILOT2 Ver 2022.1.62.0 - Case Method & iCAP® Results

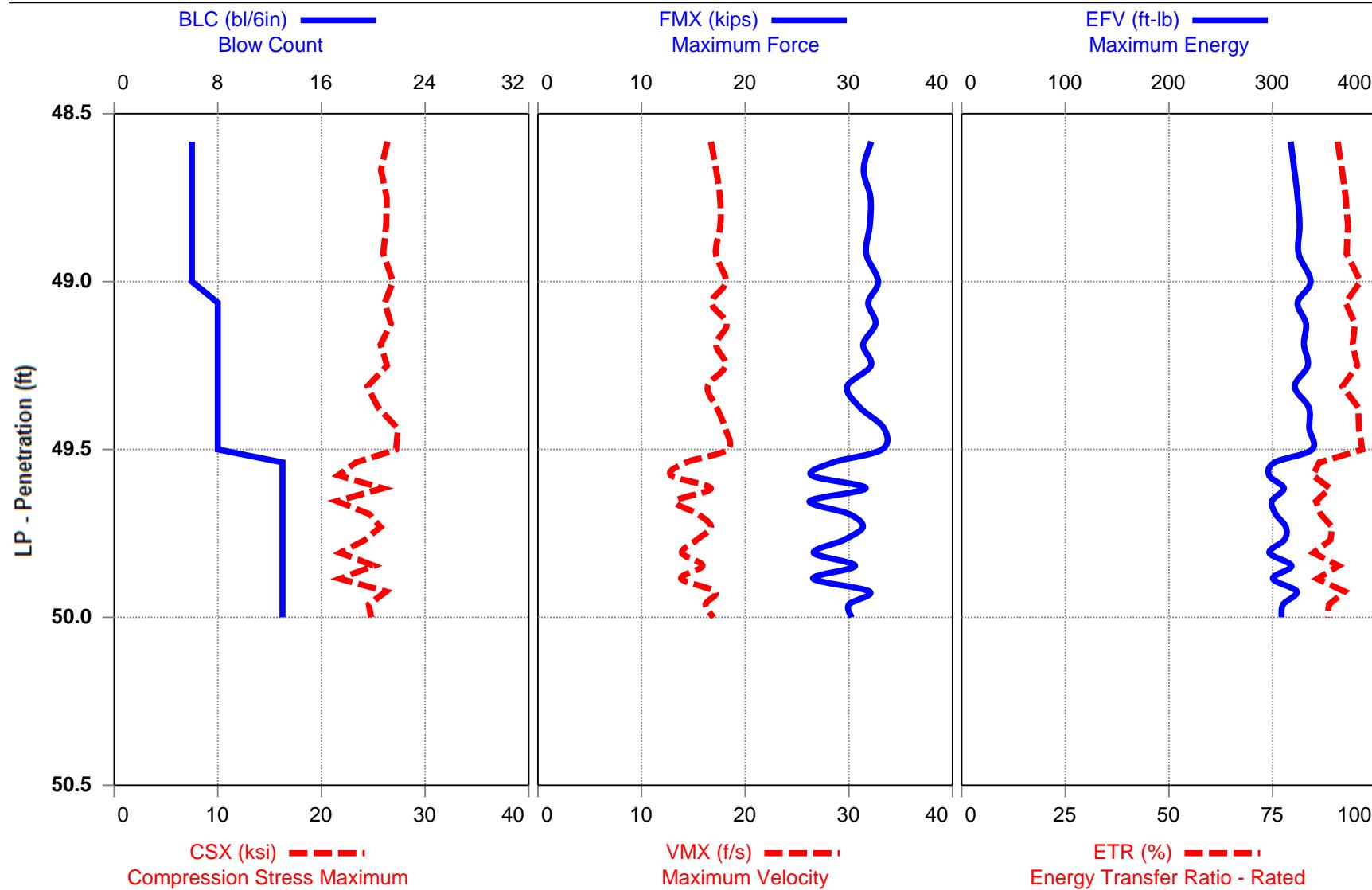
Printed: 20-December-2023

Test started: 17-November-2023



CME-550X SN 290593 - 48.5-50.0 FEET

TEST HOLE A



CME-550X SN 290593

JRW

TEST HOLE A

AR: 1.22 in²

LE: 53.55 ft

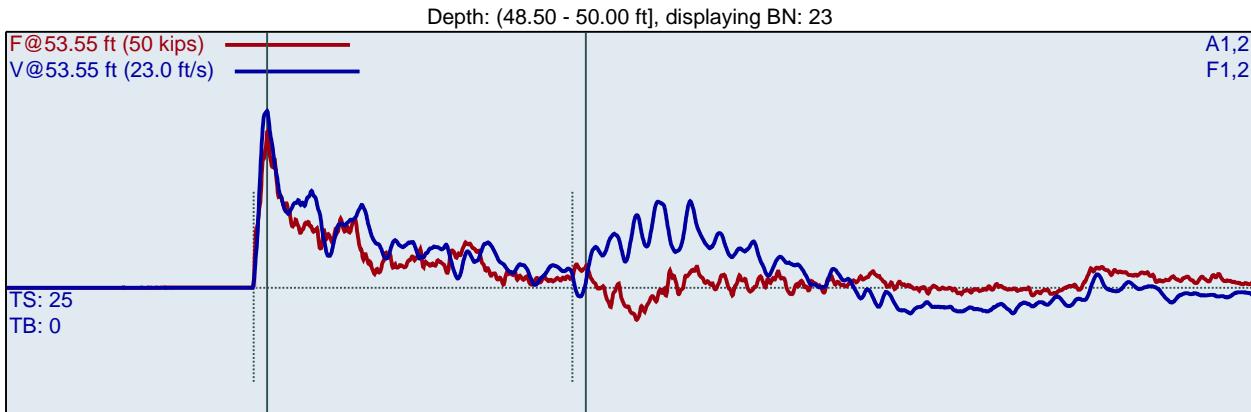
WS: 16807.9 ft/s

48.5-50.0 FEET

Interval start: 11/17/2023

SP: 0.492 k/ft³

EM: 30000 ksi



F1 : [203 AWJ-1] 208.46 PDICAL (1) FF1
F2 : [203 AWJ-2] 208.57 PDICAL (1) FF1

A1 (PR): [K4664] 376.6 mv/6.4v/5000g (1) VF1
A2 (PR): [K4665] 375.3 mv/6.4v/5000g (1) VF1

BPM: Blows/Minute

CSX: Compression Stress Maximum

FMX: Maximum Force

DFN: Final Displacement

VMX: Maximum Velocity

EFV: Maximum Energy

DMX: Maximum Displacement

ETR: Energy Transfer Ratio - Rated

BL#	LP ft	BC /6"	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
1	48.58	6	1.9	32	16.7	1.00	26.4	1.00	317	90.6
2	48.67	6	58.6	31	17.2	1.03	25.7	1.01	321	91.7
3	48.75	6	58.1	32	17.6	1.00	26.3	1.00	324	92.6
4	48.83	6	58.6	32	17.6	1.00	26.2	1.00	326	93.1
5	48.92	6	57.9	32	17.2	1.00	26.0	1.00	325	92.8
6	49.00	6	58.8	33	18.1	1.00	26.9	1.00	337	96.2
7	49.06	8	58.1	32	16.8	0.76	26.1	0.75	324	92.5
8	49.13	8	59.0	33	18.2	0.75	26.7	0.75	332	94.8
9	49.19	8	58.1	31	17.2	0.78	25.7	0.75	330	94.3
10	49.25	8	58.7	32	18.1	0.78	26.3	0.75	334	95.4
11	49.31	8	58.5	30	16.4	0.81	24.4	0.75	321	91.8
12	49.38	8	58.9	31	17.3	0.75	25.5	0.75	335	95.7
13	49.44	8	58.5	33	18.1	0.77	27.4	0.75	335	95.8
14	49.50	8	58.7	33	18.3	0.77	27.2	0.75	338	96.6
15	49.54	13	58.6	28	14.3	0.55	23.3	0.47	302	86.3
16	49.58	13	58.5	26	12.8	0.57	21.6	0.46	296	84.7
17	49.62	13	59.0	32	16.7	0.52	25.9	0.46	311	88.8
18	49.65	13	58.4	26	13.3	0.55	21.5	0.46	299	85.4
19	49.69	13	58.8	30	15.4	0.51	24.6	0.46	303	86.5
20	49.73	13	58.8	31	16.7	0.54	25.7	0.46	313	89.3
21	49.77	13	58.3	30	15.3	0.55	24.2	0.46	311	88.9
22	49.81	13	59.0	27	13.9	0.52	21.8	0.46	297	84.8
23	49.85	13	58.3	31	15.9	0.55	25.1	0.46	318	90.9
24	49.88	13	59.1	27	13.8	0.52	21.8	0.46	300	85.7
25	49.92	13	58.3	32	17.1	0.55	26.2	0.46	323	92.3
26	49.96	13	58.8	30	16.2	0.52	24.6	0.46	310	88.6
27	50.00	13	58.3	30	16.9	0.51	24.8	0.46	309	88.1

S&ME, Inc.
SPT Analyzer Results

Page 2 of 10
PDA-S Ver. 2022.35.2 - Printed: 12/19/2023

Average	58.6	30	16.1	0.63	24.8	0.57	316	90.3
Std Dev	0.3	2	1.6	0.12	1.8	0.14	14	3.9
Maximum	59.1	33	18.3	0.81	27.4	0.75	338	96.6
Minimum	58.1	26	12.8	0.51	21.5	0.46	296	84.7

N-value: 21

Sample Interval Time: 26.58 seconds.



Pile Dynamics, Inc. - PDIPILOT2 Ver 2022.1.62.0 - Case Method & iCAP® Results

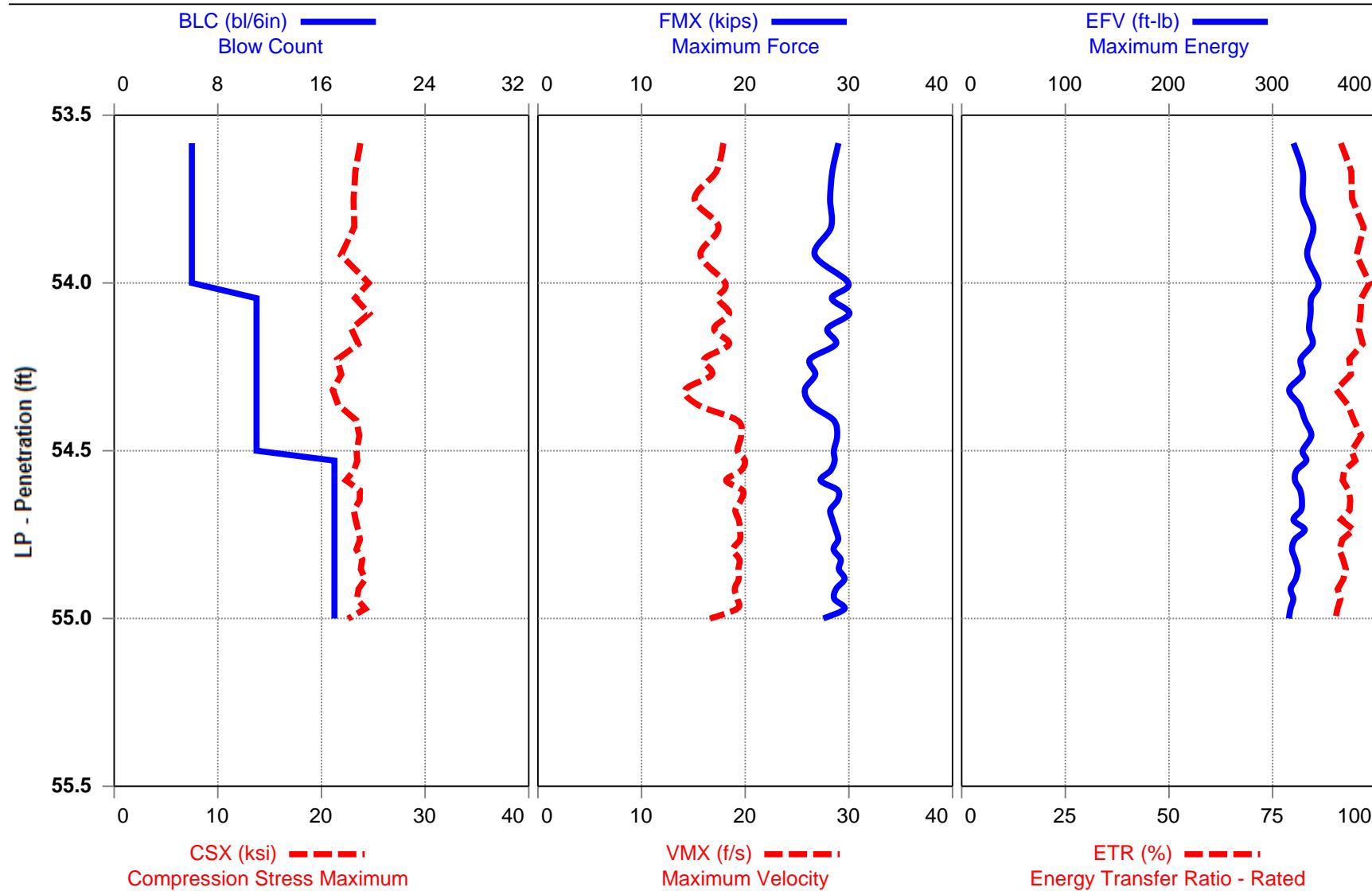
Printed: 20-December-2023

Test started: 17-November-2023



CME-550X SN 290593 - 53.5-55.0 FEET

TEST HOLE A



CME-550X SN 290593

JRW

TEST HOLE A

AR: 1.22 in²

LE: 58.55 ft

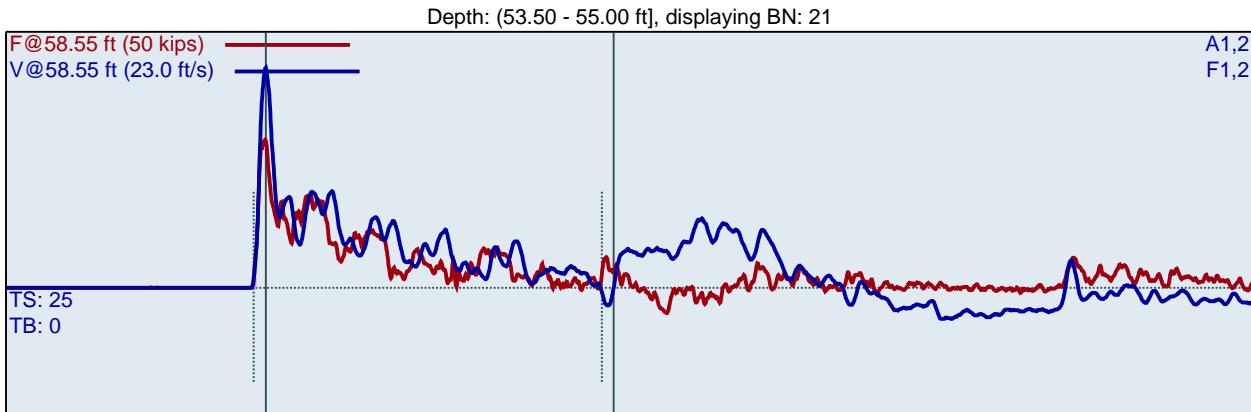
WS: 16807.9 ft/s

48.5-50.0 FEET

Interval start: 11/17/2023

SP: 0.492 k/ft³

EM: 30000 ksi



F1 : [203 AWJ-1] 208.46 PDICAL (1) FF1
F2 : [203 AWJ-2] 208.57 PDICAL (1) FF1

A1 (PR): [K4664] 376.6 mv/6.4v/5000g (1) VF1
A2 (PR): [K4665] 375.3 mv/6.4v/5000g (1) VF1

BL#	LP ft	BC /6"	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
1	53.58	6	1.9	29	17.9	1.15	23.8	1.01	320	91.4
2	53.67	6	58.7	28	17.2	1.01	23.3	1.00	329	94.0
3	53.75	6	58.6	28	15.1	1.01	23.1	1.00	329	94.1
4	53.83	6	58.5	28	17.4	1.00	23.2	1.00	339	96.9
5	53.92	6	58.4	27	15.7	1.01	21.9	1.00	333	95.2
6	54.00	6	58.9	30	18.1	1.00	24.6	1.00	344	98.3
7	54.05	11	58.2	28	17.4	0.78	23.2	0.55	337	96.3
8	54.09	11	59.3	30	18.5	0.68	24.6	0.55	337	96.2
9	54.14	11	58.4	28	17.0	0.67	22.9	0.54	335	95.7
10	54.18	11	58.9	29	18.4	0.65	23.6	0.55	338	96.7
11	54.23	11	58.6	26	16.0	0.62	21.5	0.55	327	93.4
12	54.27	11	58.9	27	16.8	0.61	21.9	0.54	329	93.9
13	54.32	11	58.9	26	14.2	0.60	21.1	0.55	316	90.3
14	54.36	11	58.7	26	15.5	0.63	21.6	0.54	326	93.1
15	54.41	11	58.9	29	19.2	0.61	23.4	0.54	331	94.6
16	54.45	11	58.5	29	19.6	0.60	23.7	0.55	337	96.3
17	54.50	11	59.1	29	19.3	0.60	23.4	0.54	329	94.0
18	54.53	17	58.6	29	20.0	0.53	23.5	0.35	332	94.9
19	54.56	17	59.0	28	19.6	0.53	23.1	0.35	323	92.2
20	54.59	17	58.6	27	18.2	0.53	22.4	0.35	322	91.9
21	54.62	17	58.6	29	19.7	0.51	23.7	0.35	327	93.3
22	54.65	17	58.9	29	19.6	0.52	23.7	0.35	328	93.7
23	54.68	17	58.6	28	19.0	0.51	23.1	0.35	327	93.5
24	54.71	17	59.2	28	19.4	0.50	23.3	0.35	320	91.5
25	54.74	17	58.4	29	19.5	0.51	23.5	0.35	331	94.6
26	54.76	17	59.1	29	19.5	0.50	23.7	0.35	321	91.8
27	54.79	17	58.4	29	18.8	0.49	23.4	0.35	319	91.0
28	54.82	17	58.9	29	19.4	0.48	23.9	0.35	322	91.9
29	54.85	17	58.7	29	19.3	0.49	23.8	0.35	324	92.6
30	54.88	17	58.5	30	19.4	0.48	24.2	0.35	322	92.1
31	54.91	17	58.9	29	19.0	0.48	23.6	0.35	317	90.6

32	54.94	17	58.5	29	19.3	0.48	23.4	0.35	320	91.4
33	54.97	17	59.1	30	19.2	0.47	24.2	0.35	317	90.6
34	55.00	17	58.4	28	16.6	0.48	22.6	0.35	316	90.2
	Average		58.7	28	18.5	0.55	23.2	0.43	326	93.2
	Std Dev		0.3	1	1.5	0.08	0.8	0.09	7	1.9
	Maximum		59.3	30	20.0	0.78	24.6	0.55	338	96.7
	Minimum		58.2	26	14.2	0.47	21.1	0.35	316	90.2
				N-value:	28					

Sample Interval Time: 33.66 seconds.



Pile Dynamics, Inc. - PDIPILOT2 Ver 2022.1.62.0 - Case Method & iCAP® Results

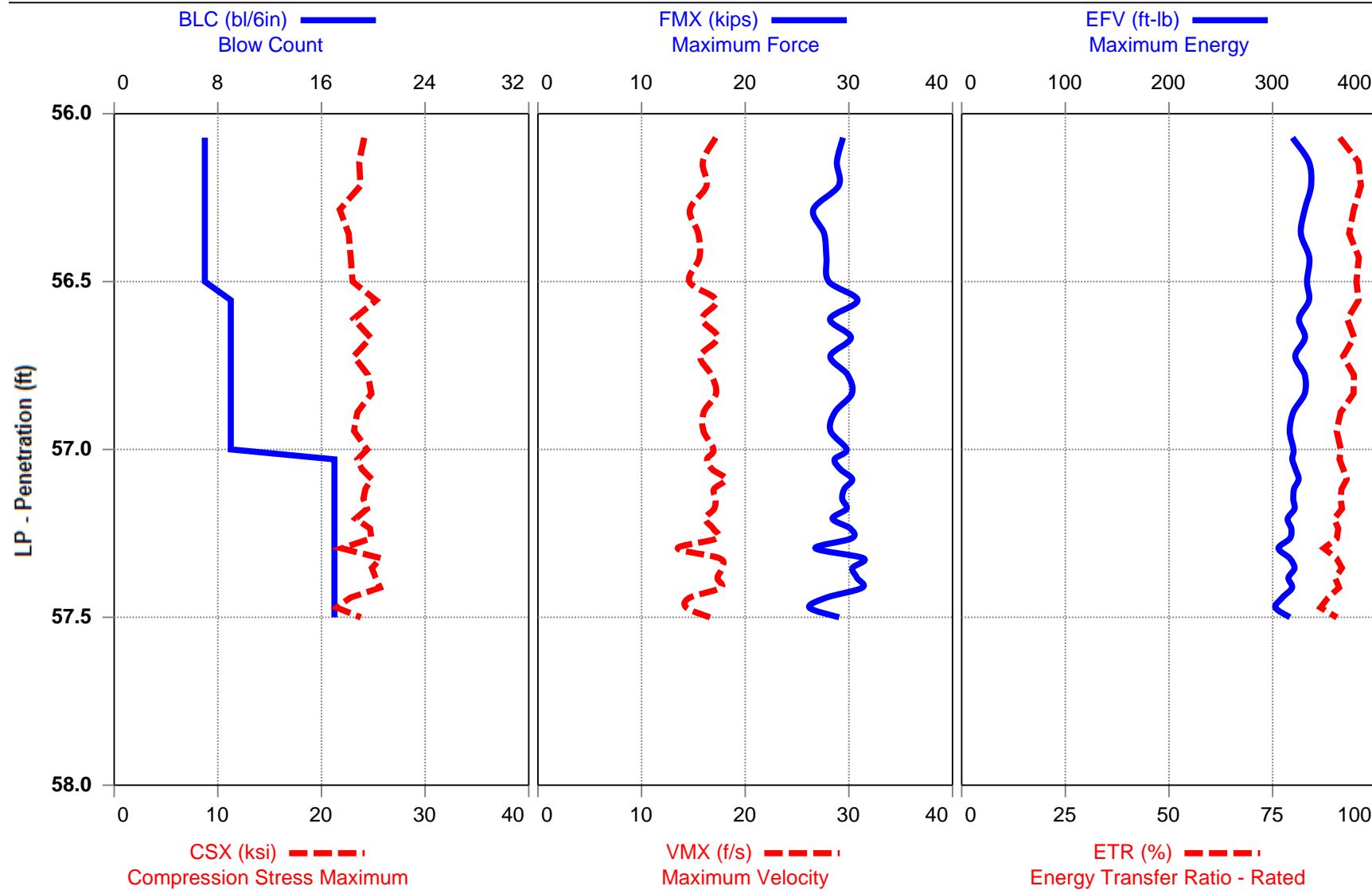
Printed: 20-December-2023

Test started: 17-November-2023



CME-550X SN 290593 - 56.0-57.5 FEET

TEST HOLE A



CME-550X SN 290593

JRW

TEST HOLE A

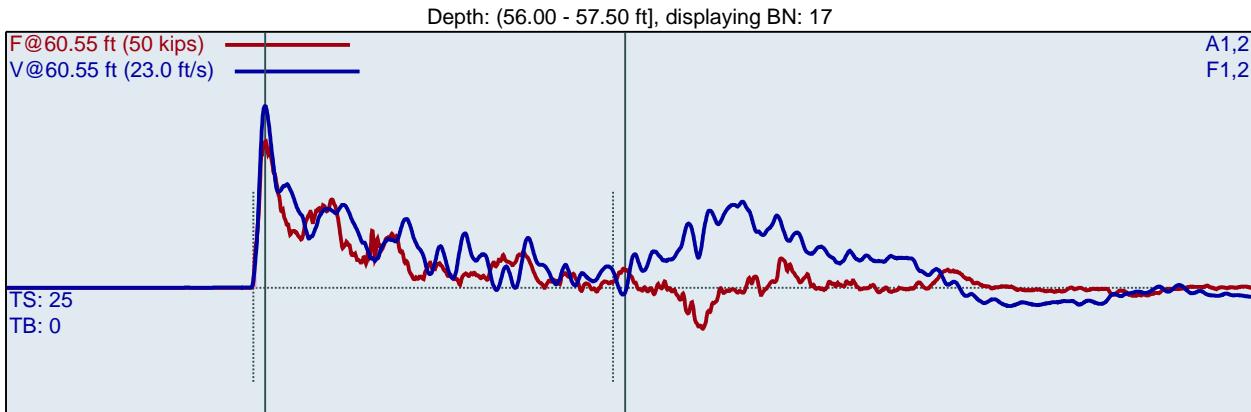
AR: 1.22 in²

LE: 60.55 ft

WS: 16807.9 ft/s

48.5-50.0 FEET
Interval start: 11/17/2023

SP: 0.492 k/ft³
EM: 30000 ksi



F1 : [203 AWJ-1] 208.46 PDICAL (1) FF1
F2 : [203 AWJ-2] 208.57 PDICAL (1) FF1

A1 (PR): [K4664] 376.6 mv/6.4v/5000g (1) VF1
A2 (PR): [K4665] 375.3 mv/6.4v/5000g (1) VF1

BL#	LP ft	BC /6"	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
1	56.07	7	1.9	29	17.1	1.01	24.1	0.86	319	91.1
2	56.14	7	58.0	29	15.9	0.87	23.6	0.86	335	95.6
3	56.21	7	58.3	29	16.3	0.87	23.8	0.86	337	96.3
4	56.29	7	58.3	27	14.7	0.89	21.8	0.86	331	94.5
5	56.36	7	58.8	28	15.5	0.88	22.6	0.86	327	93.4
6	56.43	7	58.3	28	15.6	0.88	22.8	0.86	335	95.8
7	56.50	7	58.6	28	14.6	0.87	23.0	0.86	333	95.2
8	56.56	9	58.4	31	17.2	0.75	25.3	0.66	335	95.7
9	56.61	9	58.9	28	15.8	0.73	23.1	0.67	325	93.0
10	56.67	9	58.3	30	17.3	0.75	24.7	0.66	331	94.6
11	56.72	9	58.8	28	15.7	0.74	23.1	0.67	322	92.0
12	56.78	9	58.3	30	16.7	0.76	24.5	0.67	331	94.6
13	56.83	9	58.6	30	17.2	0.75	24.8	0.67	331	94.5
14	56.89	9	58.7	29	16.0	0.74	23.5	0.67	320	91.4
15	56.94	9	58.4	28	16.0	0.73	23.1	0.67	316	90.4
16	57.00	9	58.8	30	16.9	0.67	24.4	0.67	320	91.4
17	57.03	17	58.5	29	16.3	0.63	23.5	0.36	319	91.1
18	57.06	17	58.8	29	16.8	0.61	23.9	0.35	322	92.0
19	57.09	17	58.4	30	18.1	0.60	24.9	0.35	325	92.9
20	57.12	17	58.9	30	17.0	0.57	24.2	0.35	321	91.6
21	57.15	17	58.5	29	17.1	0.56	24.1	0.36	320	91.4
22	57.18	17	58.8	30	17.0	0.55	24.4	0.35	321	91.7
23	57.21	17	58.7	28	16.1	0.50	23.3	0.35	314	89.8
24	57.24	17	58.7	30	16.9	0.49	24.7	0.35	318	90.8
25	57.26	17	58.9	30	17.3	0.48	24.8	0.35	317	90.5
26	57.29	17	58.5	27	13.5	0.48	21.9	0.35	306	87.3
27	57.32	17	59.1	31	17.5	0.47	25.7	0.35	316	90.4
28	57.35	17	58.3	30	17.7	0.46	24.9	0.35	321	91.7
29	57.38	17	58.9	31	17.3	0.46	25.2	0.35	315	90.1
30	57.41	17	58.6	31	17.6	0.46	25.6	0.35	318	91.0
31	57.44	17	58.5	28	14.6	0.45	22.8	0.36	309	88.3

S&ME, Inc.
SPT Analyzer Results

Page 6 of 10
PDA-S Ver. 2022.35.2 - Printed: 12/19/2023

32	57.47	17	58.7	26	14.3	0.45	21.5	0.35	303	86.5
33	57.50	17	58.7	29	16.6	0.45	23.8	0.35	317	90.5
Average										
Std Dev										
Maximum										
Minimum										
N-value: 26										

Sample Interval Time: 32.73 seconds.



Pile Dynamics, Inc. - PDIPILOT2 Ver 2022.1.62.0 - Case Method & iCAP® Results

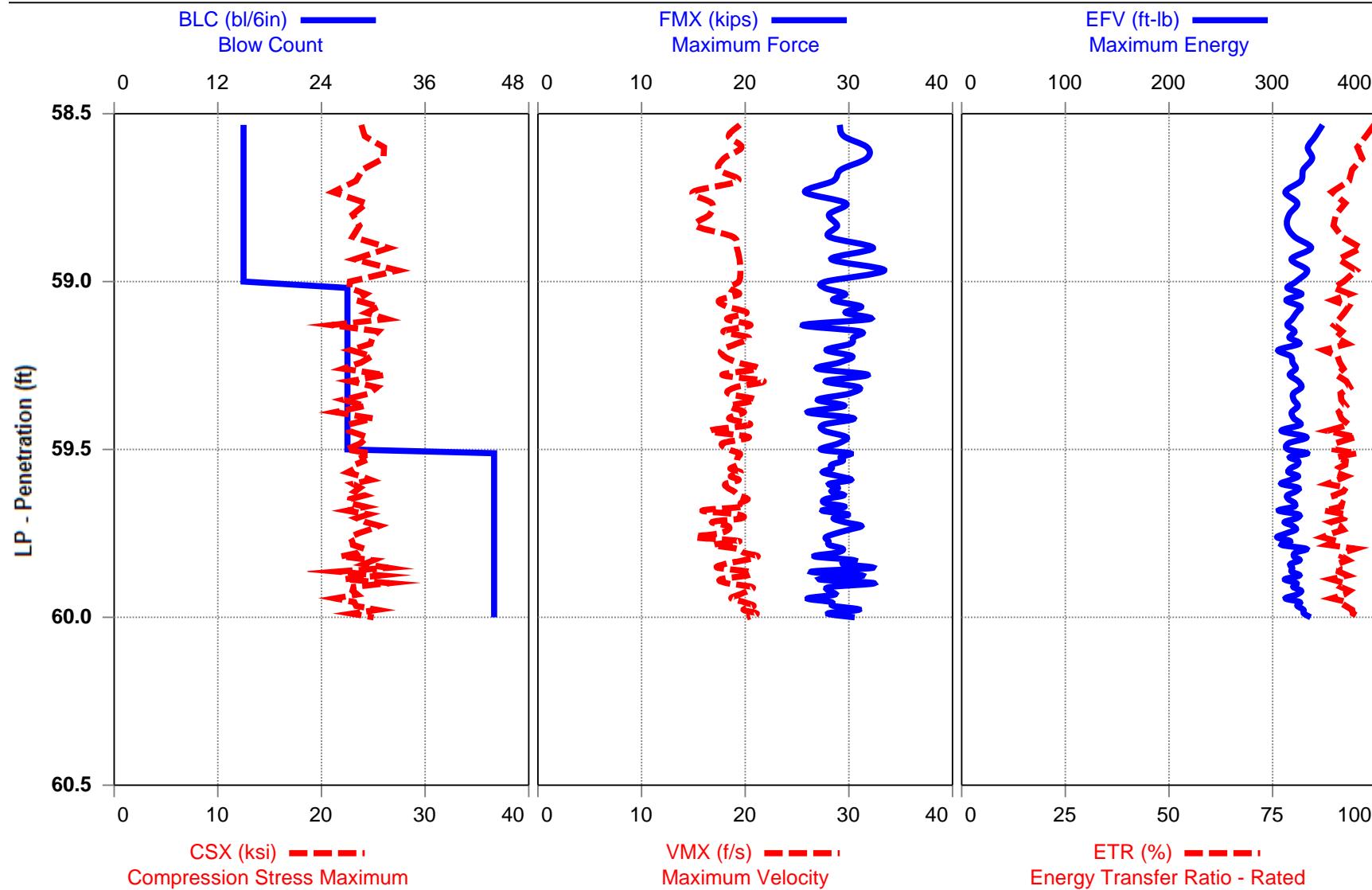
Printed: 20-December-2023

Test started: 17-November-2023



CME-550X SN 290593 - 58.5-60.0 FEET

TEST HOLE A



CME-550X SN 290593

JRW

TEST HOLE A

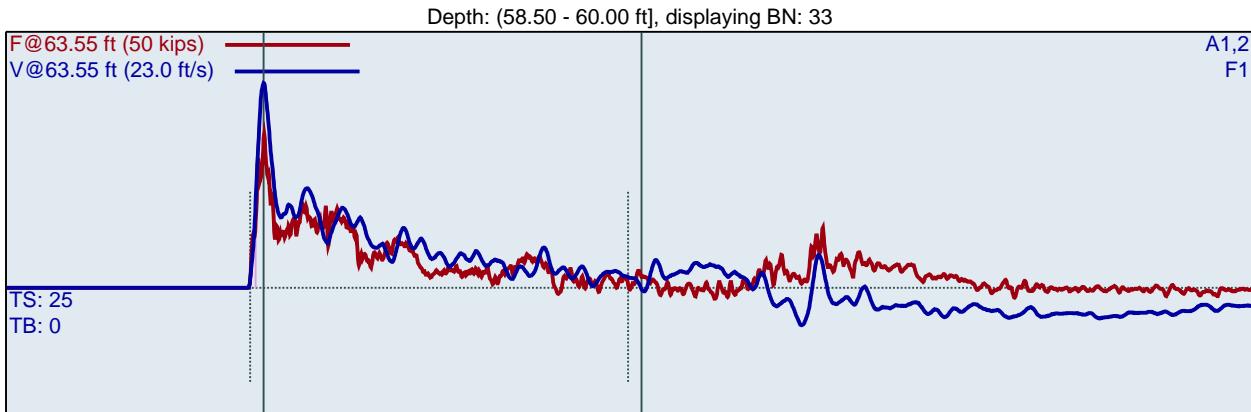
AR: 1.22 in²

LE: 63.55 ft

WS: 16807.9 ft/s

48.5-50.0 FEET
Interval start: 11/17/2023

SP: 0.492 k/ft³
EM: 30000 ksi



F1 : [203 AWJ-1] 208.46 PDICAL (1) FF1
F2 : [203 AWJ-2] 208.57 PDICAL (1) FF1

A1 (PR): [K4664] 376.6 mv/6.4v/5000g (1) VF1
A2 (PR): [K4665] 375.3 mv/6.4v/5000g (1) VF1

BL#	LP ft	BC /6"	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
1	58.53	15	1.9	29	19.5	0.82	23.9	0.40	348	99.4
2	58.57	15	58.1	29	18.4	0.63	24.2	0.40	341	97.5
3	58.60	15	58.8	32	19.6	0.57	26.0	0.40	334	95.4
4	58.63	15	58.4	32	17.9	0.58	26.0	0.40	338	96.6
5	58.67	15	59.0	29	17.4	0.56	24.0	0.40	329	94.1
6	58.70	15	59.1	28	19.3	0.54	23.3	0.40	327	93.5
7	58.73	15	58.3	26	15.0	0.53	21.1	0.40	312	89.2
8	58.77	15	59.2	30	16.8	0.52	24.4	0.40	324	92.5
9	58.80	15	58.4	28	16.6	0.52	23.0	0.40	316	90.2
10	58.83	15	59.4	29	15.2	0.51	23.7	0.40	314	89.7
11	58.87	15	58.4	28	18.8	0.49	23.0	0.40	321	91.7
12	58.90	15	58.9	32	19.2	0.50	26.5	0.40	337	96.3
13	58.93	15	59.1	28	19.4	0.48	23.2	0.40	318	90.9
14	58.97	15	58.7	33	19.5	0.48	27.4	0.40	333	95.2
15	59.00	15	59.2	28	19.4	0.49	22.7	0.40	322	92.1
16	59.02	27	58.3	28	18.4	0.48	22.7	0.22	314	89.8
17	59.04	27	59.4	30	19.4	0.48	24.3	0.22	328	93.6
18	59.06	27	58.2	29	17.5	0.47	23.4	0.22	313	89.5
19	59.07	27	59.1	31	18.2	0.48	25.5	0.22	327	93.3
20	59.09	27	58.7	30	20.1	0.46	24.3	0.22	323	92.3
21	59.11	27	59.0	32	18.2	0.46	26.3	0.22	319	91.1
22	59.13	27	58.7	26	20.5	0.44	21.0	0.22	314	89.7
23	59.15	27	58.7	31	17.9	0.45	25.5	0.22	321	91.7
24	59.17	27	59.1	30	20.3	0.44	24.9	0.22	316	90.3
25	59.19	27	58.4	30	19.1	0.46	24.7	0.22	326	93.0
26	59.20	27	58.9	28	17.7	0.43	22.8	0.22	305	87.2
27	59.22	27	58.7	30	18.0	0.44	24.8	0.22	317	90.7
28	59.24	27	58.9	29	19.3	0.43	23.8	0.22	319	91.2
29	59.26	27	58.6	27	21.2	0.44	22.1	0.22	322	92.1
30	59.28	27	59.0	32	17.8	0.41	26.1	0.22	316	90.4
31	59.30	27	58.5	28	21.8	0.42	22.8	0.22	324	92.7

32	59.31	27	58.7	31	19.1	0.40	25.4	0.23	328	93.6
33	59.33	27	59.0	30	18.4	0.40	24.6	0.23	320	91.3
34	59.35	27	58.5	27	21.0	0.39	22.1	0.22	320	91.5
35	59.37	27	58.9	30	18.5	0.39	24.2	0.22	324	92.6
36	59.39	27	58.6	26	19.9	0.39	21.3	0.22	318	91.0
37	59.41	27	59.2	30	18.4	0.38	25.0	0.22	320	91.5
38	59.43	27	58.3	28	20.4	0.38	22.6	0.22	327	93.4
39	59.44	27	59.1	28	16.6	0.38	22.7	0.22	308	88.1
40	59.46	27	58.7	30	20.3	0.39	24.4	0.22	333	95.0
41	59.48	27	58.8	29	17.8	0.38	23.8	0.22	315	90.1
42	59.50	27	59.2	27	18.5	0.39	22.4	0.23	315	89.9
43	59.51	44	58.6	30	19.5	0.40	24.7	0.13	333	95.2
44	59.52	44	59.2	29	19.3	0.38	23.9	0.14	317	90.5
45	59.53	44	58.2	29	19.2	0.38	24.1	0.14	324	92.6
46	59.55	44	59.2	28	19.3	0.38	23.2	0.13	324	92.5
47	59.56	44	58.5	28	18.6	0.38	23.2	0.14	317	90.6
48	59.57	44	58.9	27	19.6	0.38	22.5	0.13	315	90.1
49	59.58	44	58.9	29	18.6	0.39	23.8	0.14	324	92.7
50	59.59	44	58.6	30	19.4	0.38	24.8	0.14	317	90.5
51	59.60	44	59.0	28	18.1	0.38	23.0	0.14	308	88.1
52	59.61	44	58.6	29	18.3	0.39	23.7	0.14	324	92.7
53	59.63	44	58.9	28	18.9	0.39	23.2	0.14	322	92.1
54	59.64	44	58.3	30	19.4	0.37	24.2	0.14	314	89.7
55	59.65	44	59.0	28	20.2	0.37	22.8	0.14	315	90.0
56	59.66	44	58.2	28	19.6	0.38	22.7	0.14	321	91.7
57	59.67	44	59.0	30	19.7	0.38	24.2	0.14	320	91.5
58	59.68	44	58.7	27	15.9	0.37	22.5	0.14	306	87.4
59	59.69	44	58.7	30	19.2	0.38	24.5	0.14	325	92.7
60	59.70	44	59.1	29	19.7	0.38	23.4	0.14	323	92.4
61	59.72	44	58.4	30	16.8	0.37	24.2	0.14	311	89.0
62	59.73	44	59.1	31	18.3	0.38	25.6	0.14	319	91.3
63	59.74	44	58.4	30	18.4	0.37	24.6	0.13	322	92.1
64	59.75	44	58.9	29	17.4	0.38	23.5	0.14	313	89.3
65	59.76	44	58.6	28	15.2	0.37	22.8	0.14	304	87.0
66	59.77	44	58.9	28	19.4	0.37	23.0	0.14	317	90.5
67	59.78	44	58.6	28	16.9	0.38	23.0	0.14	309	88.2
68	59.80	44	58.6	29	19.2	0.38	24.1	0.13	332	94.9
69	59.81	44	58.9	29	19.8	0.37	23.7	0.14	322	92.0
70	59.82	44	58.6	27	21.2	0.38	21.9	0.14	321	91.6
71	59.83	44	59.0	31	19.9	0.38	25.0	0.14	326	93.1
72	59.84	44	58.4	29	18.0	0.38	24.1	0.14	317	90.6
73	59.85	44	59.3	32	17.4	0.38	26.5	0.14	319	91.1
74	59.86	44	58.4	26	20.3	0.37	21.6	0.14	318	90.9
75	59.88	44	59.1	31	20.2	0.38	25.7	0.14	326	93.1
76	59.89	44	58.6	27	17.6	0.38	22.2	0.14	312	89.1
77	59.90	44	58.6	32	18.2	0.38	26.6	0.14	323	92.3
78	59.91	44	58.8	28	20.6	0.37	23.1	0.13	320	91.4
79	59.92	44	58.5	28	20.3	0.38	23.0	0.14	327	93.6
80	59.93	44	59.1	29	19.4	0.38	23.5	0.14	323	92.3
81	59.94	44	58.4	26	18.7	0.37	21.3	0.13	312	89.2
82	59.95	44	59.1	28	19.9	0.38	23.2	0.14	326	93.2
83	59.97	44	58.5	28	20.8	0.37	23.4	0.14	324	92.5
84	59.98	44	58.7	31	19.8	0.37	25.4	0.14	330	94.1
85	59.99	44	58.8	28	21.1	0.39	22.9	0.13	330	94.3
86	60.00	44	58.7	31	20.2	0.39	25.1	0.14	337	96.1
Average		58.8	29	19.0	0.40	23.8	0.17	320	91.4	
Std Dev		0.3	2	1.3	0.03	1.3	0.04	7	1.9	
Maximum		59.4	32	21.8	0.48	26.6	0.23	337	96.1	
Minimum		58.2	26	15.2	0.37	21.0	0.13	304	87.0	

N-value: 71

Sample Interval Time: 86.68 seconds.

Summary of SPT Test Results

Project: CME-550X SN 290593, Test Date: 11/17/2023

BPM: Blows/Minute

CSX: Compression Stress Maximum

FMX: Maximum Force

DFN: Final Displacement

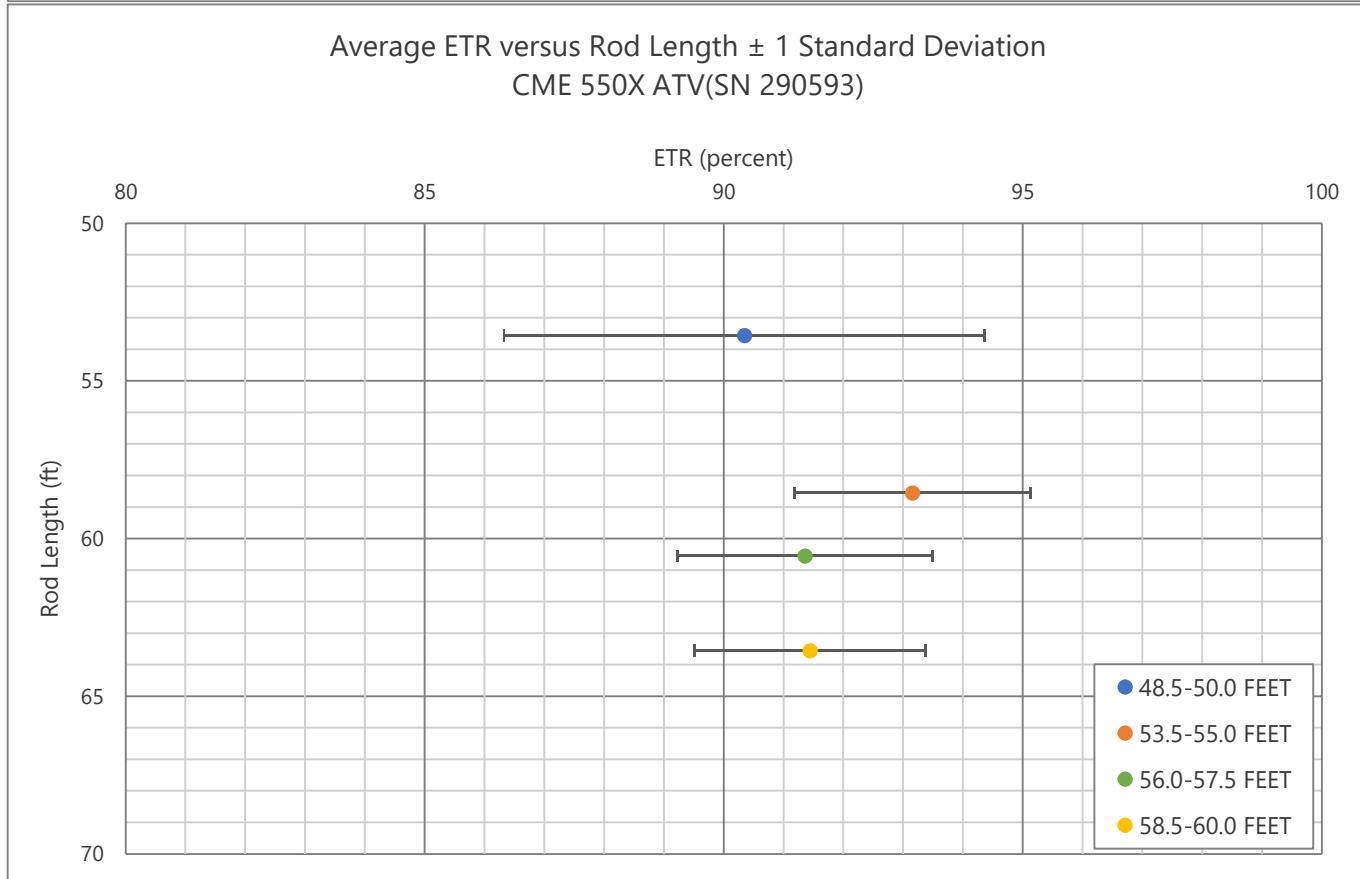
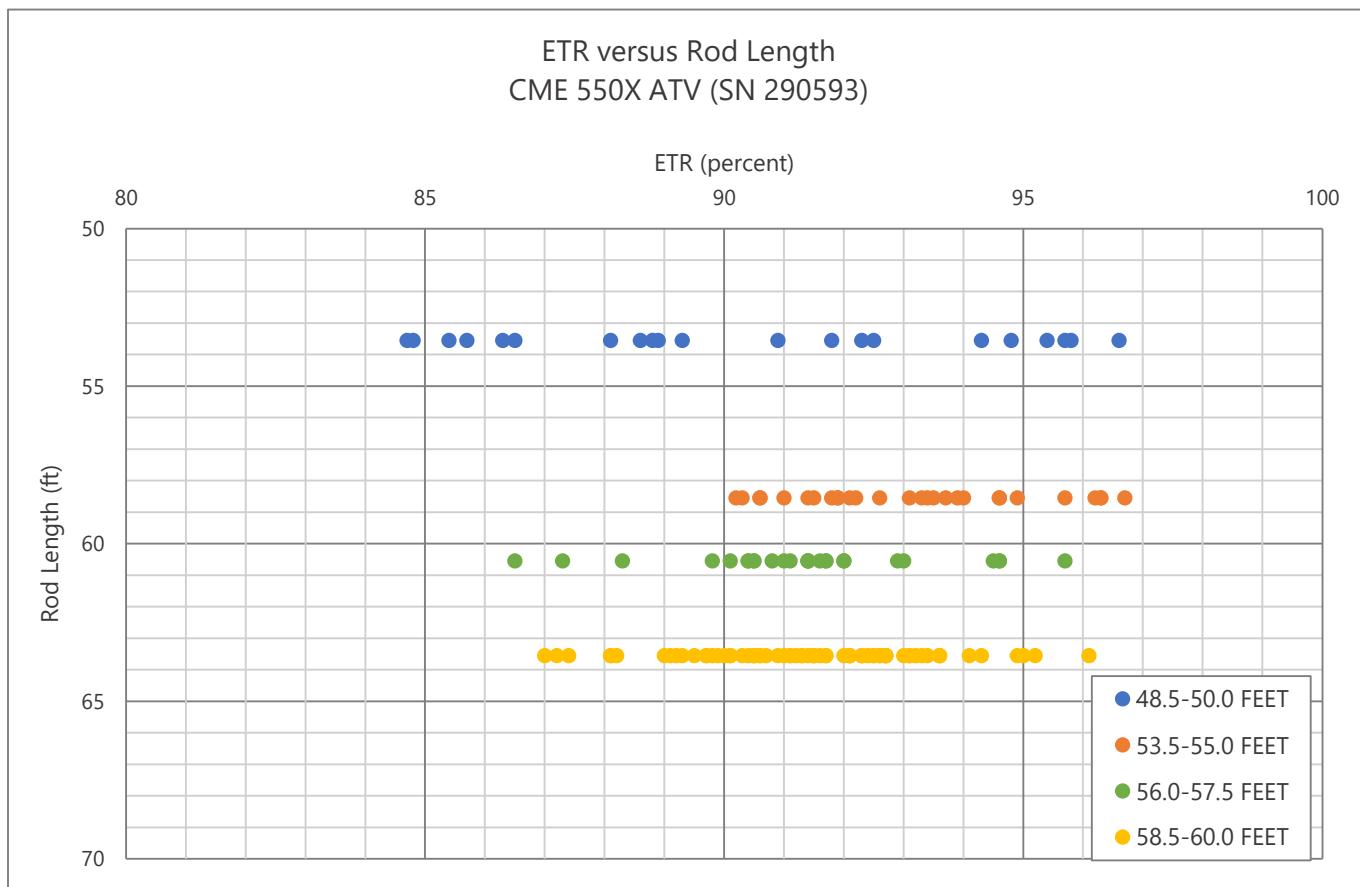
VMX: Maximum Velocity

EFV: Maximum Energy

DMX: Maximum Displacement

ETR: Energy Transfer Ratio - Rated

Instr. Length ft	Start Depth ft	Final Depth ft	Blows Applied /6"	N Value	N60 Value	Average BPM bpm	Average FMX kips	Average VMX ft/s	Average DMX in	Average CSX ksi	Average DFN in	Average Efv ft-lb	Average ETR %
53.55	48.50	50.00	6-8-13	21	32	58.6	30	16.1	0.63	24.8	0.57	316	90.3
58.55	53.50	55.00	6-11-17	28	42	58.7	28	18.5	0.55	23.2	0.43	326	93.2
60.55	56.00	57.50	7-9-17	26	39	58.6	29	16.6	0.59	24.1	0.46	320	91.3
63.55	58.50	60.00	15-27-44	71	108	58.8	29	19.0	0.40	23.8	0.17	320	91.4
				Overall Average Values:		58.7	29	18.1	0.49	23.9	0.33	321	91.6
				Standard Deviation:		0.3	2	1.8	0.12	1.3	0.19	9	2.5
				Overall Maximum Value:		59.4	33	21.8	0.81	27.4	0.75	338	96.7
				Overall Minimum Value:		58.1	26	12.8	0.37	21.0	0.13	296	84.7





Report of SPT Energy Measurements
S&ME CME-550X ATV Rig
(Serial No. 293193)
Blythewood, South Carolina

PREPARED FOR:

**North Carolina Department of Transportation
Geotechnical Engineering Unit
1589 Mail Service Center
Raleigh, North Carolina 27699**

PREPARED BY:

**S&ME, Inc.
8848 Red Oak Boulevard, Suite A
Charlotte, North Carolina 28217**

December 27, 2023



December 27, 2023

North Carolina Department of Transportation
Geotechnical Engineering Unit
1589 Mail Service Center
Raleigh, North Carolina 27699

Attention: Mr. Greg Bodenheimer, P.E.

Cc: Ms. Cheryl A. Youngblood, L.G.
Ms. Christina M. Bruinsma, L.G.

Reference: **Report of SPT Energy Measurements**
S&ME CME-550X ATV Rig (Serial No. 293193)
Blythewood, South Carolina
NC PE Firm License No. F-0176

Dear Mr. Bodenheimer:

We have completed the Standard Penetration Test (SPT) energy measurements on the automatic hammer used with our CME-550X ATV-mounted drill rig (Serial No. 293193). This service was performed by Mr. Joseph Williamson, P.E. of our firm on November 17, 2023, in general accordance with ASTM D4633 and the most recent revision of the North Carolina Department of Transportation (NCDOT) Geotechnical Engineering Unit's requirements. Review of the data quality and analyses was performed by Mr. Williamson. A copy of the Certificate of Proficiency issued by Pile Dynamics based on the Dynamic Measurement and Analysis Proficiency Test for Mr. Williamson is included in Appendix I. The testing procedures, equipment used during testing, and detailed results are presented in this report.

1.0 Dynamic Testing Methodology

Testing was performed using a model PAX (Serial No. 3726L) Pile Driving Analyzer™ (PDA) manufactured by Pile Dynamics, Inc. The PDA was used to record and interpret data from two piezoresistive accelerometers (Serial Nos. K4664 and K4665) bolted to a 2.0-foot long AWJ drill rod (Serial No. 203) internally instrumented with two strain transducers. Calibration sheets for the accelerometers and the instrumented rod are included in Appendix II. The instrumented AWJ drill rod has a cross-sectional area of 1.22 square inches and an outside diameter of approximately 1 $\frac{3}{4}$ inches. Therefore, we calculate the inside diameter to be approximately 1 $\frac{1}{4}$ inches at the gauge location. The accelerometers and strain gauges, which are diametrically opposed near the middle of the instrumented rod, monitor acceleration and strain for each hammer blow. The analyzer converts the data to velocities and forces and computes the maximum transferred hammer energies with the "EFV" method described in ASTM D4633. Preliminary results are recorded and displayed in real time for each blow.



2.0 Testing and Observations

S&ME personnel were on site November 17, 2023, to observe and perform high-strain dynamic testing during SPT sampling on the CME-550X ATV-mounted drill rig operated by Sam Eubanks of S&ME. The measurements were taken during drilling of a test hole adjacent to a previous soil test boring at an S&ME project site in Blythewood, South Carolina. SPT energy measurements were recorded during three sampling intervals that met the NCDOT required blow count criteria. The information presented in the tables below summarizes the equipment and tooling used during the SPT energy measurements. The SPT Energy Evaluation Form and the Soil Test Boring Log from the adjacent boring are included in Appendix III.

Table 2-1: Drill Rig Information

Manufacturer	CME
Model	550X
Serial Number	293193
Operator	S. Eubanks
Carrier	ATV

Table 2-2: Hammer Information

Model / Type	CME / Auto
Serial Number	293193
Typical Drop Height (inches)	30
Typical Ram Weight (pounds)	140
Ram Serial Number	N/A

Table 2-3: Drilling and Instrumented Rod Information

Instrumented Rod Type	AWJ (Serial No. 203)
OD (inches) ¹	1 3/4
ID (inches) ²	1 1/4
Cross-Sectional Area (in ²) ³	1.22
Total Instrumented Rod Length (feet) ¹	2.0
Length Below Gages (feet) ¹	0.7
Typical Rod Lengths (feet)	5
Split-Spoon Length (feet) ¹	2.85

¹ Measured with engineer's tape measure.

² Calculated using measured OD and Area from instrument rod calibration record.

³ From instrument rod calibration record.



3.0 Dynamic Testing Results

The total rod length from the instrumentation to the tip of the split-spoon sampler was determined by adding 3.55 ft to the drill rod length at each sample depth. The SPT Energy Measurement Data Summary tables in Appendix IV present the test data from every hammer blow at each sampling interval, along with representative force and velocity traces for each test interval. Per ASTM D4633, only the blows from the final foot of each sample interval (i.e. the blows that determine the N-value) are considered when computing the average measurement values of each test interval.

The reported blow counts obtained by the drill rig personnel, a summary of the test data, and average computed hammer energy and transfer ratio values are provided in Table 3-1. Based on the test data, the automatic hammer on the CME-550X operated at an average rate of about 55 blows per minute (bpm) during dynamic testing. The measured average transferred hammer energy (EFV) of the three sample intervals ranged from 301 to 312 ft-lbs, which corresponds to Energy Transfer Ratio (ETR) values of 86.1 to 89.3%, respectively. Plots and tables of the following are also included in Appendix III and present the test data with depth for each test interval:

- Penetration vs. BLC⁴
- Penetration vs. FMX⁵
- Penetration vs. EFV⁶
- Penetration vs. CSX⁷
- Penetration vs. VMX⁸
- Penetration vs. ETR⁹
- ETR vs. Rod Length
- Average ETR vs. Rod Length

Table 3-1: Summary of Dynamic Testing Results

Data Set ID	Sample Depth (ft)	Drill Rod Length (ft)	Instrumentation to Sampler Tip Length (ft)	Blows per 6" Increment / N-value	Soil Sample Description	Avg. BPM	Avg. Efv (ft-lbs)	Avg. ETR (%)
1	43.5 – 45.0	45	48.55	8-15-20 / 35	Elastic SILT	55.2	304	86.9
2	48.5 – 50.0	50	53.55	5-7-11 / 18	Elastic SILT	55.2	301	86.1
3	53.5 – 55.0	55	58.55	8-14-18 / 32	Elastic SILT	55.0	312	89.3
Overall Average						55.1	307	87.6

The overall average transferred hammer energy for the automatic hammer on the CME-550X ATV-mounted drill rig (SN 293193) was 307 foot-pounds, with an average ETR of 87.6%.

⁴ BLC - Blow Count per 6-in. increment

⁵ FMX - Maximum Compressive Force

⁶ EFV - Maximum Transferred Energy

⁷ CSX - Maximum Compressive Stress

⁸ VMX - Maximum Velocity

⁹ ETR - Energy Transfer Ratio - Ratio of Calculated Energy to Theoretical Energy of 140 lb hammer falling 30 inches



4.0 Limitations of Report

This report has been prepared in accordance with generally accepted geotechnical engineering practice for specific application to this project. The conclusions contained in this report were based on the applicable standards of our profession in this geographic area at the time this report was prepared. No other warranty, express or implied, is made.

5.0 Closing

S&ME appreciates the opportunity to provide this report to the North Carolina Department of Transportation, Geotechnical Engineering Unit. Please let us know if you have any questions concerning this report.

Sincerely,

S&ME, Inc.

A handwritten signature in black ink, appearing to read "GJ".

Joseph R. Williamson, P.E.
Project Manager
N.C. Registration No. 42168

Gregory J. Canivan, P.E.
Technical Principal

Appendices:

- Appendix I - Certificate of Proficiency
- Appendix II - Accelerometer and Instrumented Rod Calibration Sheets
- Appendix III - SPT Energy Evaluation Form (Field Log)
- Appendix IV - CME-550X ATV (SN 293193) SPT Energy Measurement Summary Plots and Tables

Appendix I- Certificate of Proficiency



This documents that

**Joseph Williamson
S&ME, Inc.**



has on March 16, 2022 achieved the rank of

MASTER

on the Dynamic Measurement and Analysis Proficiency Test.

The individual identified on this document demonstrated to the degree granted above an understanding of theory, data quality evaluation, interpretation and signal matching for high strain dynamic testing of deep foundations. ***It is recommended that individuals at the Master level seek to attain Expert level through additional study within eight years of the date of this document***

The ability of the individual named to provide appropriate knowledge and advice on a specific project is not implied or warranted by the Pile Driving Contractors Association or Pile Dynamics, Inc. The Pile Driving Contractors Association or Pile Dynamics, Inc. assumes no liability for foundation testing and analysis work performed by the bearer of this certificate. This certificate can be verified at www.PDAproficiencytest.com.

A handwritten signature in blue ink that reads "Frank T. Peters".

Frank T. Peters, Executive Director
Pile Driving Contractors Association



A handwritten signature in blue ink that reads "Garland Likins".

Garland Likins, Senior Partner
Pile Dynamics, Inc.

No. 3251

Appendix II - Calibration Sheets

Accelerometer Calibration Certificate

Pile Dynamics, Inc.



Calibrated by Pile Dynamics, Inc.
Calibration performed on 17Aug2023

Serial No: K4664 Temperature: 77.6 °F

Model: PR Humidity: 51%

Calibrated on: Channel 3 on 8G 5161 LE

PDA CALIBRATION FACTOR

376.6 mv/5000g
(75.3 μ v/g)
 $R^2: 0.999955$ [Chip programmed]

Operator: William Johnson

Ref Acc 1: 72505!
1035 g's/volt

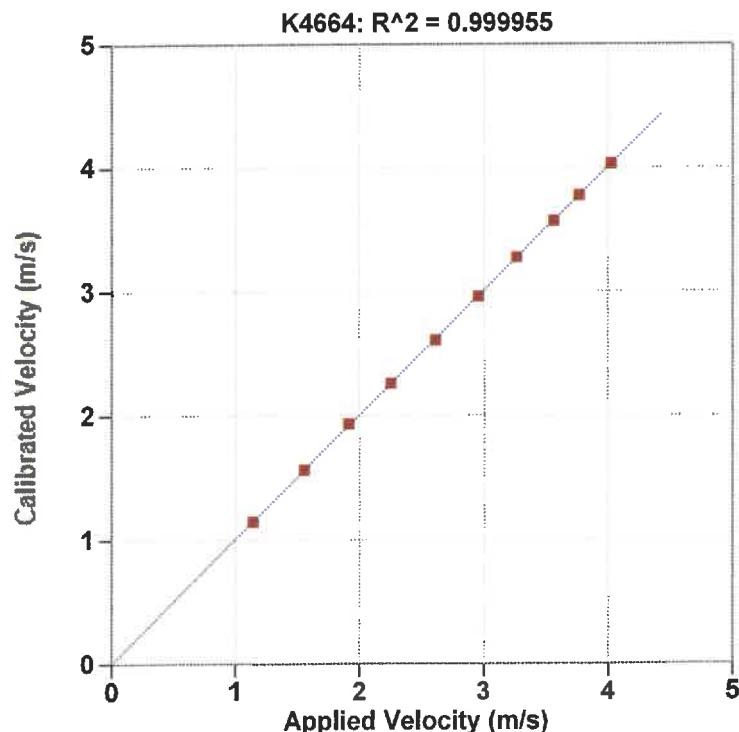
Cal on: 24Mar2022

Ref Acc 2: 72517!
1049 g's/volt

Cal on: 24Mar2022

Signed

Reference accelerometer calibrations are traceable to
the United States National Institute of Standards and
Technology (NIST).



Reference Velocity	S/N K4664 Velocity
m/s	m/s
1.146	1.143
1.560	1.559
1.915	1.932
2.255	2.258
2.612	2.606
2.962	2.958
3.270	3.273
3.569	3.566
3.772	3.773
4.030	4.027

Maximum Acceleration: 879 g's

Accelerometer Calibration Certificate

Pile Dynamics, Inc.



Calibrated by Pile Dynamics, Inc.
Calibration performed on 17Aug2023

Serial No: K4665 Temperature: 77.6 °F PDA CALIBRATION FACTOR

Model: PR Humidity: 51% 375.3 mv/5000g
(75.1 μ v/g)
R²: 0.999957 [Chip programmed]

Calibrated on: Channel 3 on 8G 5161 LE

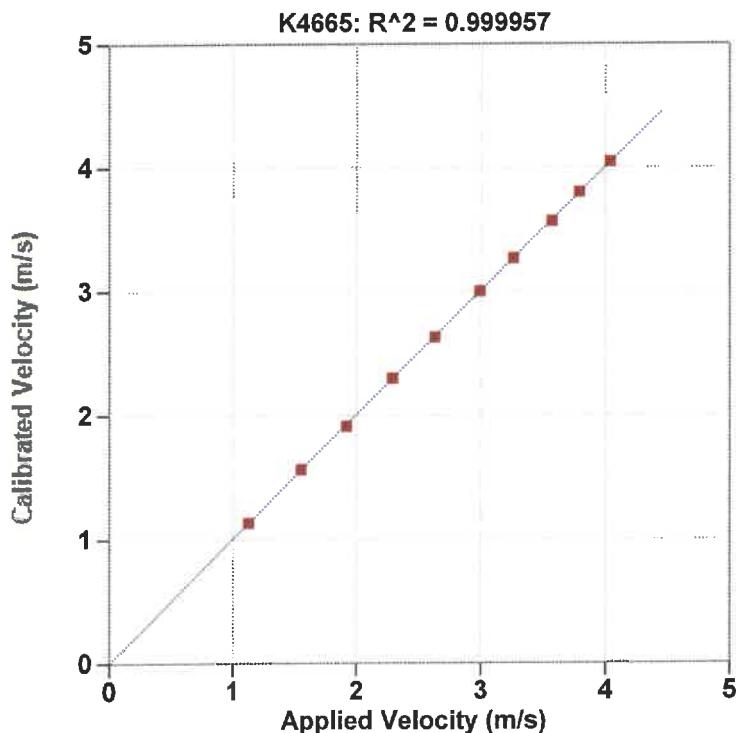
Ref Acc 1: 72505!
1035 g's/volt Cal on: 24Mar2022

Ref Acc 2: 72517!
1049 g's/volt Cal on: 24Mar2022

Operator: William Johnson


Signed

Reference accelerometer calibrations are traceable to
the United States National Institute of Standards and
Technology (NIST).



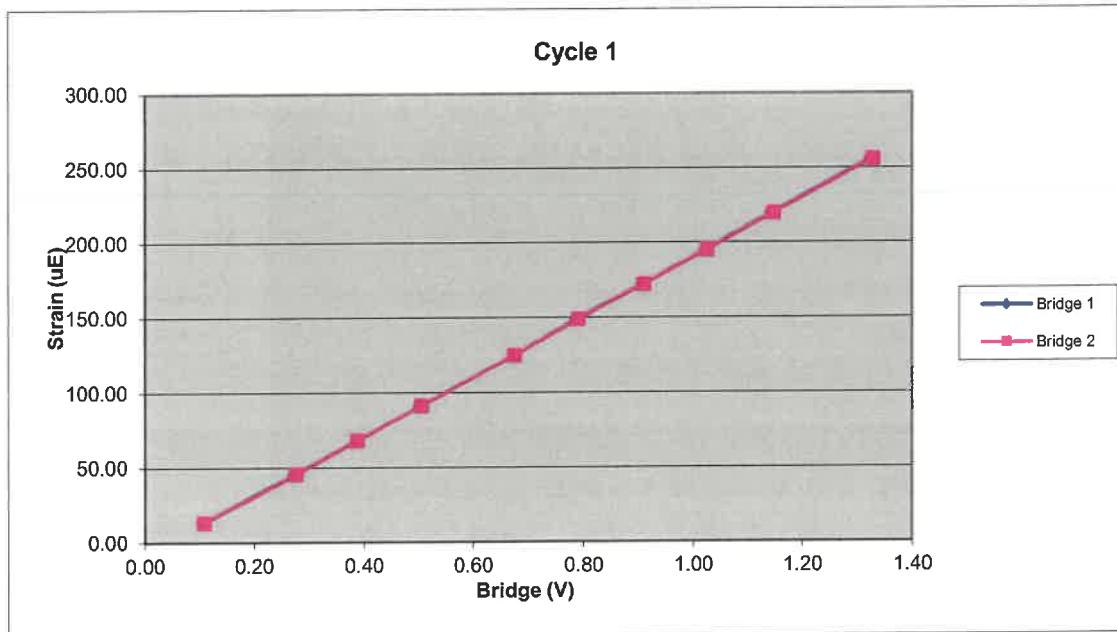
Reference Velocity	S/N K4665 Velocity
m/s	m/s
1.129	1.131
1.555	1.560
1.922	1.910
2.291	2.295
2.633	2.627
2.994	2.999
3.262	3.264
3.573	3.564
3.791	3.797
4.038	4.041

Maximum Acceleration: 880 g's

203AWJ		Cycle 1		
Sample	Force (lb)	Strain (μE)	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	819.88	13.18	0.11	0.11
3	2100.72	45.33	0.27	0.28
4	2947.11	68.12	0.39	0.39
5	3827.72	90.98	0.50	0.51
6	5122.01	124.83	0.67	0.68
7	5996.48	148.92	0.79	0.79
8	6896.87	172.25	0.91	0.91
9	7771.24	195.27	1.02	1.03
10	8694.53	219.87	1.15	1.15
11	10075.00	255.83	1.33	1.33

Bridge 1	Bridge 2
Force Calibration (lb/V)	7576.32
Offset	14.17
Correlation	0.999999
Strain Calibration ($\mu\text{E}/\text{V}$)	199.46
Offset	-9.00
Correlation	0.999979
Force Calibration (lb/V)	7575.14
Offset	2.97
Correlation	0.999999
Strain Calibration ($\mu\text{E}/\text{V}$)	199.43
Offset	-9.29
Correlation	0.999982

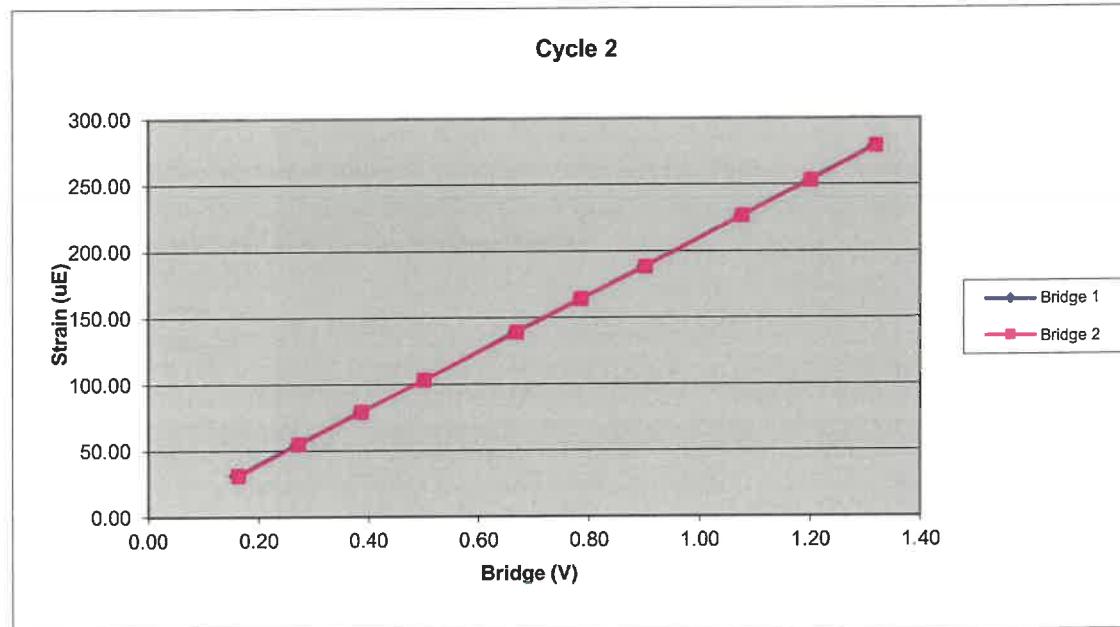
Force Strain Calibration
EA (Kips)
37982.46
Offset
356.04
Correlation
0.999980



203AWJ		Cycle 2		
Sample	Force (lb)	Strain (μE)	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	1217.00	30.72	0.16	0.16
3	2060.56	54.45	0.27	0.27
4	2939.22	78.94	0.39	0.39
5	3811.73	102.81	0.50	0.50
6	5082.83	138.71	0.67	0.67
7	5976.20	163.65	0.78	0.79
8	6861.10	187.95	0.90	0.90
9	8194.67	226.13	1.08	1.08
10	9130.84	252.84	1.20	1.20
11	10039.52	278.74	1.32	1.32

Bridge 1	Bridge 2
Force Calibration (lb/V)	7616.13
Offset	1.43
Correlation	0.999999
Strain Calibration ($\mu\text{E}/\text{V}$)	213.80
Offset	-3.74
Correlation	0.999987
Force Calibration (lb/V)	7615.56
Offset	-11.88
Correlation	0.999997
Strain Calibration ($\mu\text{E}/\text{V}$)	213.79
Offset	-4.12
Correlation	0.999990

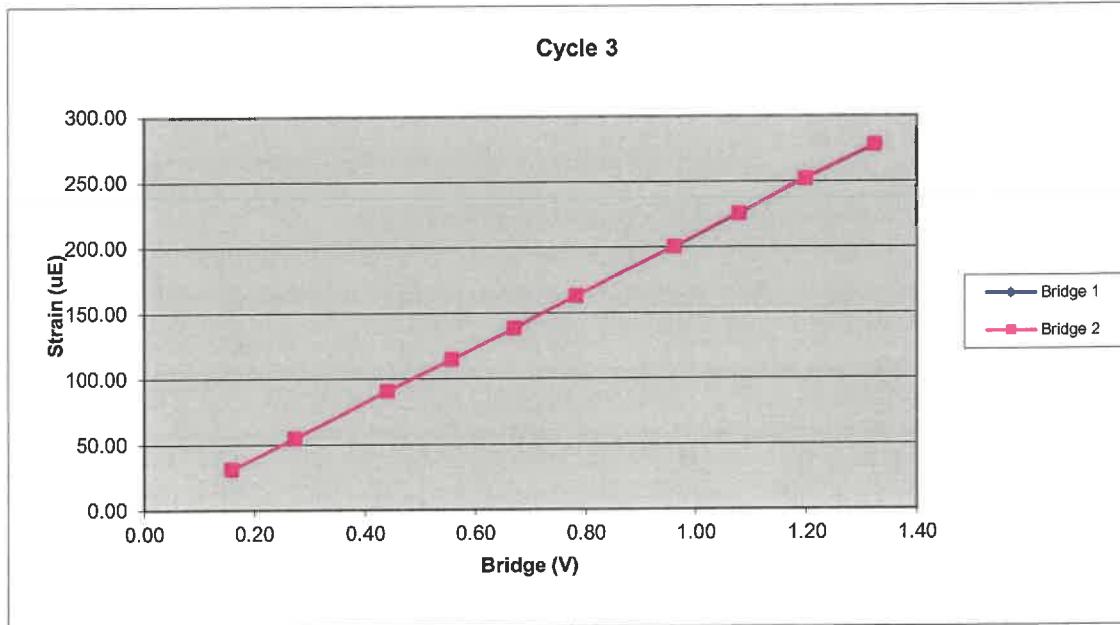
Force Strain Calibration
EA (Kips)
Offset
Correlation



203AWJ		Cycle 3		
Sample	Force (lb)	Strain (μE)	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	1216.12	31.38	0.16	0.16
3	2078.01	54.75	0.27	0.27
4	3348.13	90.71	0.44	0.44
5	4248.62	114.98	0.56	0.56
6	5110.90	138.68	0.67	0.67
7	5966.16	163.47	0.78	0.78
8	7338.73	200.80	0.96	0.96
9	8226.55	225.96	1.08	1.08
10	9144.10	252.26	1.20	1.20
11	10093.62	278.03	1.32	1.32

Bridge 1		Bridge 2	
Force Calibration (lb/V)	7621.84	Force Calibration (lb/V)	7635.13
Offset	-0.64	Offset	-3.95
Correlation	0.999999	Correlation	0.999999
Strain Calibration ($\mu\text{E}/\text{V}$)	212.12	Strain Calibration ($\mu\text{E}/\text{V}$)	212.49
Offset	-2.91	Offset	-3.01
Correlation	0.999979	Correlation	0.999985

Force Strain Calibration	
EA (Kips)	35930.12
Offset	104.27
Correlation	0.999985



Bridge Excitation (V) 5
Shunt Resistor (ohm) 60.4k

Calibration Factors	203AWJ		
Bridge 1 (μ E/V)	208.46	Bridge 2 (μ E/V)	208.57
EA Factor (Kips)	36511.28	Area (in ²)	1.22

Calibrated by: Sean Bang
Calibrated Date: 8/24/2023

Pile Dynamics Inc
30725 Aurora Rd
Solon, OH 44139

Traceable to N.I.S.T.

Appendix III – Field Log



SPT Energy Evaluation Form

Project: I-77 EXIT 26 PHASE I
Project No.: 23610178A
Boring No.: TES" HOLE B

Date: 11/17/23
Weather: CLFAR 70°
Drill Rod Type: 5' LONG AW5

On-site Personnel

Drilling Company: SIME
Rig Operator: S. EUBANKS
Engr/Geologist: N/A
Client Rep.: N/A
Analyzer Oper.: T. WILLIAMSON

Rig/Hammer Info

Drill Rig Make/Model: CME-550X
Carrier Type: ATV
Rig Serial No.: 293193 (R-46)
Hammer Type/Model: AUTO/CME
Hammer Serial No.: N/A
Hammer Drop System: CHAIN DRIVE
Lubrication Condition: PER MAN. RECS.

Manufacturer Recommended

Operation Rate (bpm): 50-55

Typical Drop Height (in.): 30

Typical Hammer Weight (lbs): 140

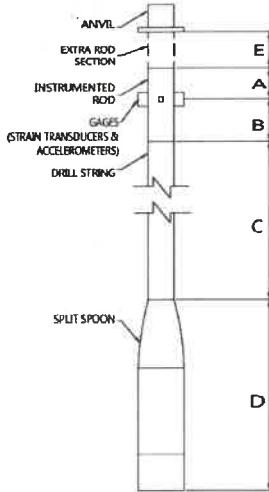
Anvil Dimension (in.): 12

Drilling Method: MUD ROTARY v12 - 14¹/₂" DRAB

Drop Height in Tolerance (y/n) y

Rod Info

(A) + (B) Instr. Rod Length: 2.0 ft
(B) Instr. Rod Length
 below Gages: 0.7 ft
(D) Spoon Length: 2.85 ft
(E) Rod Length Above
 Instr. Rod (if applicable): 0 ft
(B) + (C) + (D) (LE) -
 Length Below Gauges (C) + 3.55 ft
 Instr. Rod S/N: 203 AWJ
 Instr. Rod Outside Dia: 1.75 in.
 Instr. Rod Area: 1.22 in²
 PDA Make/Model: PDI /PAX
 PDA Serial No.: 3733 L
 Calib. Pulse Test (y/n): Y



Gage Info

Gage	Serial No.	Calibration No.
Accel.	A3	K4664 376.4
	A4	K4665 375.3
Strain	F3	Z03 AWJ-1 208.46
	F4	Z03 AWJ-2 208.57

Notes: FL SPIKING ON FIRST SAMPLE SWAPPED PIG TAIL.

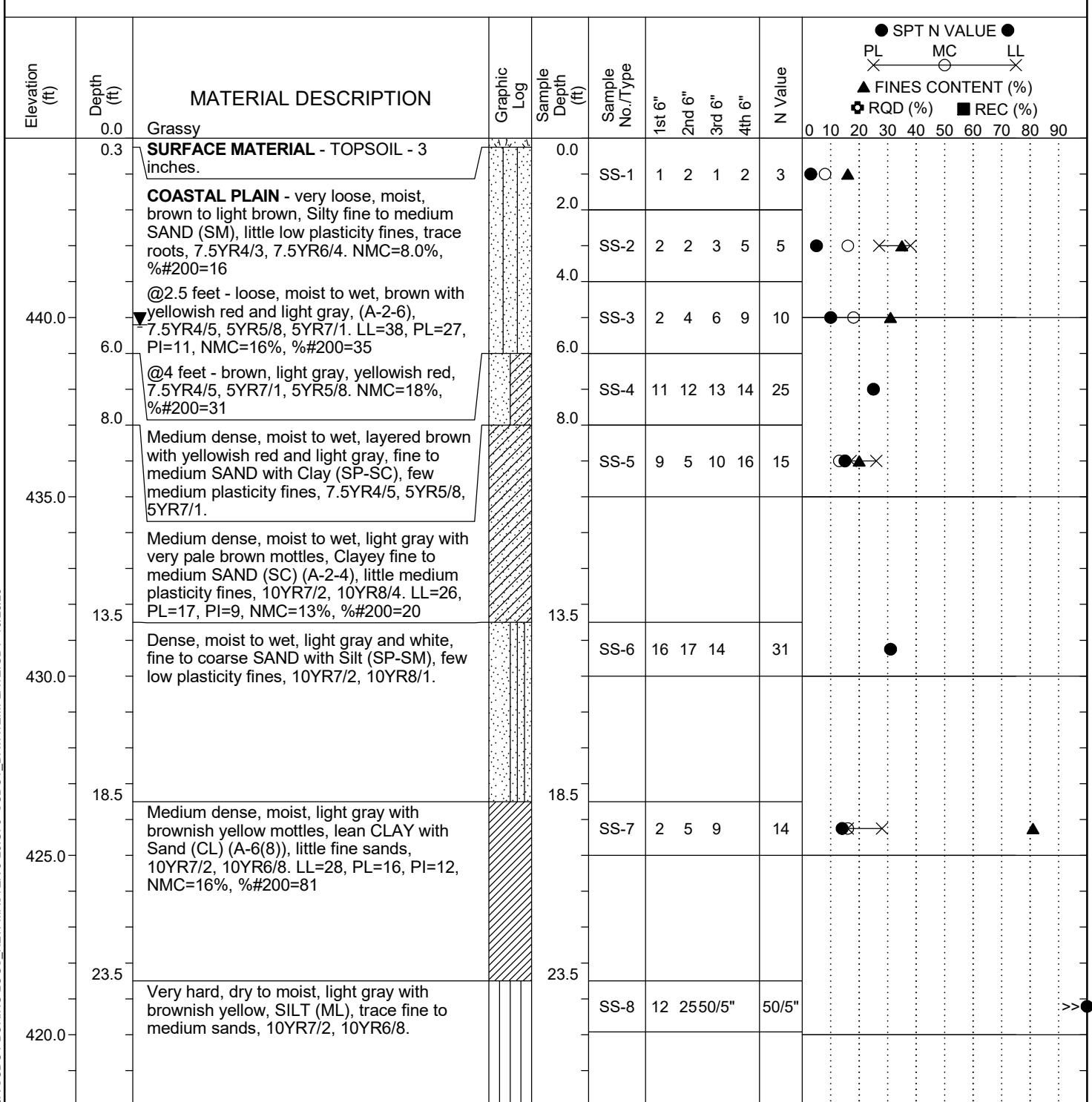
NOTE: (1) Note any unusual hammer operating conditions that affect the hammer performance, or changes in operating conditions (e.g. veritcality, weather, or lubrication between trials). (2) Note any changes in rod diameter along drill string and record locations of short rod sections.

Joseph Wilson

11/17/23

Date

Project ID:	23610178A			County:	Richland		Boring No.:	EB-2W
Site Description:	I-77 Exit 26 Phase I						Route:	US-21
Eng./Geo.:	Z. Zelaya	Boring Location:				Offset:		
Elev.:	445.0 ft	Latitude:	34.18975869	Longitude:	-80.97072615	Date Started:	7/24/2023	
Total Depth:	98.8 ft	Soil Depth:	98.8 ft	Core Depth:	N/A ft	Date Completed:	7/25/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	81.6%	
Core Size:	N/A	Driller:	S. Gowan	Groundwater:	TOB	NA	24HR	5.2 ft

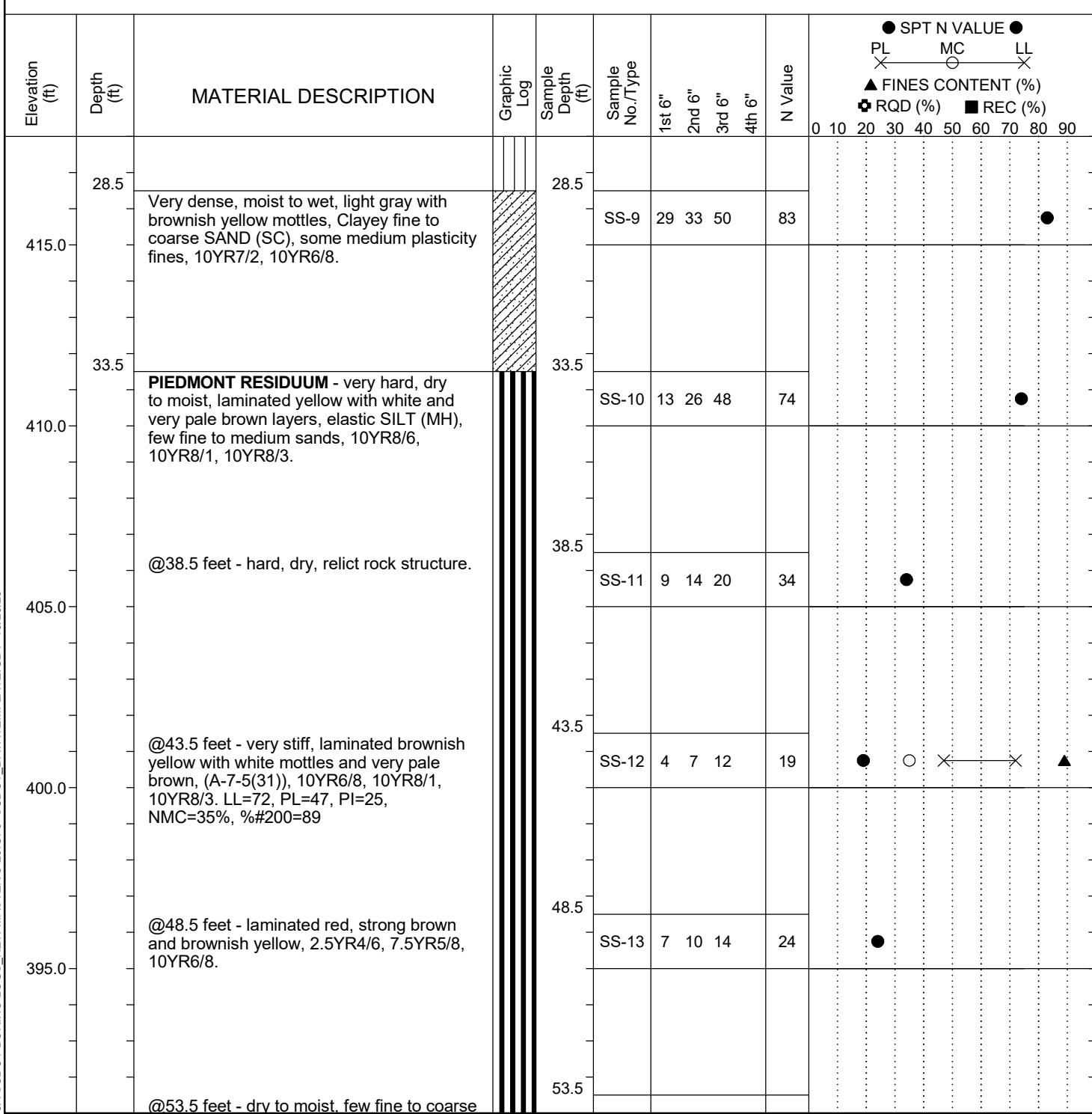


LEGEND

Continued Next Page

SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	CU - Cuttings	HSA - Hollow Stem Auger	RW - Rotary Wash	CFA - Continuous Flight Augers	DC - Driving Casing	RC - Rock Core
UD - Undisturbed Sample							
AWG - Rock Core, 1-1/8"		CT - Continuous Tube					

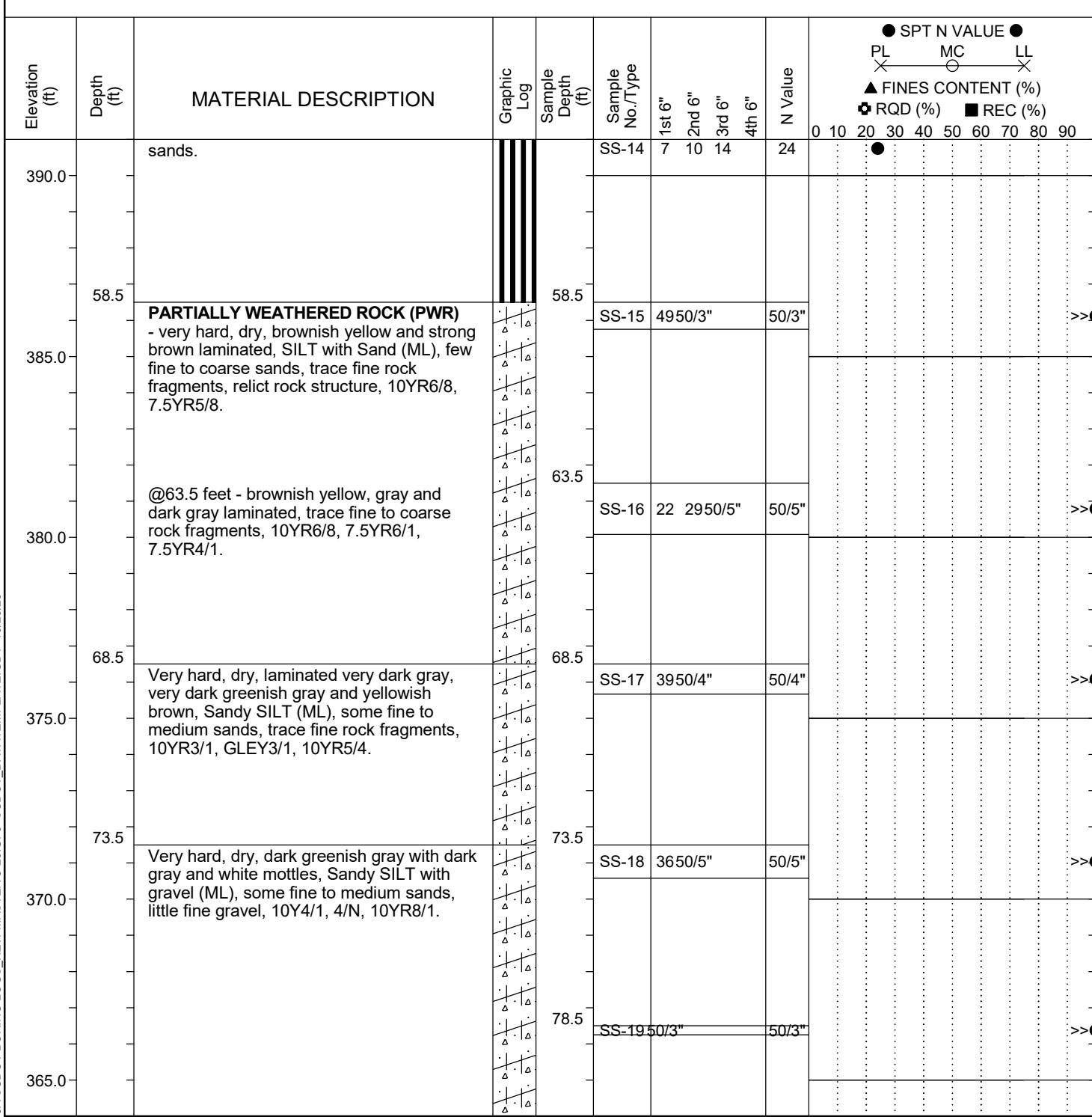
Project ID:	23610178A			County:	Richland		Boring No.:	EB-2W
Site Description:	I-77 Exit 26 Phase I						Route:	US-21
Eng./Geo.:	Z. Zelaya	Boring Location:				Offset:		
Elev.:	445.0 ft	Latitude:	34.18975869	Longitude:	-80.97072615	Date Started:	7/24/2023	
Total Depth:	98.8 ft	Soil Depth:	98.8 ft	Core Depth:	N/A ft	Date Completed:	7/25/2023	
Bore Hole Diameter (in):	4	Sampler Configuration			Liner Required:	Y (N)	Liner Used:	Y (N)
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	81.6%	
Core Size:	N/A	Driller:	S. Gowan	Groundwater:	TOB	NA	24HR	5.2 ft



SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Continued Next Page

Project ID:	23610178A			County:	Richland		Boring No.:	EB-2W
Site Description:	I-77 Exit 26 Phase I						Route:	US-21
Eng./Geo.:	Z. Zelaya		Boring Location:			Offset:		
Elev.:	445.0 ft		Latitude:	34.18975869		Longitude:	-80.97072615	
Total Depth:	98.8 ft		Soil Depth:	98.8 ft		Core Depth:	N/A ft	
Bore Hole Diameter (in):	4		Sampler Configuration		Liner Required:	Y (N)	Liner Used:	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	81.6%	
Core Size:	N/A	Driller:	S. Gowan	Groundwater:	TOB	NA	24HR	5.2 ft



LEGEND

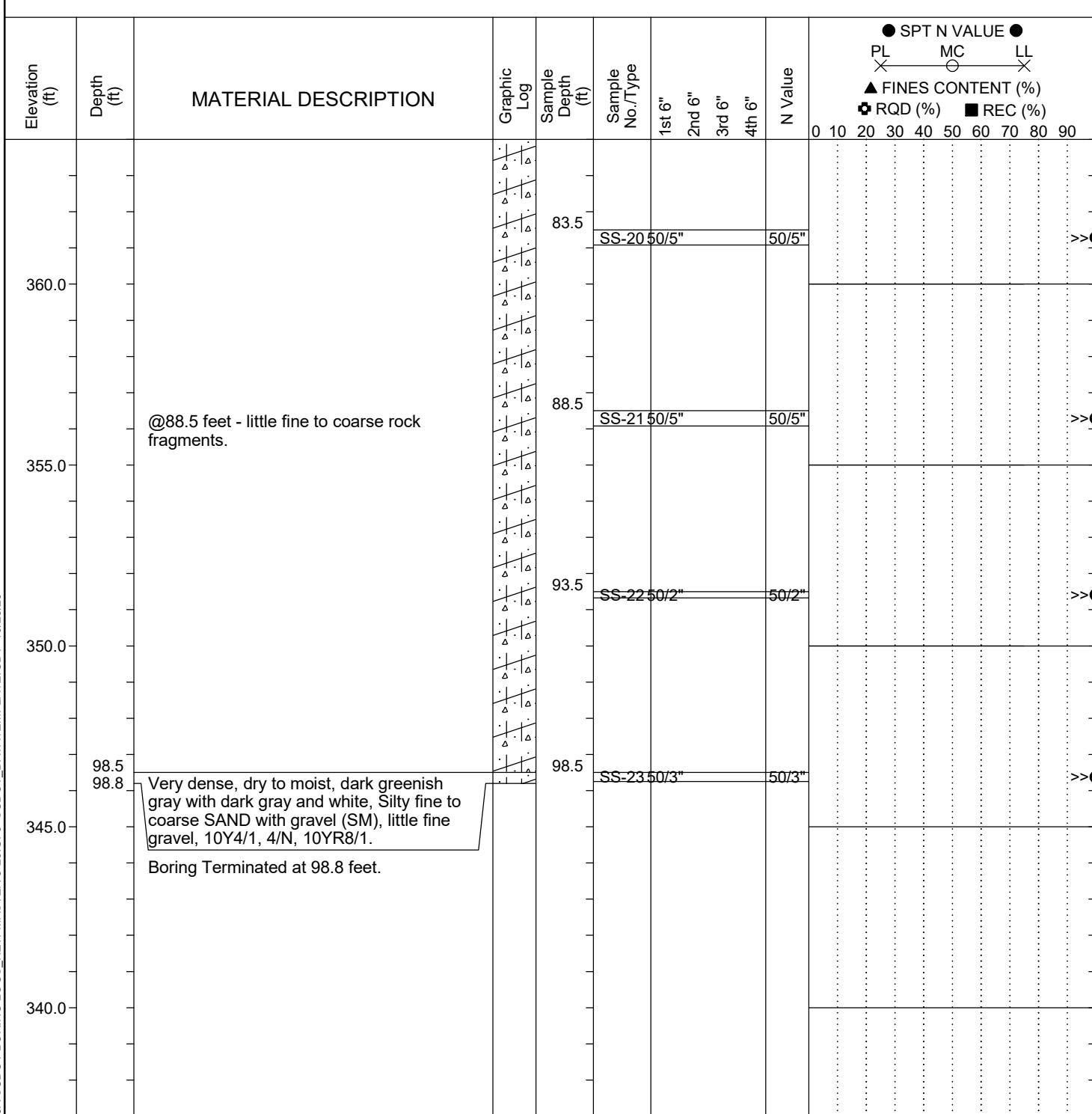
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SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



Soil Test Log

Project ID:	23610178A			County:	Richland		Boring No.:	EB-2W
Site Description:	I-77 Exit 26 Phase I						Route:	US-21
Eng./Geo.:	Z. Zelaya	Boring Location:				Offset:		
Elev.:	445.0 ft	Latitude:	34.18975869	Longitude:	-80.97072615	Date Started:	7/24/2023	
Total Depth:	98.8 ft	Soil Depth:	98.8 ft	Core Depth:	N/A ft	Date Completed:	7/25/2023	
Bore Hole Diameter (in):	4	Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)	
Drill Machine:	CME-550X	Drill Method:	RW	Hammer Type:	Automatic	Energy Ratio:	81.6%	
Core Size:	N/A	Driller:	S. Gowan	Groundwater:	TOB	NA	24HR	5.2 ft



Appendix IV – SPT Energy Measurement Plots and Tables



Pile Dynamics, Inc. - PDIPILOT2 Ver 2022.1.62.0 - Case Method & iCAP® Results

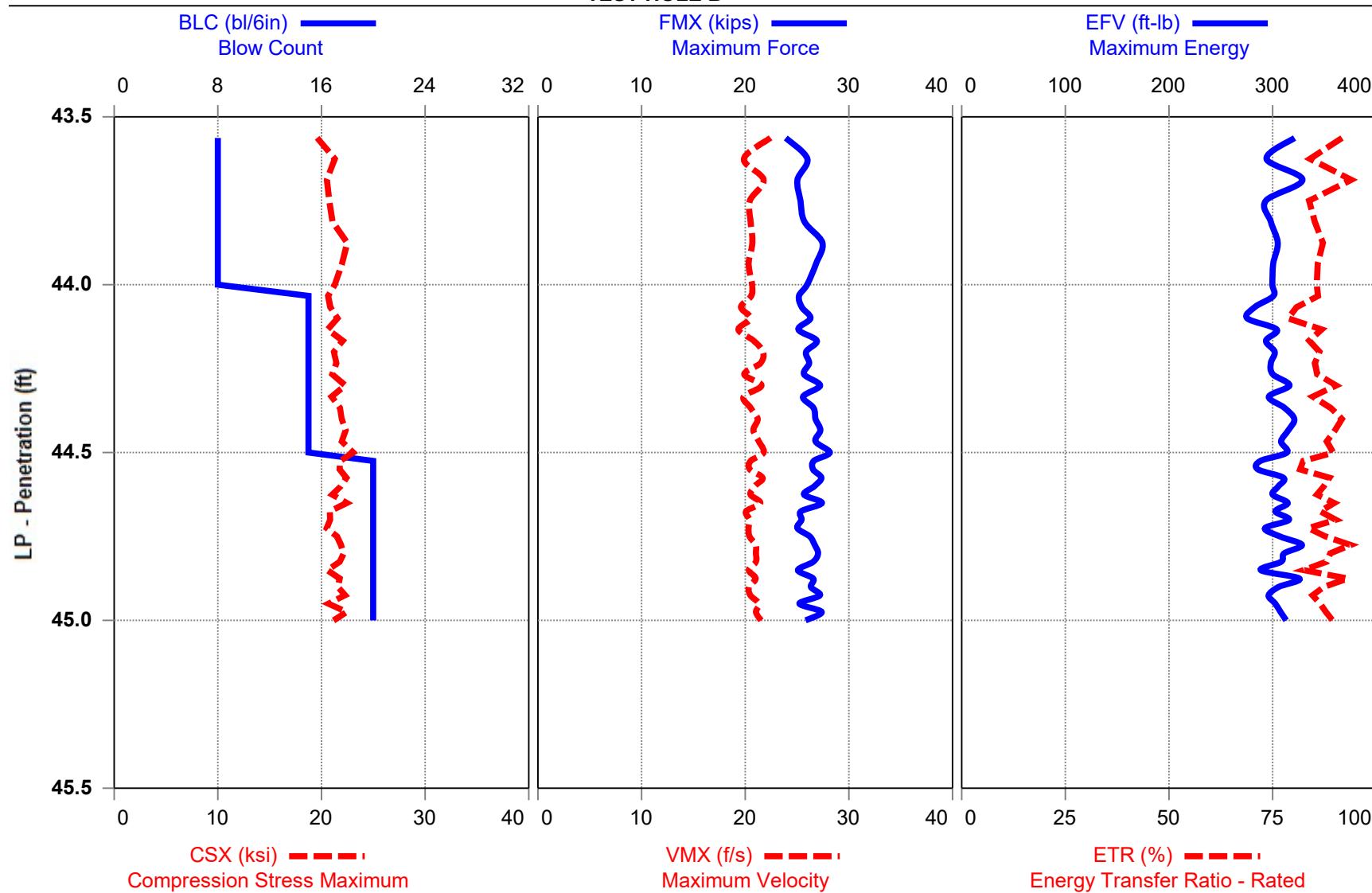
Printed: 14-December-2023

Test started: 17-November-2023



CME-550X SN 293193 - 43.5-45.0 FEET

TEST HOLE B



CME-550X SN 293193

JRW

TEST HOLE B

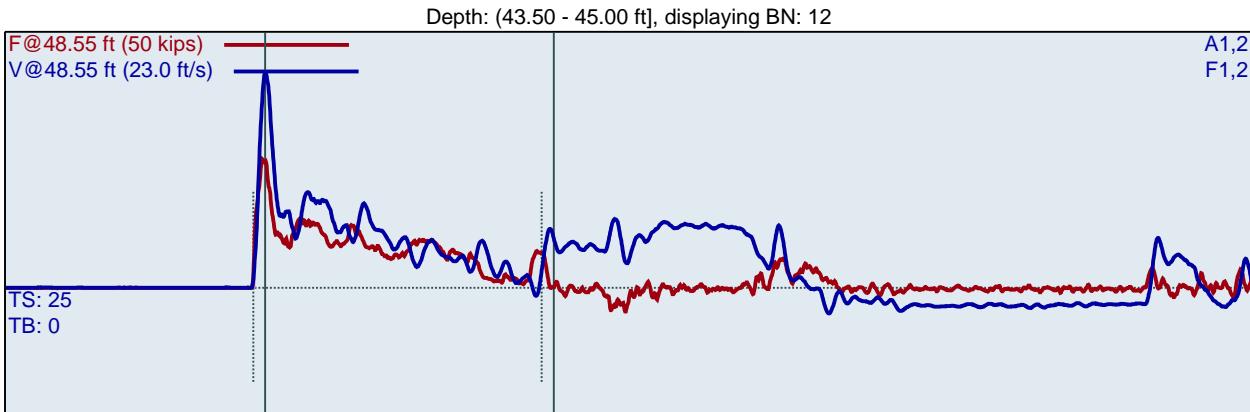
AR: 1.22 in²

LE: 48.55 ft

WS: 16807.9 ft/s

43.5-45.0 FEET
Interval start: 11/17/2023

SP: 0.492 k/ft³
EM: 30000 ksi



F1 : [203 AWJ-1] 208.46 PDICAL (1) FF1
F2 : [203 AWJ-2] 208.57 PDICAL (1) FF1

A1 (PR): [K4664] 376.6 mv/6.4v/5000g (1) VF1
A2 (PR): [K4665] 375.3 mv/6.4v/5000g (1) VF1

BPM: Blows/Minute

CSX: Compression Stress Maximum

FMX: Maximum Force

DFN: Final Displacement

VMX: Maximum Velocity

EFV: Maximum Energy

DMX: Maximum Displacement

ETR: Energy Transfer Ratio - Rated

BL#	LP ft	BC /6"	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
1	43.56	8	1.9	24	22.4	0.96	19.6	0.75	321	91.7
2	43.63	8	56.0	26	19.9	0.75	21.3	0.75	294	84.0
3	43.69	8	55.4	25	21.8	0.91	20.5	0.75	329	93.9
4	43.75	8	55.5	25	20.4	0.75	20.8	0.75	293	83.8
5	43.81	8	55.6	26	20.5	0.75	21.1	0.75	298	85.2
6	43.88	8	55.4	27	20.7	0.75	22.5	0.75	305	87.1
7	43.94	8	55.6	27	20.3	0.75	22.0	0.75	300	85.8
8	44.00	8	55.1	26	20.7	0.75	21.3	0.75	300	85.6
9	44.03	15	55.7	25	20.6	0.64	20.6	0.40	301	85.9
10	44.07	15	55.1	25	19.6	0.54	20.9	0.40	283	80.8
11	44.10	15	57.1	26	20.5	0.50	21.6	0.40	275	78.7
12	44.13	15	55.5	25	19.3	0.60	20.6	0.40	304	86.8
13	44.17	15	53.9	27	20.8	0.52	22.1	0.40	293	83.8
14	44.20	15	55.3	26	21.7	0.53	21.2	0.40	302	86.3
15	44.23	15	55.5	26	21.5	0.50	21.4	0.40	298	85.2
16	44.27	15	55.3	26	19.9	0.51	21.1	0.40	300	85.7
17	44.30	15	55.3	27	21.6	0.48	22.3	0.40	316	90.3
18	44.33	15	55.4	26	19.8	0.46	21.0	0.40	296	84.6
19	44.37	15	57.2	27	20.5	0.46	21.8	0.40	311	89.0
20	44.40	15	53.8	27	21.2	0.45	22.0	0.40	321	91.7
21	44.43	15	55.2	27	20.8	0.44	22.3	0.40	315	90.0
22	44.47	15	55.1	27	21.3	0.46	22.0	0.40	308	88.0
23	44.50	15	55.1	28	21.8	0.42	23.1	0.40	314	89.6
24	44.53	20	55.2	27	20.5	0.38	21.8	0.30	288	82.3
25	44.55	20	55.2	27	20.4	0.37	21.8	0.30	286	81.6
26	44.58	20	54.9	27	21.7	0.41	22.4	0.30	310	88.7
27	44.60	20	55.1	27	20.9	0.40	21.9	0.30	306	87.3

28	44.63	20	55.0	26	20.5	0.39	21.0	0.30	300	85.7
29	44.65	20	55.1	27	21.5	0.42	22.4	0.30	314	89.8
30	44.68	20	55.0	25	20.1	0.40	20.8	0.30	303	86.4
31	44.70	20	55.1	25	20.4	0.43	20.8	0.30	316	90.2
32	44.73	20	54.9	25	20.3	0.39	20.5	0.30	293	83.6
33	44.75	20	55.0	26	20.4	0.41	21.5	0.30	307	87.8
34	44.78	20	55.0	27	21.0	0.44	21.9	0.30	328	93.8
35	44.80	20	55.1	27	21.0	0.41	22.1	0.30	311	88.9
36	44.83	20	54.9	27	21.0	0.40	21.8	0.30	308	88.0
37	44.85	20	56.5	25	20.3	0.39	20.6	0.30	289	82.4
38	44.88	20	53.9	27	21.0	0.44	21.8	0.30	326	93.1
39	44.90	20	54.9	26	20.3	0.41	21.6	0.30	306	87.3
40	44.93	20	54.8	27	20.5	0.38	22.3	0.30	296	84.6
41	44.95	20	56.4	25	21.3	0.41	20.7	0.30	302	86.4
42	44.98	20	53.6	27	21.0	0.39	22.4	0.30	307	87.9
43	45.00	20	54.9	26	21.5	0.41	21.2	0.30	313	89.4
Average		55.2	26	20.8	0.45	21.6	0.34	304	86.9	
Std Dev		0.8	1	0.6	0.06	0.7	0.05	12	3.3	
Maximum		57.2	28	21.8	0.64	23.1	0.40	328	93.8	
Minimum		53.6	25	19.3	0.37	20.5	0.30	275	78.7	

N-value: 35

Sample Interval Time: 45.56 seconds.



Pile Dynamics, Inc. - PDIPILOT2 Ver 2022.1.62.0 - Case Method & iCAP® Results

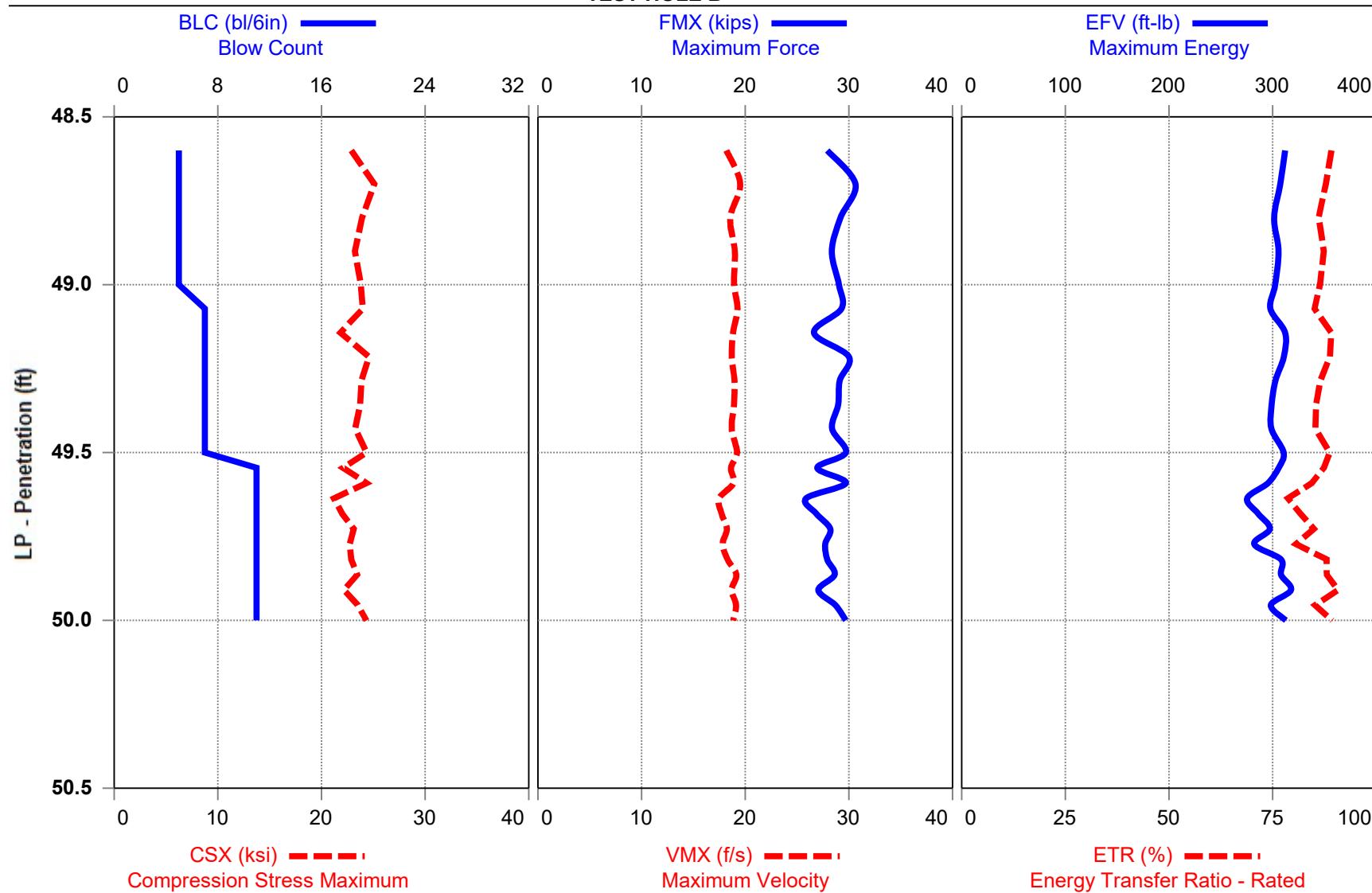
Printed: 14-December-2023

Test started: 17-November-2023



CME-550X SN 293193 - 48.5-50.0 FEET

TEST HOLE B



CME-550X SN 293193

JRW

TEST HOLE B

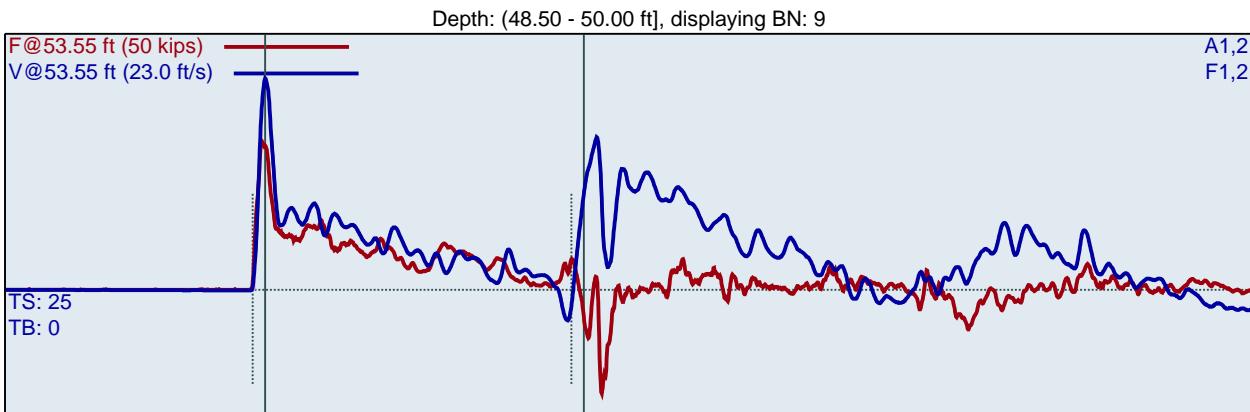
AR: 1.22 in²

LE: 53.55

WS: 16807.9 ft/s

43.5-45.0 FEET
Interval start: 11/17/2023

SP: 0.492 k/ft³
EM: 30000 ksi



F1 : [203 AWJ-1] 208.46 PDICAL (1) FF1
F2 : [203 AWJ-2] 208.57 PDICAL (1) FF1

A1 (PR): [K4664] 376.6 mv/6.4v/5000g (1) VF1
A2 (PR): [K4665] 375.3 mv/6.4v/5000g (1) VF1

Sample Interval Time: 23.95 seconds.



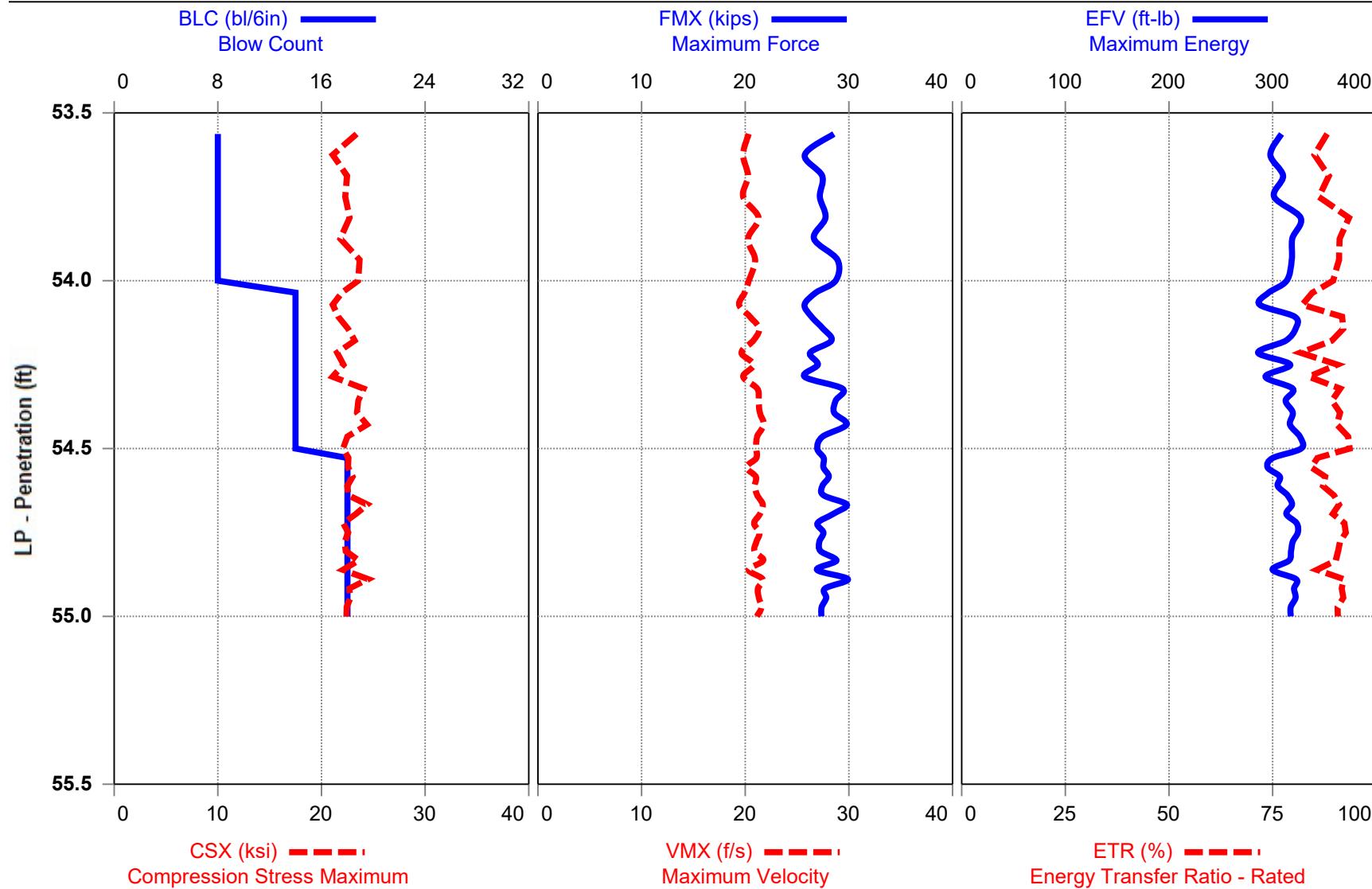
Printed: 14-December-2023

Pile Dynamics, Inc. - PDIPILOT2 Ver 2022.1.62.0 - Case Method & iCAP® Results

Test started: 17-November-2023



**CME-550X SN 293193 - 53.5-55.0 FEET
TEST HOLE B**



CME-550X SN 293193

JRW

TEST HOLE B

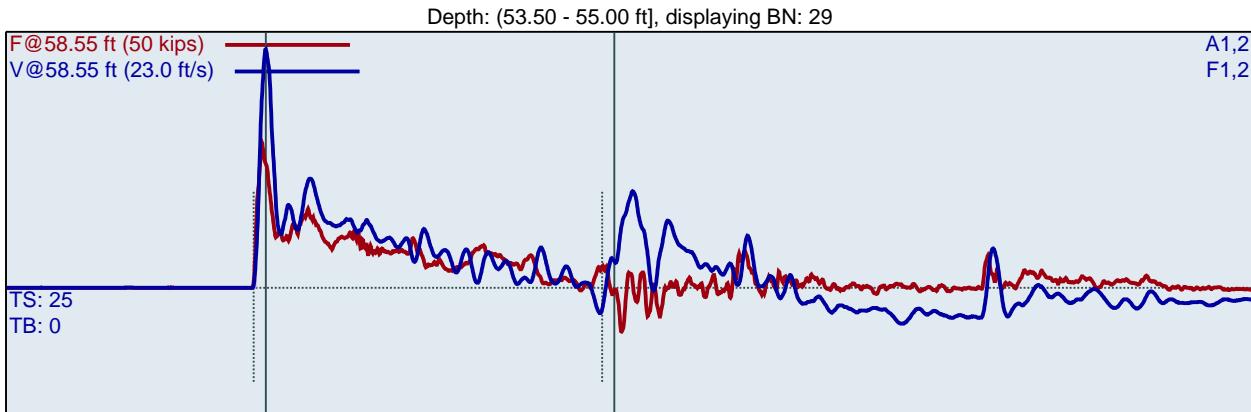
AR: 1.22 in²

LE: 58.55 ft

WS: 16807.9 ft/s

43.5-45.0 FEET
Interval start: 11/17/2023

SP: 0.492 k/ft3
EM: 30000 ksi



F1 : [203 AWJ-1] 208.46 PDICAL (1) FF1
F2 : [203 AWJ-2] 208.57 PDICAL (1) FF1

A1 (PR): [K4664] 376.6 mv/6.4v/5000g (1) VF1
A2 (PR): [K4665] 375.3 mv/6.4v/5000g (1) VF1

BL#	LP ft	BC /6"	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
1	53.56	8	1.9	29	20.3	1.10	23.4	0.75	308	88.1
2	53.63	8	56.4	26	19.8	0.89	21.1	0.75	298	85.0
3	53.69	8	55.0	27	20.3	0.83	22.5	0.75	310	88.5
4	53.75	8	55.5	27	19.8	0.77	22.3	0.75	301	86.1
5	53.81	8	55.0	28	21.3	0.75	22.7	0.75	327	93.4
6	53.88	8	55.3	27	20.3	0.75	21.8	0.75	319	91.1
7	53.94	8	55.1	29	21.0	0.75	23.7	0.75	318	91.0
8	54.00	8	55.2	29	20.3	0.76	23.5	0.75	313	89.6
9	54.04	14	55.3	27	19.9	0.56	22.0	0.43	296	84.6
10	54.07	14	56.9	26	19.4	0.55	21.1	0.43	287	82.1
11	54.11	14	53.3	26	20.5	0.58	21.6	0.43	321	91.7
12	54.14	14	55.5	28	21.3	0.55	22.6	0.43	322	92.0
13	54.18	14	55.1	28	20.8	0.53	23.2	0.43	312	89.2
14	54.21	14	56.6	26	19.6	0.51	21.5	0.43	286	81.7
15	54.25	14	53.6	27	20.8	0.53	22.1	0.43	317	90.6
16	54.29	14	56.7	26	19.8	0.50	21.1	0.43	293	83.7
17	54.32	14	53.9	29	21.2	0.51	24.1	0.43	319	91.3
18	54.36	14	54.7	29	21.3	0.47	23.5	0.43	313	89.3
19	54.39	14	55.1	29	21.4	0.49	23.4	0.43	319	91.3
20	54.43	14	55.2	30	21.8	0.47	24.4	0.43	317	90.5
21	54.46	14	54.9	30	21.1	0.47	24.2	0.43	319	91.2
22	54.50	14	55.1	29	21.1	0.48	23.8	0.43	320	91.3
23	54.53	18	56.6	28	21.1	0.45	22.6	0.33	300	85.8
24	54.56	18	53.5	28	20.1	0.45	22.6	0.33	295	84.3
25	54.58	18	55.1	28	21.0	0.46	23.0	0.33	307	87.7
26	54.61	18	55.1	27	20.9	0.44	22.5	0.33	305	87.1
27	54.64	18	55.0	28	21.2	0.46	22.6	0.33	314	89.8
28	54.67	18	55.1	30	21.7	0.47	24.4	0.33	319	91.0
29	54.69	18	55.1	28	21.4	0.46	23.3	0.33	313	89.5
30	54.72	18	54.8	27	20.9	0.48	22.1	0.33	323	92.3
31	54.75	18	55.1	28	21.4	0.48	22.6	0.33	324	92.6

32	54.78	18	55.1	27	21.1	0.46	22.3	0.33	319	91.2
33	54.81	18	54.9	29	20.9	0.45	23.8	0.33	321	91.6
34	54.83	18	55.0	29	21.7	0.46	23.6	0.33	316	90.2
35	54.86	18	55.0	27	20.3	0.42	22.1	0.33	300	85.7
36	54.89	18	54.9	30	21.7	0.44	24.5	0.33	323	92.2
37	54.92	18	55.1	28	21.2	0.44	22.7	0.33	321	91.6
38	54.94	18	54.7	28	21.3	0.42	22.8	0.33	322	92.0
39	54.97	18	54.8	27	21.6	0.41	22.4	0.33	317	90.7
40	55.00	18	54.6	27	21.1	0.42	22.4	0.33	317	90.7
Average		55.0	28	21.0	0.48	22.8	0.38	312	89.3	
Std Dev		0.8	1	0.6	0.04	0.9	0.05	11	3.1	
Maximum		56.9	30	21.8	0.58	24.5	0.43	324	92.6	
Minimum		53.3	26	19.4	0.41	21.1	0.33	286	81.7	

N-value: 32

Sample Interval Time: 42.36 seconds.

Summary of SPT Test Results

Project: CME-550X SN 293193, Test Date: 11/17/2023

BPM: Blows/Minute

CSX: Compression Stress Maximum

FMX: Maximum Force

DFN: Final Displacement

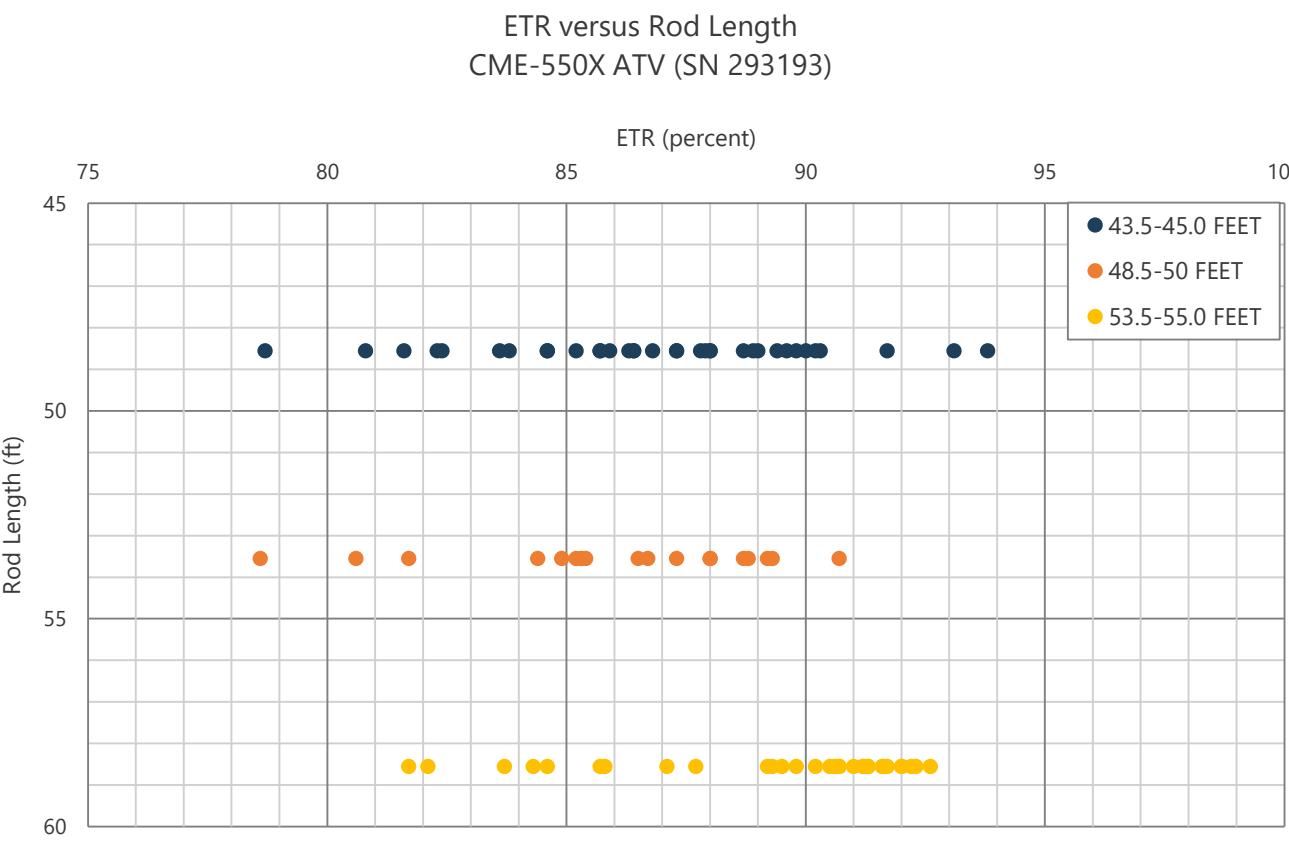
VMX: Maximum Velocity

EFV: Maximum Energy

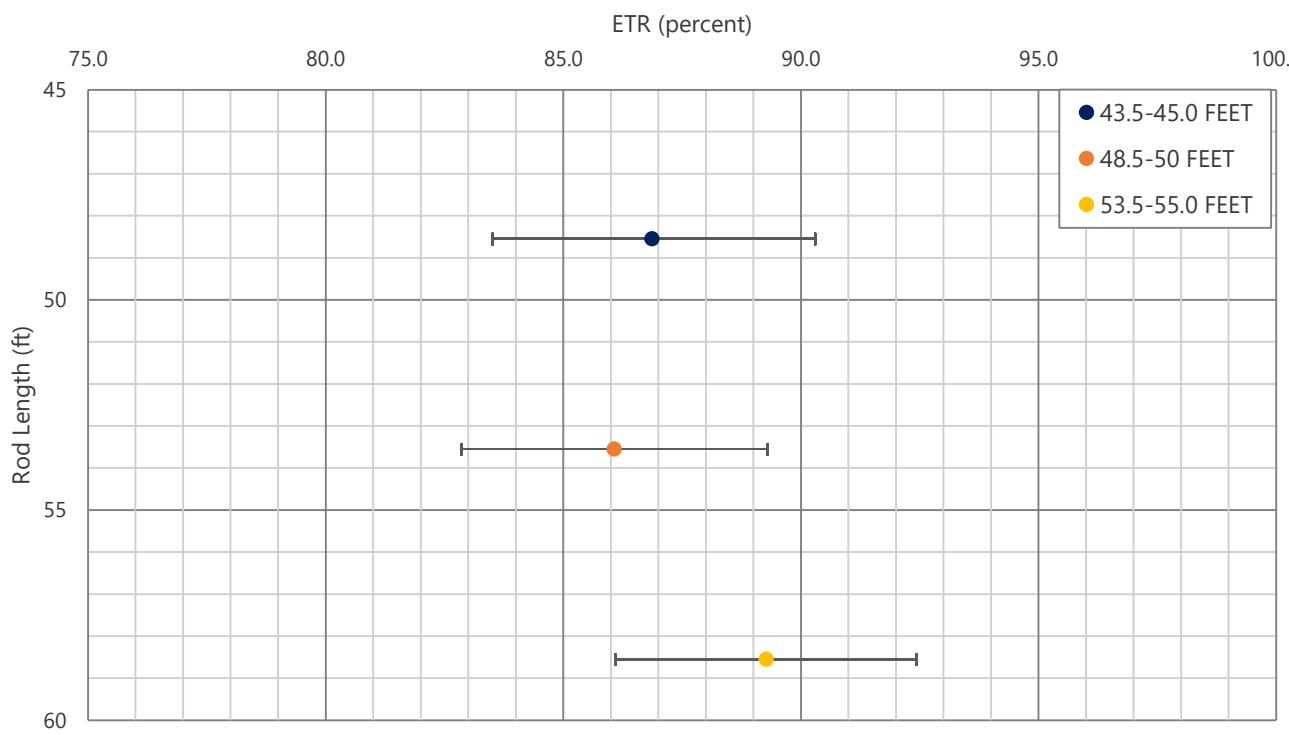
DMX: Maximum Displacement

ETR: Energy Transfer Ratio - Rated

Instr. Length ft	Start Depth ft	Final Depth ft	Blows Applied /6"	N Value	N60 Value	Average BPM bpm	Average FMX kips	Average VMX ft/s	Average DMX in	Average CSX ksi	Average DFN in	Average Efv ft-lb	Average ETR %
48.55	43.50	45.00	8-15-20	35	51	55.2	26	20.8	0.45	21.6	0.34	304	86.9
53.55	48.50	50.00	5-7-11	18	26	55.2	28	18.6	0.71	23.3	0.67	301	86.1
58.55	53.50	55.00	8-14-18	32	46	55.0	28	21.0	0.48	22.8	0.38	312	89.3
Overall Average Values:				55.1	27	20.4	0.51	22.4	0.42	307	87.6		
Standard Deviation:				0.8	1	1.1	0.14	1.1	0.15	12	3.5		
Overall Maximum Value:				57.2	31	21.8	0.99	25.4	0.86	328	93.8		
Overall Minimum Value:				53.3	25	17.5	0.37	20.5	0.30	275	78.6		



Average ETR versus Rod Length ± 1 Standard Deviation
CME-550X ATV (SN 293193)





Report of SPT Energy Measurements
S&ME CME-750X ATV (Serial No. 322938)
Columbia, South Carolina
S&ME Project No. 1535-22-200

PREPARED FOR:

**North Carolina Department of Transportation
Geotechnical Engineering Unit
1589 Mail Service Center
Raleigh, North Carolina 27699**

PREPARED BY:

**S&ME, Inc.
9751 Southern Pine Boulevard
Charlotte, North Carolina 28273**

December 23, 2022



December 23, 2022

North Carolina Department of Transportation
Geotechnical Engineering Unit
1589 Mail Service Center
Raleigh, North Carolina 27699

Attention: Mr. Greg Bodenheimer, P.E.

Cc: Ms. Cheryl A. Youngblood, L.G.
Ms. Christina M. Bruinsma, L.G.

Reference: **Report of SPT Energy Measurements**
S&ME CME-750X ATV (Serial No. 322938)
Columbia, South Carolina
S&ME Project No. 1535-22-200
NC PE Firm License No. F-0176

Dear Mr. Bodenheimer:

We have completed the Standard Penetration Test (SPT) energy measurements on the automatic hammer used with our CME-750X ATV-mounted drill rig (Serial No. 322938). This service was performed by Mr. Joseph Williamson, P.E. of our firm on November 10, 2022, in general accordance with ASTM D4633 and the most recent revision of the North Carolina Department of Transportation (NCDOT) Geotechnical Engineering Unit's requirements. Review of the data quality and analyses was performed by Mr. Williamson. A copy of the Certificate of Proficiency issued by Pile Dynamics based on the Dynamic Measurement and Analysis Proficiency Test for Mr. Williamson is included in Appendix I. The testing procedures, equipment used during testing, and detailed results are presented in this report.

1.0 Dynamic Testing Methodology

Testing was performed using a model PAX (Serial No. 3733L) Pile Driving Analyzer™ (PDA) manufactured by Pile Dynamics, Inc. The PDA was used to record and interpret data from two piezoresistive accelerometers (Serial Nos. K4664 and K4665) bolted to a 2.0-foot long AWJ drill rod (Serial No. 203) internally instrumented with two strain transducers. Calibration sheets for the accelerometers and the instrumented rod are included in Appendix II. The instrumented AWJ drill rod has a cross-sectional area of 1.19 square inches and an outside diameter of approximately 1.75 inches. Therefore, we calculate the inside diameter to be approximately 1.25 inches at the gauge location. The accelerometers and strain gauges, which are diametrically opposed near the middle of the instrumented rod, monitor acceleration and strain for each hammer blow. The analyzer converts the data to velocities and forces and computes the maximum transferred hammer energies with the "EFV" method described in ASTM D4633. Preliminary results are recorded and displayed in real time for each blow.



2.0 Testing and Observations

S&ME personnel were on site November 10, 2022, to observe and perform high-strain dynamic testing during SPT sampling on the CME-750X ATV-mounted drill rig operated by Sam Gowan of S&ME. The measurements were taken during drilling and sampling of a soil test boring performed on an S&ME project site in Columbia, South Carolina. SPT energy measurements presented herein were recorded during three sampling intervals that satisfied the NCDOT required blow count criteria. The information presented in the tables below summarizes the equipment and tooling used during the SPT energy measurements. The Boring Log and SPT Energy Evaluation Form is included in Appendix III.

Table 2-1: Drill Rig Information

Manufacturer	CME
Model	750X
Serial Number	322938
Operator	S. Gowan
Carrier	ATV

Table 2-2: Hammer Information

Model / Type	CME / Auto
Typical Drop Height (inches)	30
Typical Ram Weight (pounds)	140

Table 2-3: Drilling and Instrumented Rod Information

Drill Rod Type	AWJ
OD (inches)	1.75
ID (inches)	1.25
Cross-Sectional Area (in ²)	1.19
Typical Lengths (feet)	5
Instrumented Rod Type	AWJ (Serial No. 203)
OD (inches)	1.75
ID (inches)	1.25
Cross-Sectional Area (in ²)	1.19
Total Instrumented Rod Length (feet)	2.0
Length Below Gages (feet)	0.8
Split-Spoon Length (feet)	2.85



3.0 Dynamic Testing Results

The total rod length from the instrumentation to the tip of the split-spoon sampler was determined by adding 3.65 ft to the drill rod length at each sample depth. The SPT Energy Measurement Data Summary tables in Appendix IV present the test data from every hammer blow at each sampling interval, along with representative force and velocity traces for each test interval. Within some of the strain gauge (F2) records, electrical noise or "spikes" relatively late in the record (i.e., after $2L/c$) were observed. However, hammer impacts were relatively uniform and any bending appeared to be minor. Therefore, data collected from the F2 channel was excluded from the calculations when this phenomenon was observed. Per ASTM D4633, only the blows from the final foot of each sample interval (i.e. the blows that determine the N-value) are considered when computing the average measurement values of each test interval.

The reported blow counts obtained by the drill rig personnel, a summary of the test data, and average computed hammer energy and transfer ratio values are provided in Table 3-1. Based on the test data, the automatic hammer on the CME-750X operated at an average rate of about 53 blows per minute (bpm) during dynamic testing. The measured average transferred hammer energy (EFV) of the three sample intervals tested ranged from 281 to 291 ft-lbs, which corresponds to Energy Transfer Ratio (ETR) values of 80.4 to 83.2%, respectively, based on an assumed maximum energy of 350 ft-lbs. Plots and tables of the following are also included in the Appendix and present the test data with depth for each test interval:

- Penetration vs. BLC¹
- Penetration vs. FMX²
- Penetration vs. EFV³
- Penetration vs. CSX⁴
- Penetration vs. VMX⁵
- Penetration vs. ETR⁶
- ETR vs. Rod Length
- Average ETR vs. Rod Length

¹ BLC - Blow Count per 6-in. increment

² FMX - Maximum Compressive Force

³ EFV - Maximum Transferred Energy

⁴ CSX - Maximum Compressive Stress

⁵ VMX - Maximum Velocity

⁶ ETR - Energy Transfer Ratio - Ratio of Calculated Energy to Theoretical Energy of 140 lb hammer falling 30 inches



Table 3-1: Summary of Dynamic Testing Results

Data Set ID	Sample Depth (ft)	Drill Rod Length (ft)	Instrumentation to Sampler Tip Length (ft)	Blows per 6" Increment / N-value	Soil Sample Description	Avg. BPM	Avg. EFV (ft-lbs)	Avg. ETR (%)
1	43.5 – 45	45	48.65	3-4-4 / 8	Poorly Graded Sand with Silt ^A	53.4	291	83.2
2	48.5 – 50	50	53.65	8-19-27 / 46	Lean Clay ^{CP}	53.2	287	82.0
3	53.5 – 55	55	58.65	6-11-12 / 23	Silty Sand & Sandy Lean Clay ^{CP}	53.3	281	80.4
Overall Average						53.2	286	81.6

^A – Alluvium Soil Deposit; ^{CP} – Coastal Plain Soil Deposit

The overall average transferred hammer energy for the automatic hammer on the CME-750X ATV-mounted drill rig was 286 foot-pounds, with an average ETR of 81.6%.

4.0 Limitations of Report

This report has been prepared in accordance with generally accepted geotechnical engineering practice for specific application to this project. The conclusions contained in this report were based on the applicable standards of our profession in this geographic area at the time this report was prepared. No other warranty, express or implied, is made.



5.0 Closing

S&ME appreciates the opportunity to provide this report to the North Carolina Department of Transportation, Geotechnical Engineering Unit. Please let us know if you have any questions concerning this report.

Sincerely,

S&ME, Inc.

A handwritten signature in black ink, appearing to read "GJ".

Joseph R. Williamson, P.E.
Project Manager
N.C. Registration No. 42168

Gregory J. Canivan, P.E.
Technical Principal

Appendices:

- Appendix I - Certificate of Proficiency
- Appendix II - Instrumented Rod and Accelerometer Calibration Sheets
- Appendix III – Boring Log B-2 and SPT Energy Evaluation Form (Field Log)
- Appendix IV - CME-750X ATV (SN 322938) SPT Energy Measurements Summary Plots and Tables

Appendices

Appendix I



This documents that

**Joseph Williamson
S&ME, Inc.**



has on March 16, 2022 achieved the rank of

MASTER

on the Dynamic Measurement and Analysis Proficiency Test.

The individual identified on this document demonstrated to the degree granted above an understanding of theory, data quality evaluation, interpretation and signal matching for high strain dynamic testing of deep foundations. ***It is recommended that individuals at the Master level seek to attain Expert level through additional study within eight years of the date of this document***

The ability of the individual named to provide appropriate knowledge and advice on a specific project is not implied or warranted by the Pile Driving Contractors Association or Pile Dynamics, Inc. The Pile Driving Contractors Association or Pile Dynamics, Inc. assumes no liability for foundation testing and analysis work performed by the bearer of this certificate. This certificate can be verified at www.PDAproficiencytest.com.

A handwritten signature in blue ink that reads "Frank T. Peters".

Frank T. Peters, Executive Director
Pile Driving Contractors Association



A handwritten signature in blue ink that reads "Garland Likins".

Garland Likins, Senior Partner
Pile Dynamics, Inc.

No. 3251

Appendix II



PDI Certificate of Calibration

PDI Accelerometer Calibration

Model PR-K Serial # K4664

Cal Date: OCT 16, 2021

Cal Due : OCT 15, 2023

Temperature: 72 deg. F

Humidity 65 %

Calibrated at
Pile Dynamics, Inc.
30725 Aurora Road
Cleveland, OH 44139

Manufactured by Pile Dynamics, Inc.

Procedure used: PDA Accelerometer Calibration Procedure 2016-6, Revision 20160422

Equipment was found to be

in tolerance As Received out of tolerance As Received

in tolerance As Returned out of tolerance As Returned

PDI Calibration: 380 mv/5000g

Calibration Standards Utilized
Hopkinson Bar Force Calibration F2, verified on July 28, 2021

PDI HopBar DOS PAK, serial number 1273K, verified on July 19, 2021

Calibration performed by:

William Johnson, Technician

Reviewed by:

Robert Sprenger, Production Manager

Accelerometer CC-5 Issued 20160426

QBTA: ON [ALT-F1/BB=60]

Pile Dynamics, Inc.

TG F2 DPF

Pile Dynamics
1999-03-17 20:50FS — BN 1441 PJ:
SL 940/ 3440/ 2 PN: HOPBARA 4 -- US
F 2 3.3LE 39.6 ft
AR 1.7 in²
EM 30000 ksi
SP 0.492 K/ft³
WS 16815 ft/s
WC 17032 ft/sJC 0.40
FM 1.00
UM 1.00EA/C 30.3 Ks/ft
UN KIPS*0.1
FR 20000 MB 90DL -31
UT -1 IP 0.00
PK 1 TM-PEAKF1/2 500/ 213
F3/4 213/ 213
A1/2 999/ 999
A3/4 999/ 380TS 12 E B PD: K4664 LP 0.00 ft
TB 8.0 T1 9.4 2L/C 4.7 UA 1000 UE 1024 LI 1.0

ACCEPT SQ-OFF FL-OFF PR-OFF

ACCEPT



<-AT:PIEZORESISTIVE

VMX= 5.3 FMX= 84 AMX= 169
EMX= 0.4 MEX= 164 FVP= 1.00

ACCELEROMETER CALIBRATION N.I.S.T. Traceable

SERIAL NUMBER: K4664

CALIBRATION FACTOR: .076 m/s

PAK (*5000): 380 DATE: 10/16/2021

PDA OPERATOR: Will BH

OP: WILL [ver:5.01]

AT:PIEZOELECTRIC->

Smart Sensor

Programmed By: WJ

CRC Value 4898



PDI Certificate of Calibration

PDI Accelerometer Calibration

Model PR-1K Serial # K4665

Cal Date: AUG 10, 2021

Cal Due : AUG 9, 2023

Temperature: 72 deg. F

Humidity 70 %

Calibrated at
Pile Dynamics, Inc.
30725 Aurora Road
Cleveland, OH 44139

Manufactured by Pile Dynamics, Inc.

Procedure used: PDA Accelerometer Calibration Procedure 2016-6, Revision 20160422

Equipment was found to be

in tolerance As Received out of tolerance As Received

in tolerance As Returned out of tolerance As Returned

PDI Calibration: 365 mv/5000g

Calibration Standards Utilized
Hopkinson Bar Force Calibration F2, verified on July 28, 2021

PDI HopBar DOS PAK, serial number 1273K, verified on July 19, 2021

Calibration performed by: William Johnson
William Johnson, Technician

Reviewed by: Bob Sprenger
Bob Sprenger, production Manager

Accelerometer CC-5 Issued 20160426

QBTA: ON [ALT-F1/BB=60]

Pile Dynamics, Inc.

Pile Dynamics
1999-01-07 21:09

FS — BN 66

10 SL 805/ 3440/ 99

PJ:
PN: HOPBAR

TG F2 DPF

A 4 -- US

F 2 3.3

LE 39.6 ft
AR 1.7 in²
EM 30000 ksi
SP 0.492 K/ft³
WS 16815 ft/s
WC 16851 ft/s

JG 0.40
FM 1.00
UM 1.00

EA/C 30.3 Ks/ft

UN KIPS*0.1

FR 20000 MB 90

DL -44
UT -1 IP 0.00
PK 1 TM-PEAK

F1/2 500/ 213
F3/4 213/ 213
A1/2 999/ 999 TS 12
A3/4 999/ 365 TB 8.0 T1 9.6 E B PD: K4665
2L/C 4.7 VA 1000 UE 1024 LP 0.00 ft LI 1.0

ACCEPT SQ-OFF FL-OFF PR-OFF

ACCEPT



<-AT:PIEZORESISTIVE

VMX= 4.9 FMX= 75 AMX= 169
EMX= 0.3 MEX= 147 FVP= 0.98

ACCELEROMETER CALIBRATION N.I.S.T. Traceable

SERIAL NUMBER: K4665

CALIBRATION FACTOR: .073 m/s

PAK (*5000): 365 DATE: 8/10/2021

PDA OPERATOR: Wm JH

OP: WILL [ver:5.01]

AT:PIEZOELECTRIC->

Smart Sensor

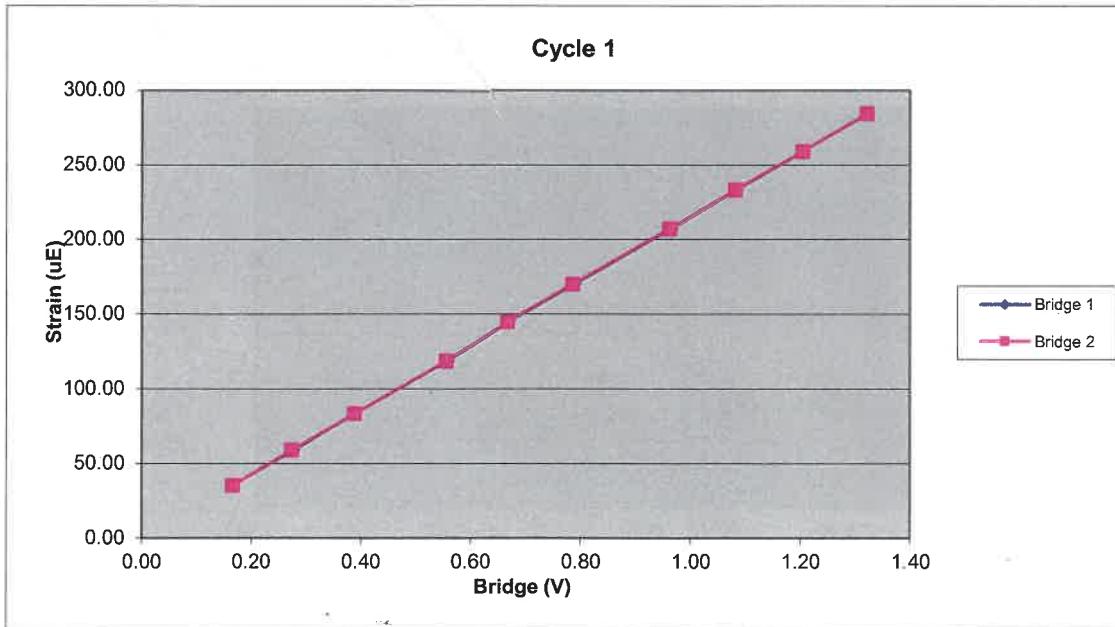
Programmed By: WJ

CRC Value C59F

203AWJ		Cycle 1		
Sample	Force (lb)	Strain (μE)	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	1246.03	34.91	0.17	0.17
3	2081.11	58.65	0.28	0.27
4	2941.63	83.02	0.39	0.39
5	4214.76	118.53	0.56	0.56
6	5056.27	144.80	0.67	0.67
7	5965.04	170.09	0.79	0.79
8	7294.42	207.16	0.96	0.96
9	8206.79	233.22	1.08	1.08
10	9138.76	259.03	1.21	1.20
11	10040.70	284.32	1.32	1.32

Bridge 1	Bridge 2
Force Calibration (lb/V)	7599.69
Offset	-24.15
Correlation	0.999998
Strain Calibration ($\mu\text{E}/\text{V}$)	215.94
Offset	-0.96
Correlation	0.999977
Force Calibration (lb/V)	7601.86
Offset	-17.41
Correlation	0.999998
Strain Calibration ($\mu\text{E}/\text{V}$)	216.00
Offset	-0.77
Correlation	0.999970

Force Strain Calibration	
EA (Kips)	35191.11
Offset	10.07
Correlation	0.999966

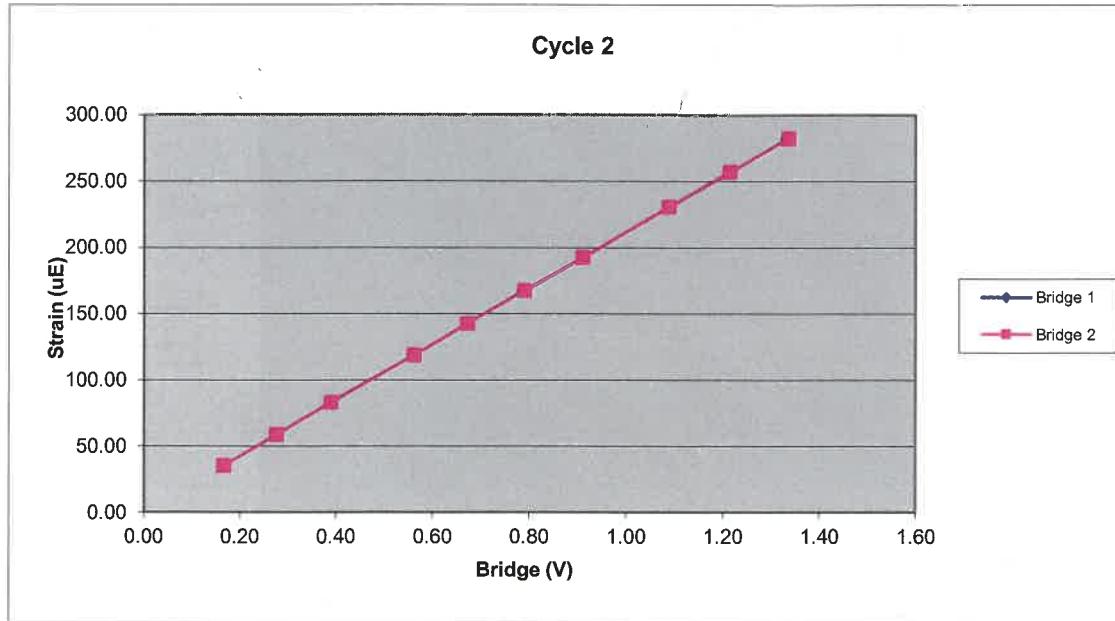


203AWJ		Cycle 2		
Sample	Force (lb)	Strain (μE)	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	1258.51	34.91	0.17	0.17
3	2095.24	58.34	0.28	0.28
4	2959.17	82.77	0.39	0.39
5	4259.41	118.34	0.56	0.56
6	5099.16	142.25	0.67	0.67
7	6003.44	167.19	0.79	0.79
8	6914.94	192.10	0.91	0.91
9	8280.29	230.44	1.09	1.09
10	9224.63	256.64	1.22	1.21
11	10143.64	281.95	1.33	1.34

Bridge 1	Bridge 2
Force Calibration (lb/V)	7599.73
Offset	-6.06
Correlation	0.999998
Strain Calibration ($\mu\text{E}/\text{V}$)	211.24
Offset	0.01
Correlation	0.999992
Force Calibration (lb/V)	7596.59
Offset	-5.65
Correlation	0.999998
Strain Calibration ($\mu\text{E}/\text{V}$)	211.15
Offset	0.02
Correlation	0.999991

Force Strain Calibration
EA (Kips)
Offset
Correlation

35976.99
-6.36
0.999996

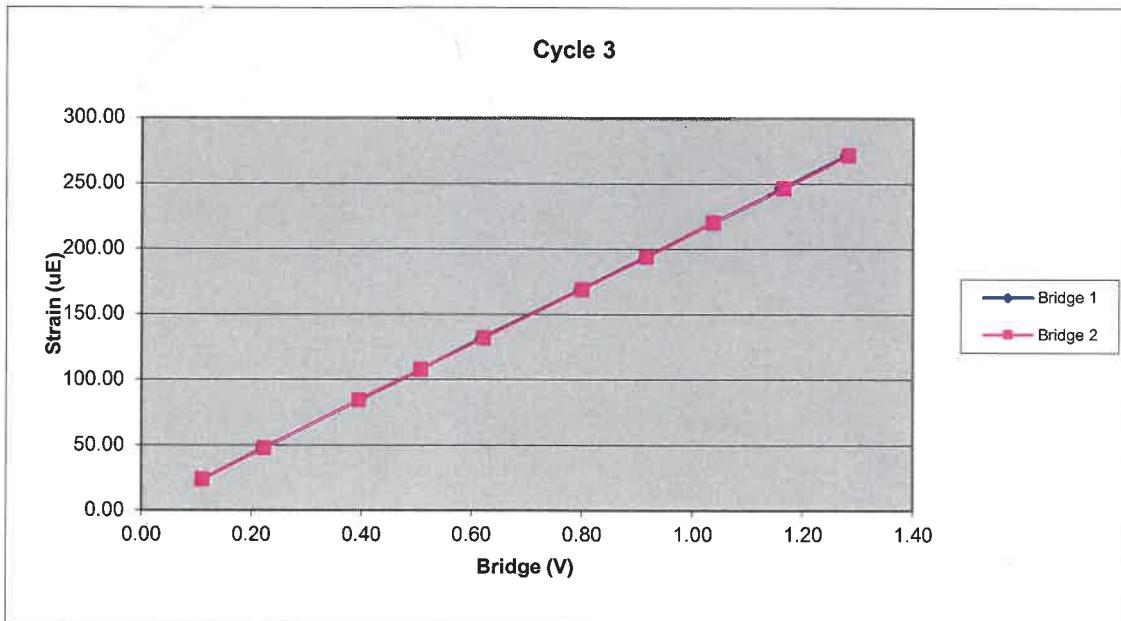


203AWJ		Cycle 3		
Sample	Force (lb)	Strain (μE)	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	846.19	23.53	0.11	0.11
3	1695.30	47.55	0.22	0.22
4	3007.23	84.21	0.40	0.40
5	3855.56	107.72	0.51	0.51
6	4714.72	131.93	0.62	0.62
7	6082.40	169.34	0.80	0.80
8	6969.72	194.06	0.92	0.92
9	7881.90	220.26	1.04	1.04
10	8834.83	246.28	1.16	1.17
11	9750.91	271.69	1.28	1.28

Bridge 1	Bridge 2
Force Calibration (lb/V)	7615.81
Offset	-9.63
Correlation	0.999996
Strain Calibration ($\mu\text{E}/\text{V}$)	212.11
Offset	0.00
Correlation	0.999995
Force Calibration (lb/V)	7596.50
Offset	-6.69
Correlation	0.999998
Strain Calibration ($\mu\text{E}/\text{V}$)	211.57
Offset	0.08
Correlation	0.999995

Force Strain Calibration
EA (Kips)
Offset
Correlation

35905.21
-9.52
0.999994



Bridge Excitation (V) 5
Shunt Resistor (ohm) 60.4k

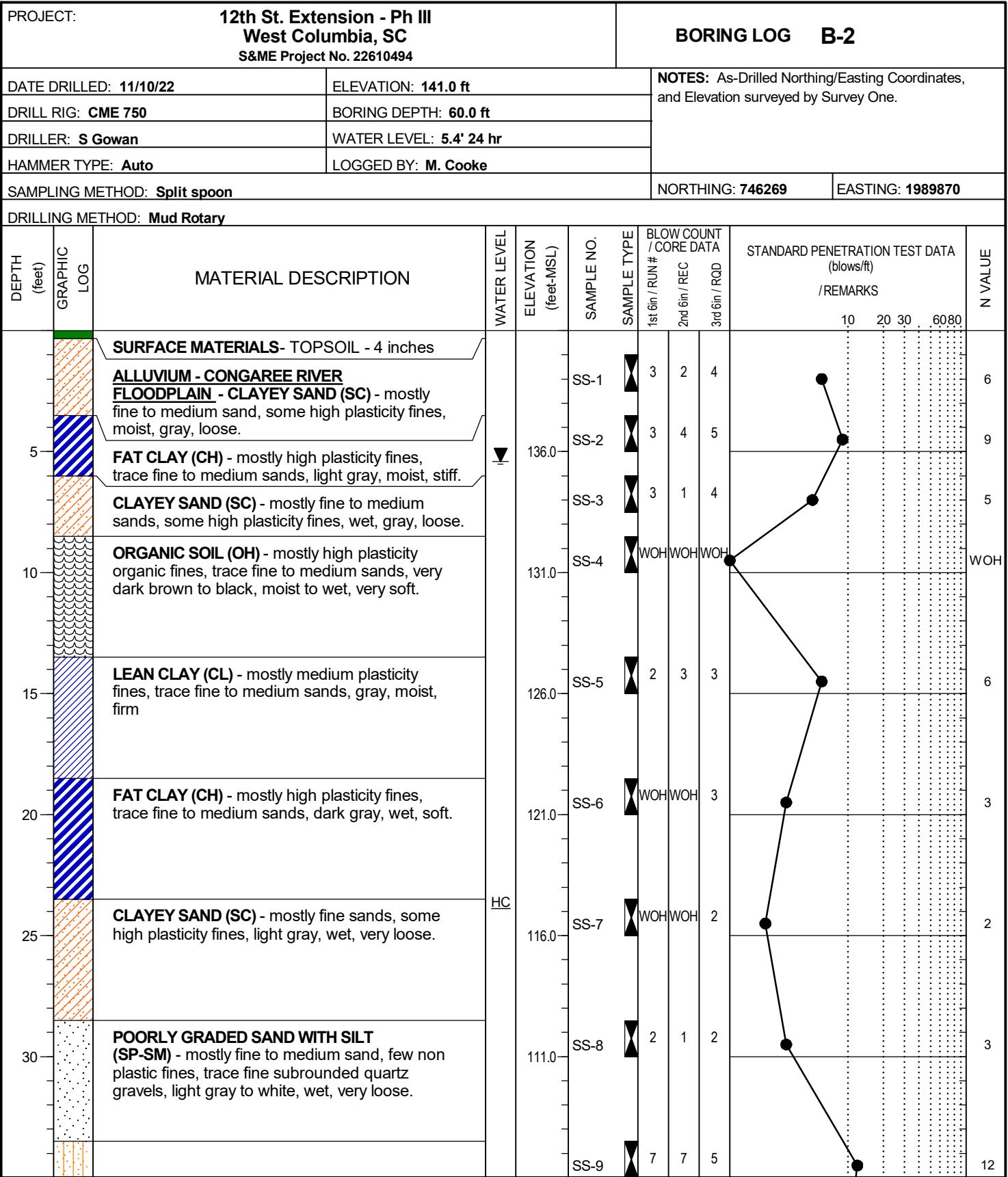
Calibration Factors	203AWJ		
Bridge 1 (μ E/V)	213.10	Bridge 2 (μ E/V)	212.91
EA Factor (Kips)	35691.10	Area (in ²)	1.19

Calibrated by: Albert J. Inc.
Calibrated Date: 3/25/2021

Pile Dynamics Inc
30725 Aurora Rd
Solon, OH 44139

Traceable to N.I.S.T.

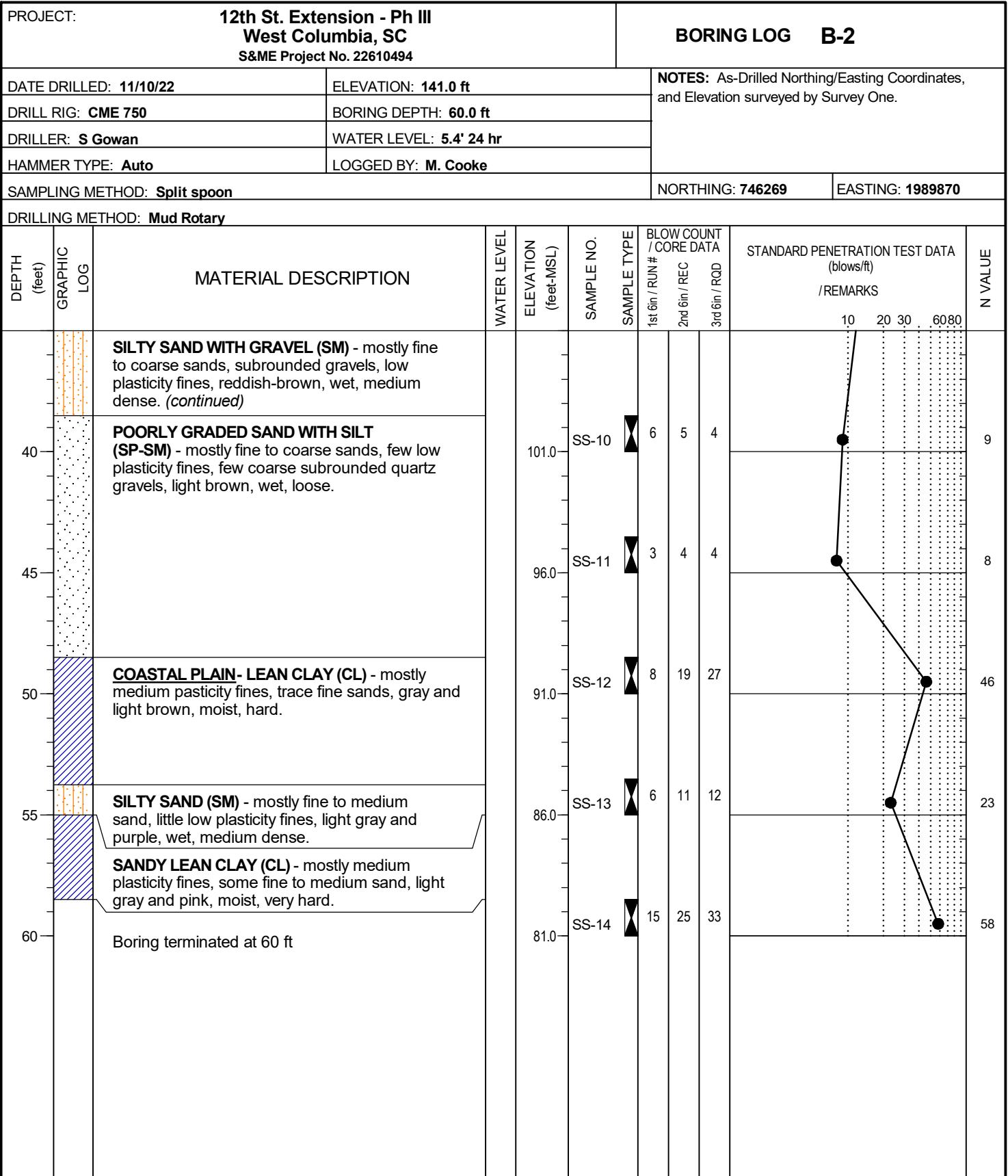
Appendix III



NOTES:

1. THIS LOG IS ONLY A PORTION OF A REPORT PREPARED FOR THE NAMED PROJECT AND MUST ONLY BE USED TOGETHER WITH THAT REPORT.
2. BORING, SAMPLING AND PENETRATION TEST DATA IN GENERAL ACCORDANCE WITH ASTM D-1586.
3. STRATIFICATION AND GROUNDWATER DEPTHS ARE NOT EXACT.
4. WATER LEVEL IS AT TIME OF EXPLORATION AND WILL VARY.





NOTES:

1. THIS LOG IS ONLY A PORTION OF A REPORT PREPARED FOR THE NAMED PROJECT AND MUST ONLY BE USED TOGETHER WITH THAT REPORT.
2. BORING, SAMPLING AND PENETRATION TEST DATA IN GENERAL ACCORDANCE WITH ASTM D-1586.
3. STRATIFICATION AND GROUNDWATER DEPTHS ARE NOT EXACT.
4. WATER LEVEL IS AT TIME OF EXPLORATION AND WILL VARY.





SPT Energy Evaluation Form

Project: ANNUAL SPT ENERGY MEASUREMENT
Project No.: 1535-22-200
Boring No.: B-2

Date: 11/10/2022
Weather: OVERCAST 60's
Drill Rod Type: 5-FT LONG AWJ

On-site Personnel

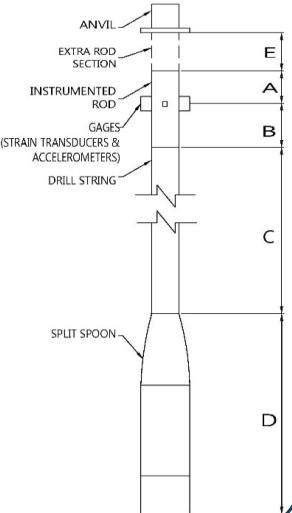
Drilling Company: S&ME
Rig Operator: S. GOWAN
Engr/Geologist: N/A
Client Rep.: N/A
Analyzer Oper.: J. WILLIAMSON

Rig/Hammer Info

Drill Rig Make/Model: CME-750X
Carrier Type: ATV
Rig Serial No.: 322938
Hammer Type/Model: CME / AUTO
Hammer Serial No.: N/A
Hammer Drop System: CHAIN DRIVE
Lubrication Condition: PER MANUFACTURERS RECS
Manufacturer Recommended
Operation Rate (bpm): 50-55
Typical Drop Height (in.): 30
Typical Hammer Weight (lbs): 140
Anvil Dimension (in.): 12
Drilling Method: MUD ROTARY w/ 2-7/8" DRAG BIT
Drop Height in Tolerance (y/n) YES

Rod Info

(A) + (B) Instr. Rod Length: 2.0 ft
(B) Instr. Rod Length below Gages: 0.8 ft
(D) Spoon Length: 2.85 ft
(E) Rod Length Above Instr. Rod (if applicable): - ft
(B)+(C)+(D) (LE) - Length Below Gauges (C) +3.65 ft
Instr. Rod S/N: 203AWJ
Instr. Rod Outside Dia.: 1.75 in.
Instr. Rod Area: 1.19 in²
PDA Make/Model: PDI / PAX
PDA Serial No.: 3733L
Calib. Pulse Test (y/n): YES



Gage Info

Gage		Serial No.	Calibration No.
Accel.	A1	K4664	380.0
	A2	K4665	365.0
Strain	F1	203AWJ-1	213.10
	F2	203AWJ-2	212.91

Date of Test	Test Depth Increment (ft to ft)	Test Time Start / Stop (military)	Length of Drill String (ft) (C)	(LE) Length below Gages (ft) (B) + (C) + (D)	Avg. Meas. Hammer Rate (BPM)	SPT Blow Counts						AASHTO / USCS Classification
						Total Blows by PDA	6"	12"	18"	N-Value	Extra Blows	
11/10/2022	28.5 - 30	10:21	30	33.65	53	5	2	1	2	3	0	SP-SM
	33.5 - 35	10:28	35	38.65	53	18	7	7	5	12	0	SM
	38.5 - 40	10:36	40	43.65	53	17	6	5	4	9	0	SP-SM
	43.5 - 45	10:56	45	48.65	53	11	3	4	4	8	0	SP-SM
	48.5 - 50	11:07	50	53.65	53	56	8	19	27	46	2	CL
	53.5 - 55	11:18	55	58.65	53	29	6	11	12	23	0	SM
	58.5 - 60	11:28	60	63.65	53	73	15	25	33	58	0	CL

Notes: 33.5-35 ft - PDA missed 1 blow plus 1 bad blow = 2 missed blows.

38.5 - 40 ft - Bad Data from PDA. Switched pig tail & main cable & reconfigured wire attachments.

F2 gauge spiking after 2L/c in various blows in all data sets.

NOTE: (1) Note any unusual hammer operating conditions that affect the hammer performance, or changes in operating conditions (e.g. veritcality, weather, or lubrication between trials). (2) Note any changes in rod diameter along drill string and record locations of short rod sections.

11/10/2022

Date

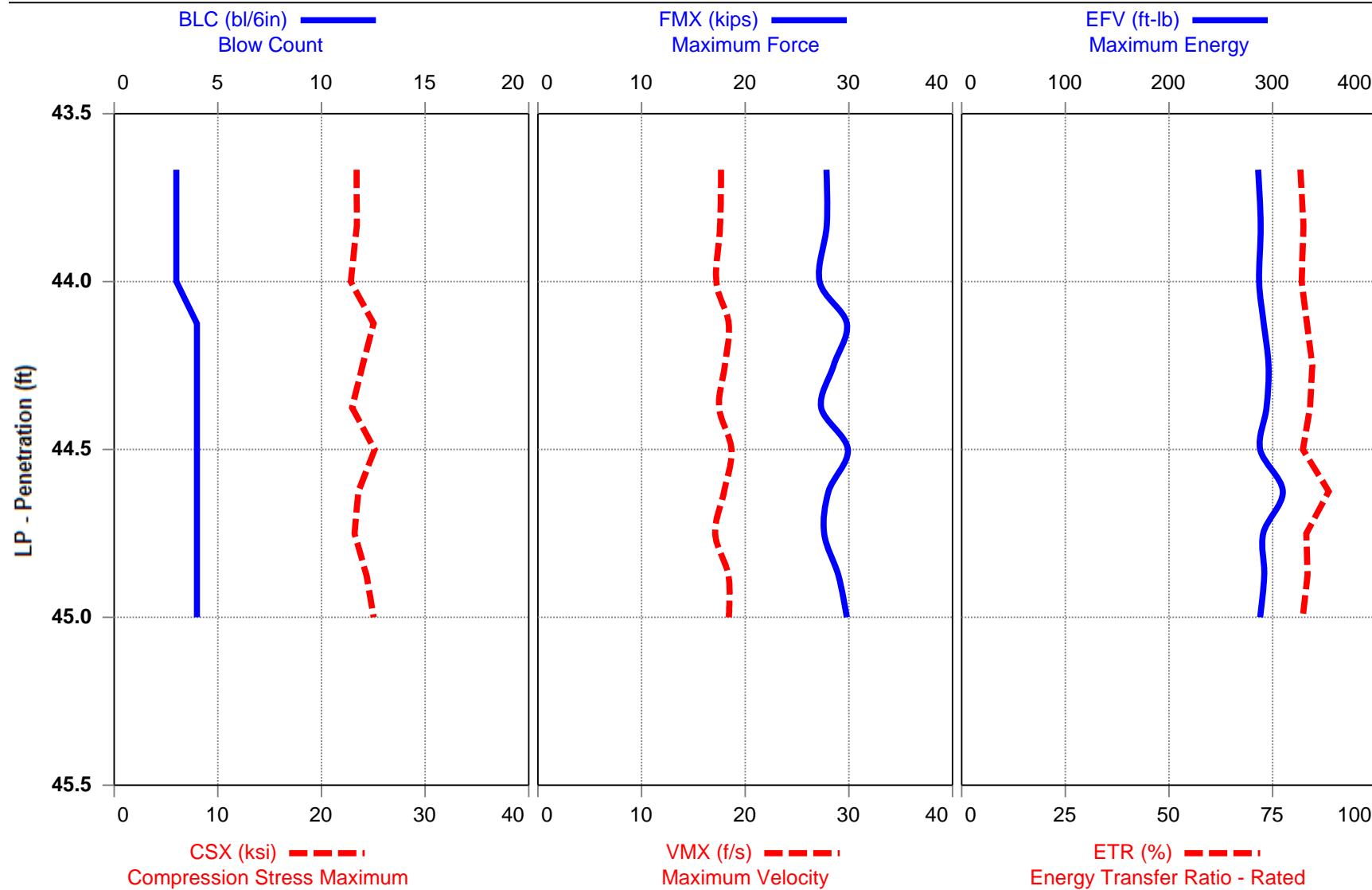
Prepared By (print/signature)

Appendix IV



CME-750X (SN 322938) - 43.5-45.0 FEET

B-2



CME-750X (SN 322938)

JRW

B-2

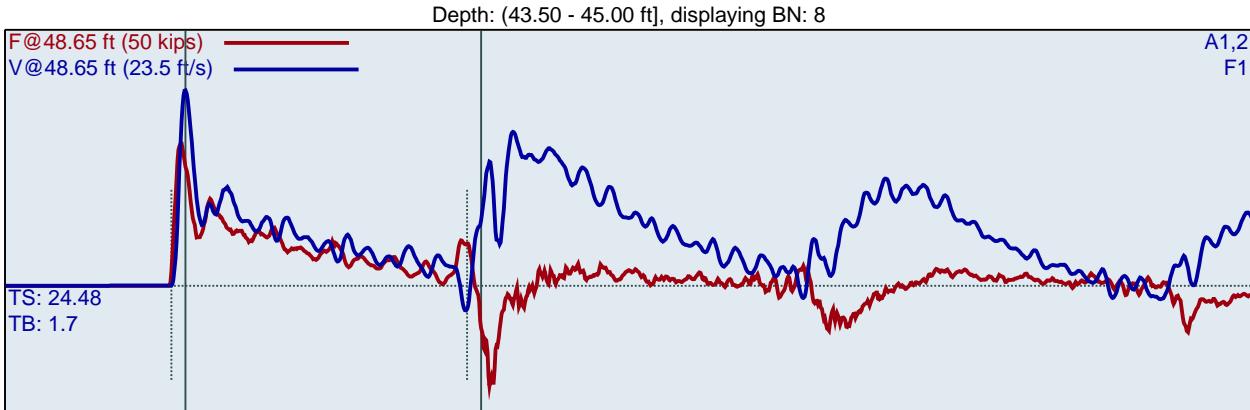
AR: 1.19 in²

LE: 48.65 ft

WS: 16807.9 ft/s

Annual Energy Measurements
Interval start: 11/10/2022

SP: 0.492 k/ft³
EM: 30000 ksi



F1 : [203 AWJ-1] 213.1 PDICAL (1) FF1
F2 : [203 AWJ-2] 212.91 PDICAL (1) FF1

A1 (PR): [K4664] 380 mv/6.4v/5000g (1) VF1
A2 (PR): [K4665] 365 mv/6.4v/5000g (1) VF1

BPM: Blows/Minute

CSX: Compression Stress Maximum

FMX: Maximum Force

DFN: Final Displacement

VMX: Maximum Velocity

EFV: Maximum Energy

DMX: Maximum Displacement

ETR: Energy Transfer Ratio - Rated

BL#	LP ft	BC /6"	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
1	43.67	3	1.9	28	17.7	2.00	23.4	2.00	286	81.7
2	43.83	3	53.5	28	17.6	2.00	23.4	2.00	288	82.4
3	44.00	3	53.7	27	17.2	2.00	22.8	2.00	287	82.0
4	44.13	4	53.5	29	18.4	1.67	24.5	1.50	291	83.3
5	44.25	4	53.2	29	18.0	1.54	24.0	1.50	296	84.6
6	44.38	4	53.3	27	17.5	1.50	23.0	1.50	294	84.0
7	44.50	4	53.6	29	18.7	1.50	24.6	1.50	288	82.4
8	44.63	4	53.4	28	18.0	1.52	23.4	1.50	291	83.2
9	44.75	4	53.2	27	17.1	1.77	22.9	1.50	290	82.8
10	44.88	4	53.3	29	18.4	1.60	24.4	1.50	292	83.4
11	45.00	4	53.4	30	18.4	1.50	25.0	1.50	288	82.2
Average			53.4	29	18.1	1.58	24.0	1.50	291	83.2
Std Dev			0.1	1	0.5	0.09	0.8	0.00	3	0.7
Maximum			53.6	30	18.7	1.77	25.0	1.50	296	84.6
Minimum			53.2	27	17.1	1.50	22.9	1.50	288	82.2

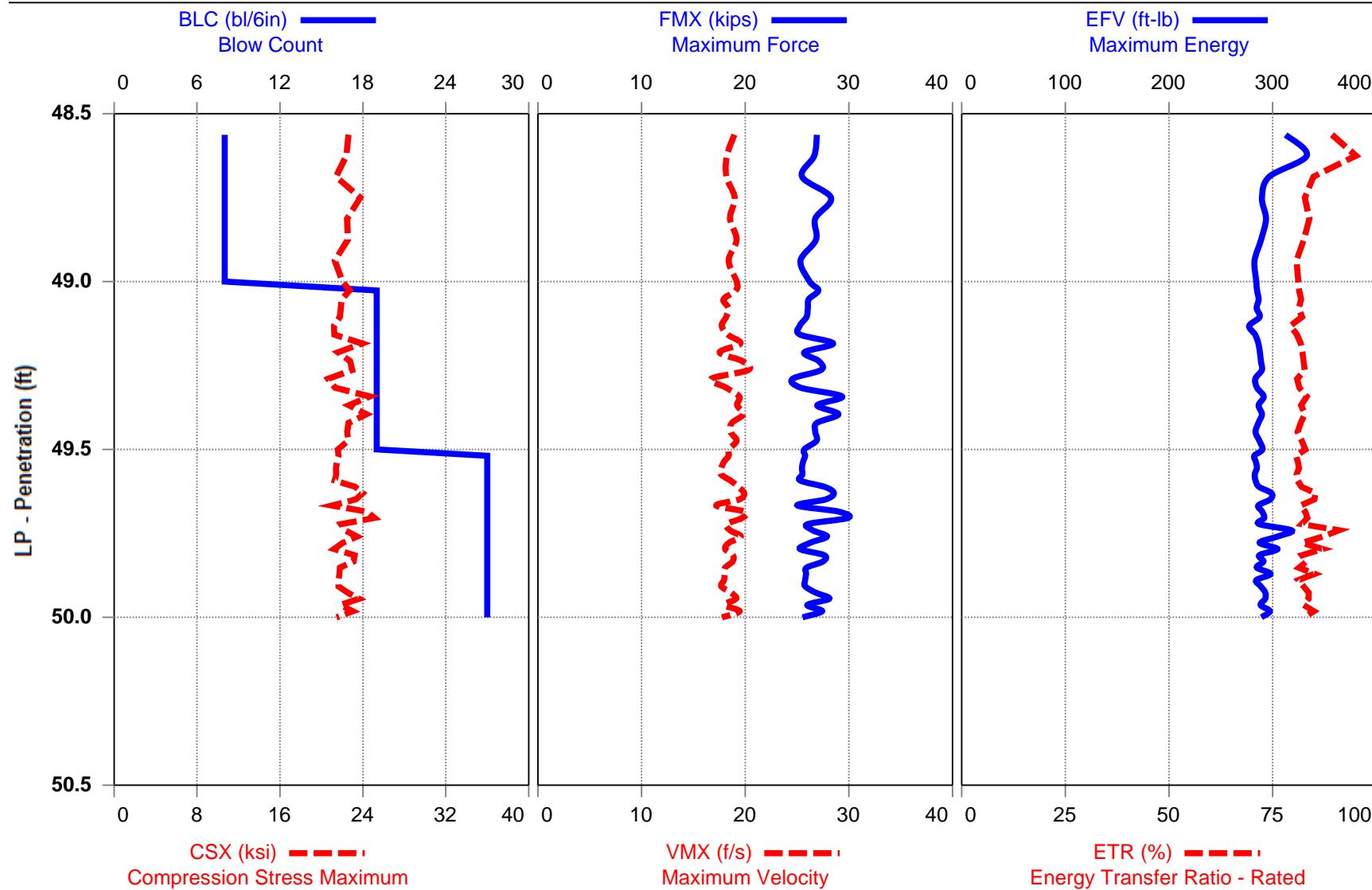
N-value: 8

Sample Interval Time: 11.22 seconds.



CME-750X (SN 322938) - 48.5-50.0 FEET

B-2



CME-750X (SN 322938)

JRW

B-2

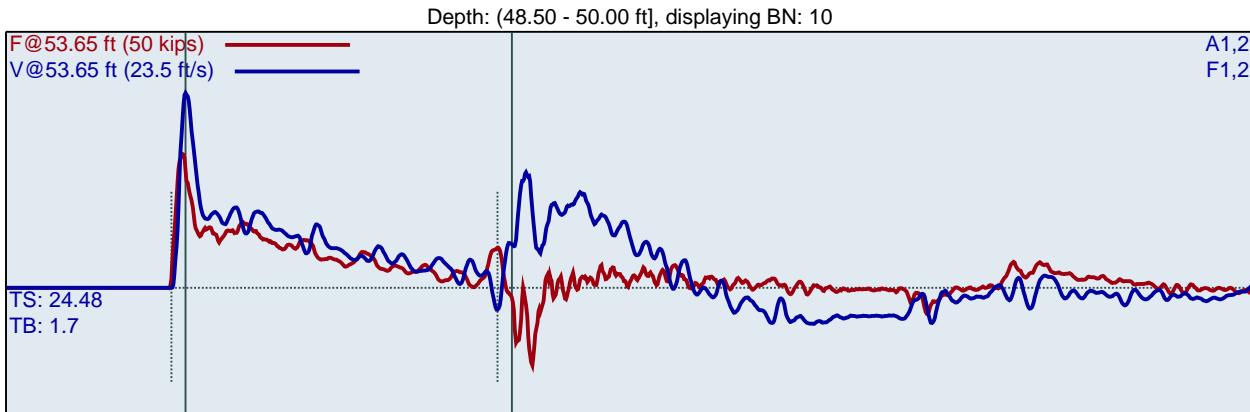
AR: 1.19 in²

LE: 53.65 ft

WS: 16807.9 ft/s

Annual Energy Measurements
Interval start: 11/10/2022

SP: 0.492 k/ft³
EM: 30000 ksi



F1 : [203 AWJ-1] 213.1 PDICAL (1) FF1

A1 (PR): [K4664] 380 mv/6.4v/5000g (1) VF1
A2 (PR): [K4665] 365 mv/6.4v/5000g (1) VF1

BL#	LP ft	BC /6"	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
1	48.56	8	1.9	27	19.0	1.18	22.6	0.75	296	84.5
2	48.63	8	42.7	27	18.2	0.99	22.3	0.75	290	82.7
3	48.69	8	54.0	25	18.2	0.79	21.3	0.75	282	80.5
4	48.75	8	53.3	28	19.0	0.75	23.2	0.75	291	83.1
5	48.81	8	53.5	26	18.5	0.75	22.3	0.75	290	82.9
6	48.88	8	53.3	27	19.2	0.75	22.3	0.75	287	81.9
7	48.94	8	53.5	25	18.4	0.75	21.1	0.75	283	80.8
8	49.00	8	53.5	26	19.2	0.75	21.9	0.75	284	81.2
9	49.03	19	53.2	27	19.1	0.56	22.5	0.32	286	81.7
10	49.05	19	53.6	26	17.9	0.56	22.0	0.32	286	81.8
11	49.08	19	53.2	26	18.4	0.54	21.8	0.32	285	81.4
12	49.11	19	53.3	26	18.2	0.54	21.6	0.32	288	82.2
13	49.13	19	53.8	25	17.7	0.52	21.2	0.32	277	79.2
14	49.16	19	53.2	25	18.3	0.51	21.2	0.32	283	80.8
15	49.18	19	53.4	28	19.5	0.50	23.7	0.32	283	81.0
16	49.21	19	53.1	24	17.5	0.51	20.6	0.32	287	81.9
17	49.24	19	53.1	27	19.7	0.51	22.7	0.32	288	82.2
18	49.26	19	53.1	28	20.3	0.49	23.1	0.32	289	82.5
19	49.29	19	53.0	24	16.7	0.49	20.2	0.32	283	80.9
20	49.32	19	53.2	25	18.1	0.48	21.1	0.32	285	81.5
21	49.34	19	53.1	29	19.4	0.48	24.3	0.32	292	83.3
22	49.37	19	52.8	27	19.2	0.46	22.4	0.32	287	82.0
23	49.39	19	53.8	29	19.8	0.46	24.0	0.32	290	82.9
24	49.42	19	53.2	27	18.7	0.45	22.6	0.32	287	81.9
25	49.45	19	53.1	27	18.6	0.44	22.5	0.32	284	81.0
26	49.47	19	53.0	27	19.2	0.44	22.5	0.32	286	81.8
27	49.50	19	53.3	26	18.4	0.44	22.0	0.32	289	82.7
28	49.52	27	53.1	26	18.4	0.42	21.5	0.22	282	80.6
29	49.54	27	52.9	26	17.9	0.43	21.4	0.22	284	81.2
30	49.56	27	53.4	25	17.7	0.43	21.2	0.22	285	81.5
31	49.57	27	53.1	25	17.7	0.42	21.3	0.22	283	80.9

32	49.59	27	52.9	25	18.6	0.41	21.2	0.22	283	80.8
33	49.61	27	53.2	27	19.3	0.41	23.1	0.22	286	81.7
34	49.63	27	52.9	28	19.9	0.41	23.8	0.22	287	82.0
35	49.65	27	53.3	28	19.5	0.43	23.2	0.22	291	83.3
36	49.67	27	53.1	25	17.2	0.41	20.9	0.22	286	81.7
37	49.69	27	53.2	29	20.0	0.41	24.0	0.22	289	82.7
38	49.70	27	52.9	30	19.7	0.41	24.9	0.22	291	83.3
39	49.72	27	53.2	26	18.2	0.41	22.1	0.22	287	82.0
40	49.74	27	53.2	27	18.5	0.41	22.6	0.22	290	82.9
41	49.76	27	53.2	28	19.6	0.41	23.4	0.22	289	82.5
42	49.78	27	53.0	26	18.4	0.41	22.3	0.22	287	82.1
43	49.80	27	53.2	25	18.1	0.40	21.4	0.22	286	81.6
44	49.81	27	53.1	28	18.8	0.39	23.4	0.22	286	81.7
45	49.83	27	52.9	28	18.8	0.40	23.3	0.22	290	82.8
46	49.85	27	53.2	26	18.1	0.39	21.8	0.22	285	81.3
47	49.87	27	53.1	26	18.0	0.39	21.6	0.22	288	82.2
48	49.89	27	53.2	26	17.9	0.39	21.6	0.22	285	81.3
49	49.91	27	52.9	26	17.7	0.39	21.5	0.22	288	82.3
50	49.93	27	53.1	27	18.6	0.39	23.0	0.22	291	83.2
51	49.94	27	52.9	28	19.1	0.39	23.6	0.22	292	83.4
52	49.96	27	53.1	26	18.0	0.38	21.8	0.22	288	82.3
53	49.98	27	53.2	27	19.5	0.40	23.1	0.22	294	84.1
54	50.00	27	53.2	25	17.8	0.39	21.4	0.22	288	82.3
Average		53.2	27	18.6	0.44	22.3	0.26	287	82.0	
Std Dev		0.2	1	0.8	0.05	1.1	0.05	3	0.9	
Maximum		53.8	30	20.3	0.56	24.9	0.32	294	84.1	
Minimum		52.8	24	16.7	0.38	20.2	0.22	277	79.2	

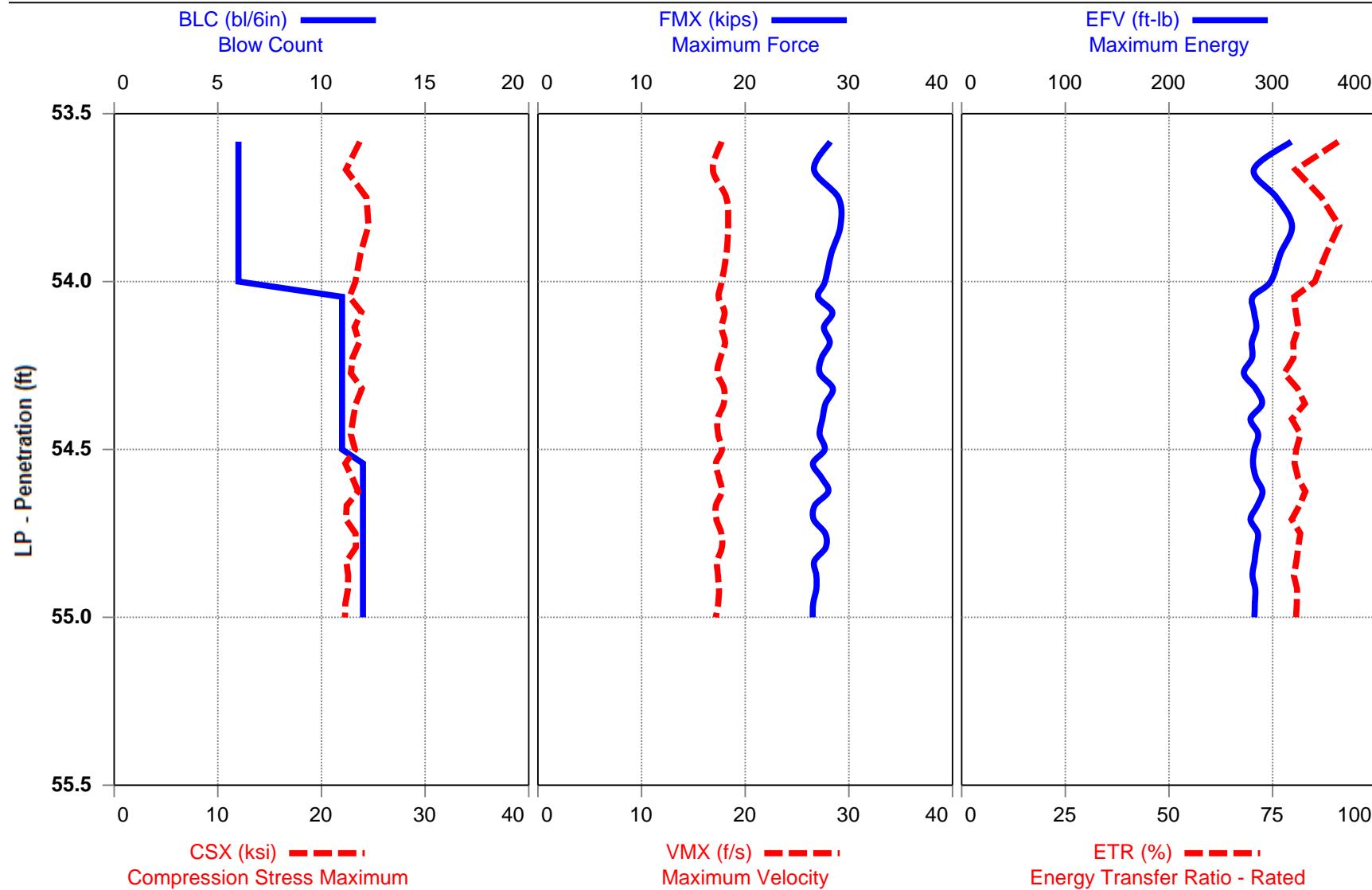
N-value: 46

Sample Interval Time: 59.96 seconds.



CME-750X (SN 322938) - 53.5-55.0 FEET

B-2



CME-750X (SN 322938)

JRW

B-2

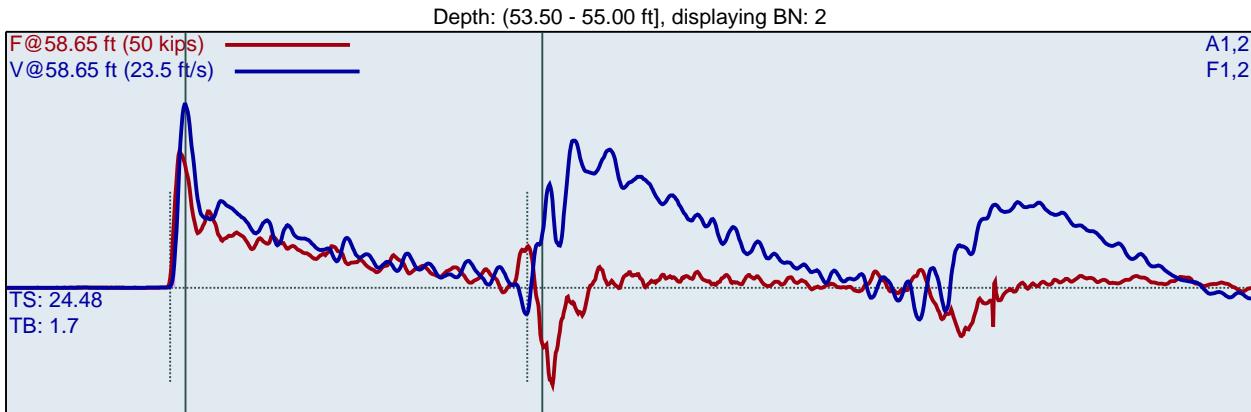
AR: 1.19 in²

LE: 58.65 ft

WS: 16807.9 ft/s

Annual Energy Measurements
Interval start: 11/10/2022

SP: 0.492 k/ft³
EM: 30000 ksi



F1 : [203 AWJ-1] 213.1 PDICAL (1) FF1

A1 (PR): [K4664] 380 mv/6.4v/5000g (1) VF1
A2 (PR): [K4665] 365 mv/6.4v/5000g (1) VF1

BL#	LP ft	BC /6"	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
1	53.58	6	1.9	28	17.7	1.41	23.4	1.00	296	84.6
2	53.67	6	55.5	27	16.9	1.15	22.4	1.00	282	80.5
3	53.75	6	53.3	28	18.2	1.00	23.8	1.00	288	82.2
4	53.83	6	53.2	28	18.3	1.00	23.9	1.00	289	82.7
5	53.92	6	53.4	28	18.2	1.00	23.5	1.00	287	82.1
6	54.00	6	53.4	28	17.7	1.00	23.2	1.00	291	83.3
7	54.05	11	53.5	27	17.4	0.61	22.6	0.55	281	80.2
8	54.09	11	53.0	29	18.0	0.57	24.1	0.55	280	80.1
9	54.14	11	53.5	28	17.7	0.60	23.1	0.55	283	80.9
10	54.18	11	53.3	28	18.0	0.58	23.9	0.55	278	79.5
11	54.23	11	53.6	27	17.6	0.58	22.9	0.55	277	79.0
12	54.27	11	53.2	27	17.3	0.57	22.5	0.55	271	77.6
13	54.32	11	53.4	28	18.0	0.57	23.3	0.55	282	80.4
14	54.36	11	53.2	27	17.9	0.58	22.5	0.55	283	80.8
15	54.41	11	53.5	27	17.3	0.58	22.4	0.55	278	79.4
16	54.45	11	53.0	27	17.4	0.59	22.3	0.55	284	81.1
17	54.50	11	53.4	27	17.7	0.56	22.8	0.54	281	80.4
18	54.54	12	53.2	26	17.2	0.57	21.9	0.50	281	80.4
19	54.58	12	53.4	27	17.5	0.56	22.6	0.50	283	80.8
20	54.63	12	53.2	27	17.7	0.60	22.9	0.50	290	82.7
21	54.67	12	53.1	26	17.2	0.58	22.2	0.50	285	81.3
22	54.71	12	53.5	26	17.2	0.57	22.1	0.50	279	79.6
23	54.75	12	53.2	27	17.7	0.57	23.0	0.50	284	81.2
24	54.79	12	53.4	27	17.7	0.59	22.9	0.50	284	81.1
25	54.83	12	53.4	26	17.3	0.59	22.1	0.50	282	80.6
26	54.88	12	53.4	26	17.4	0.58	22.2	0.50	280	80.1
27	54.92	12	53.0	27	17.5	0.57	22.4	0.50	282	80.6
28	54.96	12	53.2	26	17.4	0.58	22.1	0.50	282	80.6
29	55.00	12	53.4	27	17.2	0.58	22.3	0.50	281	80.3

S&ME, Inc.
SPT Analyzer Results

Page 5 of 6
PDA-S Ver. 2021.34 - Printed: 12/23/2022

Average	53.3	27	17.5	0.58	22.7	0.52	281	80.4
Std Dev	0.2	1	0.3	0.01	0.5	0.02	3	1.0
Maximum	53.6	29	18.0	0.61	24.1	0.55	290	82.7
Minimum	53.0	26	17.2	0.56	21.9	0.50	271	77.6

N-value: 23

Sample Interval Time: 31.43 seconds.

Summary of SPT Test Results

Project: CME-750X (SN 322938), Test Date: 11/10/2022

BPM: Blows/Minute

CSX: Compression Stress Maximum

FMX: Maximum Force

DFN: Final Displacement

VMX: Maximum Velocity

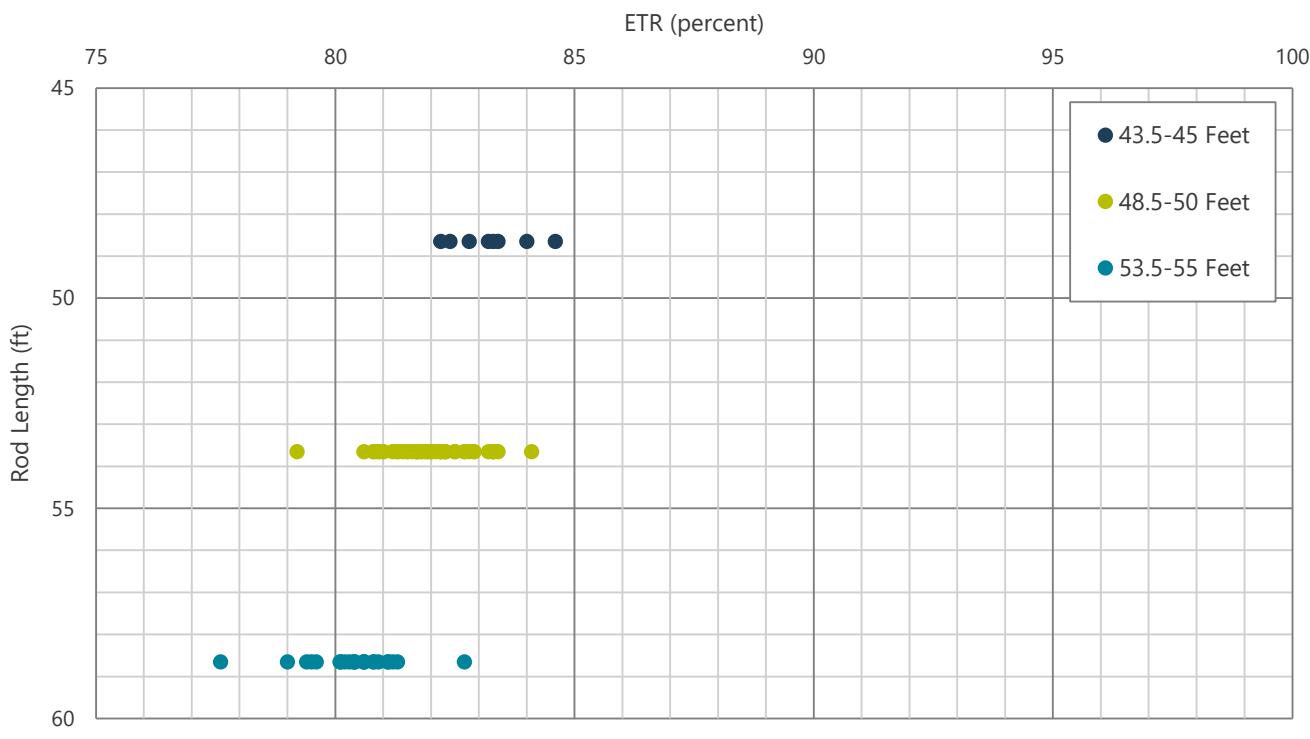
EFV: Maximum Energy

DMX: Maximum Displacement

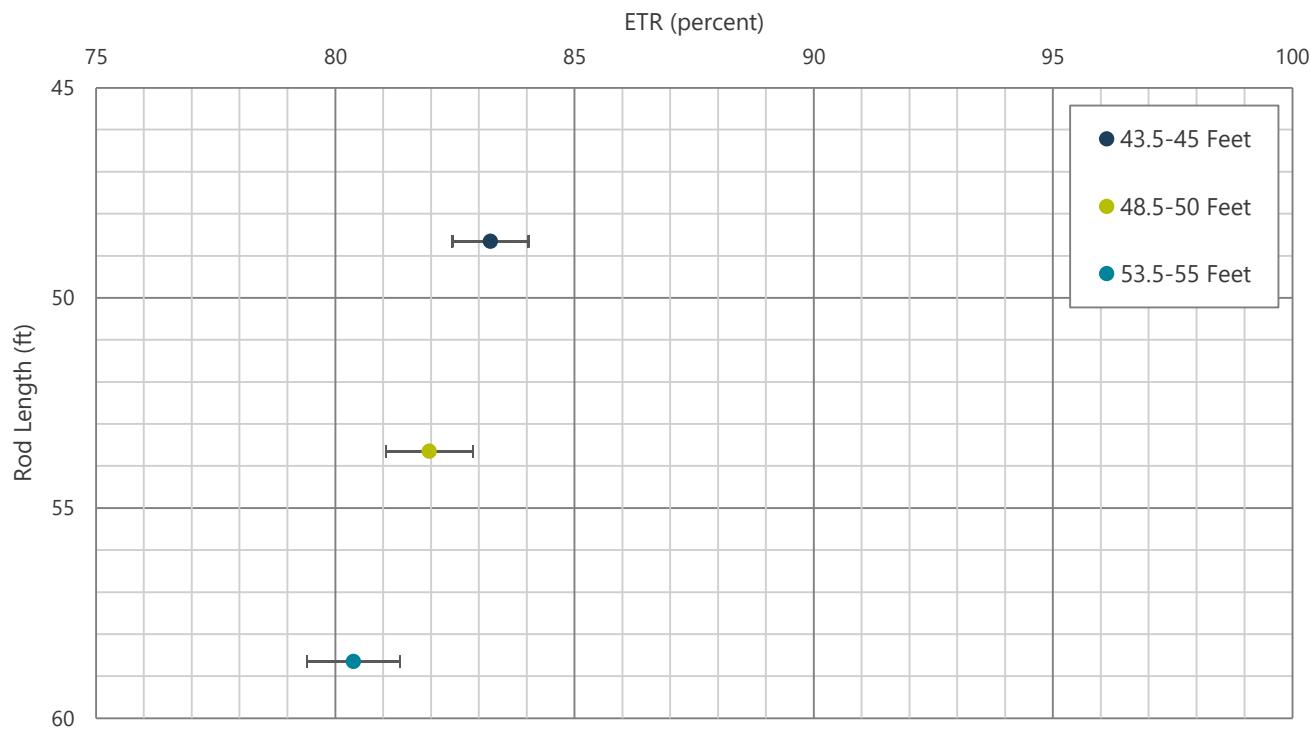
ETR: Energy Transfer Ratio - Rated

Instr. Length ft	Start Depth ft	Final Depth ft	Blows Applied /6"	N Value	N60 Value	Average BPM bpm	Average FMX kips	Average VMX ft/s	Average DMX in	Average CSX ksi	Average DFN in	Average Efv ft-lb	Average ETR %
48.65	43.50	45.00	3-4-4	8	10	53.4	29	18.1	1.58	24.0	1.50	291	83.2
53.65	48.50	50.00	8-19-27	46	62	53.2	27	18.6	0.44	22.3	0.26	287	82.0
58.65	53.50	55.00	6-11-12	23	31	53.3	27	17.5	0.58	22.7	0.52	281	80.4
Overall Average Values:				53.2	27	18.2	0.60	22.6	0.47	286	81.6		
Standard Deviation:				0.2	1	0.8	0.34	1.0	0.37	4	1.3		
Overall Maximum Value:				53.8	30	20.3	1.77	25.0	1.50	296	84.6		
Overall Minimum Value:				52.8	24	16.7	0.38	20.2	0.22	271	77.6		

ETR versus Rod Length CME-750X ATV (SN 322938)



Average ETR versus Rod Length \pm 1 Standard Deviation CME-750X ATV (SN 322938)





Memorandum

To: File – S&ME Project No.: 22350835A – TVA CRN Geotechnical Investigation, Oak Ridge, TN

From: Joseph R. Williamson, P.E. (NC & SC) and Jason S. Reeves, P.E. *Jason S. Reeves* 6/14/23

Cc: Julie P. Robertson, P.G. *Joseph Williamson* 6/14/23

Date: June 14, 2023

Subject: Summary of SPT Energy Measurements – S&ME Diedrich D-50 Track (Serial No. 316) – Tested 6/8/23

◆ Purpose

In accordance with the project specifications, we have completed the Standard Penetration Test (SPT) energy measurements on the automatic hammer used with our Diedrich D-50 track-mounted drill rig (Serial No. 316). This testing was performed prior to the beginning of our field exploration services for this project. This service was performed by Mr. Joseph Williamson, P.E. (NC and SC) of S&ME on June 8, 2023, in general accordance with ASTM D4633. Review of the data quality and analyses was performed by Mr. Williamson. A copy of the Certificate of Proficiency issued by Pile Dynamics based on the Dynamic Measurement and Analysis Proficiency Test for Mr. Williamson is included in the attachments. The testing procedures, equipment used during testing, and detailed results are presented in this memorandum.

◆ Dynamic Testing Methodology

Testing was performed using a model PAX (Serial No. 3733L) Pile Driving Analyzer™ (PDA) manufactured by Pile Dynamics, Inc. The PDA was used to record and interpret data from two piezoresistive accelerometers (Serial Nos. K4664 and K4665) bolted to a 2.0-foot long AWJ drill rod (Serial No. 203) internally instrumented with two strain transducers. Calibration sheets for the accelerometers and the instrumented rod are included in the attachments. The instrumented AWJ drill rod has a cross-sectional area of 1.21 square inches (verified during equipment calibration) and an outside diameter of approximately 1-7/8 inches. Therefore, we calculate the inside diameter to be approximately 1.23 inches at the gauge location. The accelerometers and strain gauges, which are diametrically opposed near the middle of the instrumented rod, monitor acceleration and strain for each hammer blow. The analyzer converts the data to velocities and forces and computes the maximum transferred hammer energies with the "EFV" method described in ASTM D4633. Preliminary results are recorded and displayed in real time for each blow.



◆ Testing and Observations

S&ME personnel were on site June 8, 2023, to observe and perform high-strain dynamic testing during SPT sampling on the Diedrich D-50 track-mounted drill rig operated by Frank Crane of S&ME. The measurements were taken during drilling and sampling of a test hole (Test Hole 2) at our office in Louisville, Tennessee. SPT energy measurements were recorded during four sample intervals that met the N-value requirements of ASTM D4633. The information presented in the tables below summarizes the equipment and tooling used during the SPT energy measurements. The SPT Energy Evaluation Form is included in the attachments.

Table 1: Drill Rig Information

Manufacturer	Diedrich
Model	D-50
Serial Number	316
Operator	F. Crane
Carrier	Track

Table 2: Hammer Information

Type / Model	Auto / Diedrich
Drop Height from Calibration Record (inches)	30.0
Calibration Hammer Weight (pounds)	139.66

Table 3: Drilling and Instrumented Rod Information

Drill Rod Type	AWJ
OD (inches) ¹	1.75
ID (inches) ¹	1.25
Cross-Sectional Area (in ²) ²	1.18
Typical Lengths (feet)	5
Instrumented Rod Type	AWJ (Serial No. 203)
OD (inches) ³	1-7/8
ID (inches) ⁴	1.23
Cross-Sectional Area (in ²) ⁵	1.21
Total Instrumented Rod Length (feet) ³	2.0
Length Below Gages (feet) ³	0.75
Split-Spoon Length (feet) ³	2.84

¹ Per manufacturer's specifications.

² Calculated using OD and ID from manufacturer's specifications.

³ Measured with engineer's tape measure at top of instrumented rod.

⁴ Calculated using typical drill rod OD and Area from instrument rod calibration record.

⁵ From instrument rod calibration record.



◆ Dynamic Testing Results

The total rod length from the instrumentation to the tip of the split-spoon sampler was determined by adding 3.59 ft to the drill rod length at each sample depth. The SPT Energy Measurement Data Summary tables in the attachments present the test data from every hammer blow at each sampling interval, along with representative force and velocity traces for each test interval. Per ASTM D4633, only the blows from the final foot of each sample interval (i.e. the blows that determine the N-value) are considered when computing the average measurement values of each test interval.

The reported blow counts obtained by the drill rig personnel, a summary of the test data, and average computed hammer energy and transfer ratio values are provided in Table 4. Based on the test data, the automatic hammer on the Diedrich D-50 operated at an average rate of about 51 blows per minute (bpm) during dynamic testing. The measured average transferred hammer energy (EFV) of the four sample intervals tested ranged from 335 to 344 ft-lbs, which corresponds to Energy Transfer Ratio (ETR) values of 95.7 to 98.2%, respectively, based on a typical theoretical maximum energy of 350 ft-lbs. Plots and tables of the following are also included in the Appendix and present the test data with depth for each test interval:

- Penetration vs. BLC⁶
- Penetration vs. FMX⁷
- Penetration vs. EFV⁸
- Penetration vs. CSX⁹
- Penetration vs. VMX¹⁰
- Penetration vs. ETR¹¹
- ETR vs. Rod Length
- Average ETR vs. Rod Length

Table 4: Summary of Dynamic Testing Results

Data Set ID	Sample Depth (ft)	Drill Rod Length (ft)	Instrumentation to Sampler Tip Length (ft)	Blows per 6" Increment / N-value	Soil Sample Description (Residual)	Avg. BPM	Avg. Efv (ft-lbs)	Avg. ETR (%)
1	31.0 – 32.5	32.0	35.59	5-14-19 / 33	Lean Clay	50.2	340	97.2
2	33.5 – 35.0	34.0	37.59	4-11-16 / 27	Lean Clay	50.4	336	96.1
3	36.0 – 37.5	36.0	39.59	7-12-19 / 31	Lean Clay	50.7	344	98.2
4	38.5 – 40.0	39.0	42.59	5-11-17 / 28	Lean Clay	50.7	335	95.7
Overall Average							50.5	339
Overall Average								96.8

The overall average transferred hammer energy for the automatic hammer on the Diedrich D-50 track-mounted drill rig was 339 foot-pounds, with an average ETR of 96.8%.

⁶ BLC - Blow Count per 6-in. increment

⁷ FMX - Maximum Compressive Force

⁸ EFV - Maximum Transferred Energy

⁹ CSX - Maximum Compressive Stress

¹⁰ VMX - Maximum Velocity

¹¹ ETR - Energy Transfer Ratio - Ratio of Calculated Energy to Theoretical Energy of 140 lb hammer falling 30 inches

Attachments

Certificate of Proficiency

Instrumented Rod and Accelerometer Calibration Sheets

SPT Energy Evaluation Form

Diedrich D-50 Track (SN 316) SPT Energy Measurements Summary Plots and Tables



This documents that

**Joseph Williamson
S&ME, Inc.**



has on March 16, 2022 achieved the rank of

MASTER

on the Dynamic Measurement and Analysis Proficiency Test.

The individual identified on this document demonstrated to the degree granted above an understanding of theory, data quality evaluation, interpretation and signal matching for high strain dynamic testing of deep foundations. ***It is recommended that individuals at the Master level seek to attain Expert level through additional study within eight years of the date of this document***

The ability of the individual named to provide appropriate knowledge and advice on a specific project is not implied or warranted by the Pile Driving Contractors Association or Pile Dynamics, Inc. The Pile Driving Contractors Association or Pile Dynamics, Inc. assumes no liability for foundation testing and analysis work performed by the bearer of this certificate. This certificate can be verified at www.PDAproficiencytest.com.

A handwritten signature in blue ink that reads "Frank T. Peters".

Frank T. Peters, Executive Director
Pile Driving Contractors Association



A handwritten signature in blue ink that reads "Garland Likins".

Garland Likins, Senior Partner
Pile Dynamics, Inc.

No. 3251

Certificate of Calibration

Pile Dynamics, Inc. certifies that the

Pile Driving Analyzer®, Model PAX

Serial Number: 3733L

was calibrated on 22 May 2023

using a PDA Calibration Box whose output was calibrated with test equipment
traceable to NIST.

This certificate is valid for 2 years from above date.



Tested by:



Pile Dynamics, Inc.
30725 Aurora Road
Cleveland, Ohio 44139 USA



Reviewed
6/5/2023
HJL

PDI Certificate of Calibration

PDI PDA Model PAX Serial # 3733L

Cal Date: May 19, 2023

Cal Due: May 18, 2025

Temperature: 74 deg. F

Humidity: 43%

Calibrated at:
Pile Dynamics, Inc.
30725 Aurora Road
Cleveland, OH 44139

Manufactured by Pile Dynamics, Inc.

Procedure used: PDA Calibration Procedure 2016-2, Revision 20160422

Actual Measurements: Attach PDA Calibration Data Sheet

Equipment was found to be:

in tolerance As Received _____ out of tolerance As Received

in tolerance As Returned _____ out of tolerance As Returned

Calibration Standards Utilized

PDA Cal Box serial 000002, verified on 21June2022.

Calibration performed by:

Marcus Johnson, Technician

Reviewed by:

Bob Sprenger, Product Support Manager

PDA CC-9 Issued 20160422



Quality Assurance for Deep Foundations

PDA Calibration Data Sheet Revision number 20160422
Use Calibration Procedure Number 2016-2, Revision 20160422

Reviewed
6/5/2023
MJD

PDI PDA Model PAX Serial # 3733L Cal Date: May 19, 2023

Reference Notes: Connect PDA Cal box to PDA sensor inputs. Set F3 & F4 to 147.5 and A3 & A4 to 1000. PDA to display the quantities FMX, VMX, and EMX. Select metric units. Set Area = 244 cm². Set EM = 2100 tonnes/cm². Set Frequency to 50000HZ. Record actual value displayed:

Channel 3 (F3 & V3)

Calculation	Expected	Acceptable Range	Measured	Acceptable	Not Acceptable
FMX	378 tonnes	370 to 386	376	X	_____
VMX (PR)	4.21 m/sec.	4.13 to 4.29	4.15	X	_____
EMX (PR)	7.94 tonnes m	7.62 to 8.26	7.83	X	_____

Channel 4 (F4 & V4)

Calculation	Expected	Acceptable Range	Measured	Acceptable	Not Acceptable
FMX	378 tonnes	370 to 386	374	X	_____
VMX (PR)	4.21 m/sec.	4.13 to 4.29	4.13	X	_____
EMX (PR)	7.94 tonnes m	7.62 to 8.26	7.75	X	_____

Calibration performed by:

MJ
Marcus Johnson, Technician

Reviewed by:

BS
Bob Sprenger, Product Support Manager

PDA DS-10 Issued 20160422



Reviewed
TND
6/5/2023
✓

PDI Certificate of Calibration

PDI SPT Drill Rod Serial # 203AWJ

Cal Date: May 23, 2023

Cal Due: May 22, 2025

Temperature: 74 deg. F

Humidity 42%

Manufactured by Pile Dynamics, Inc.

Calibrated at: Pile Dynamics, Inc., 30725 Aurora Road, Cleveland, OH 44139

Procedure used: SPT Drill Rod Calibration Procedure 2016-4, Revision 20160422

Calibration Data: Attach SPT Rod Data Sheet DS-17

Equipment was found to be

in tolerance As Received _____ out of tolerance As Received

in tolerance As Returned _____ out of tolerance As Returned

Calibration Standards Utilized

1. PDI SPT Calibration Signal Conditioning Unit #000001, verified on 20220909
2. PDI Load Cell #75, Certificate # 22005433-181-00675
3. Capacitec Displacement Sensor #2034, Certificate # 22005433-177-00618
4. Capacitec Displacement Sensor #2040, Certificate # 22005433-177-00618
5. Capacitec Displacement Mainframe #4004-671, Certificate # 22005433-177-00618
7. National Instruments USB-6210 DAQ serial number 159AFDE, Certificate # 22005433-177-00617

Calibration performed by:

A handwritten signature in blue ink that appears to read "Sean Bonner".

Sean Bonner, Technician

Reviewed by:

A handwritten signature in blue ink that appears to read "Robert Sprenger".

Robert Sprenger, Product Support Manager

SPT CC-16 Issued 20160425



Quality Assurance for Deep Foundations

SPT Calibration Data Sheet Revision number 20160426
Use Calibration Procedure Number 2016-6, Revision 20160422

SPT Drill Rod Data

Serial Number: 203AWJ Calibration Date: May 23, 2023

Temperature: 74 Deg F Humidity: 42%

Calibration performed in accordance with PDI SPT Calibration Procedure 2016-4, Revision 20160422

As Received (circle one): Operational - Malfunctioning - Damaged

Calibration data

Pre-Load: 1. 7226 lbs. 2. 7257 lbs. 3. 7245 lbs.

Total Load: 1. 18750 lbs. 2. 18900 lbs. 3. 18400 lbs.

Common typical theoretical EA values based on SPT Rod Type:

AW: 35400 NW: 43100 or 68100 N3: 70800 BW: 52344

EA Theoretical 35400 EA Measured 35236.75 Error 0.46%

Within 4% Tolerance: Y / N

Alternative EA verification: Measure wall thickness, calculate area and multiply by 30000.
(Use spreadsheet for calculation)

Calibration values

Channel 1: As Found: (last cal): 213.1 As Left: 210.82 Within 5% Tolerance: Y / N

Channel 2: As Found: (last cal): 212.91 As Left: 210.55 Within 5% Tolerance: Y / N

EA: As Found: (last cal): 35691.1 As Left: 36210.02 Difference: 1.45%

Calibration performed by:

Sean Bonner, Technician

Reviewed by:

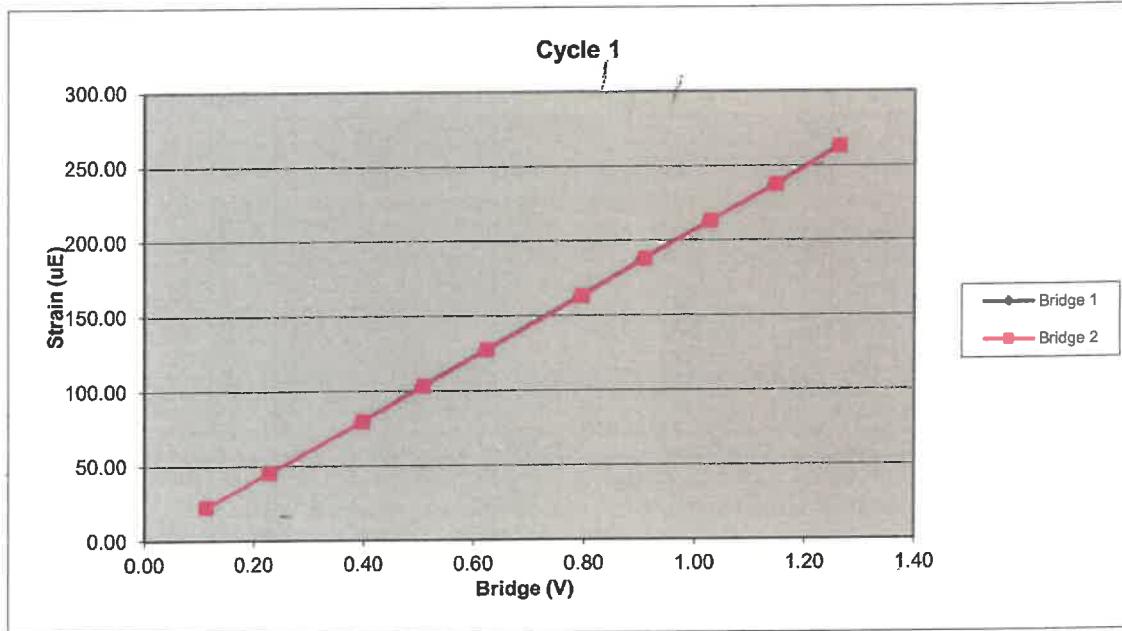
Robert Sprenger, Product Support Manager

SPT DS-17 Issued 20160426

203AWJ		Cycle 1		
Sample	Force (lb)	Strain (μE)	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	865.79	21.69	0.11	0.11
3	1747.56	44.88	0.23	0.23
4	3032.21	79.18	0.40	0.40
5	3859.50	102.90	0.51	0.51
6	4747.02	127.03	0.62	0.62
7	6064.42	163.03	0.79	0.80
8	6930.50	187.70	0.91	0.91
9	7843.76	212.75	1.03	1.03
10	8759.06	237.12	1.15	1.15
11	9650.58	262.68	1.26	1.26

Bridge 1	Bridge 2
Force Calibration (lb/V)	7640.67
Offset	3.38
Correlation	0.999999
Strain Calibration ($\mu\text{E}/\text{V}$)	209.98
Offset	-3.04
Correlation	0.999976
Force Calibration (lb/V)	7626.60
Offset	-0.21
Correlation	0.999997
Strain Calibration ($\mu\text{E}/\text{V}$)	209.60
Offset	-3.14
Correlation	0.999971

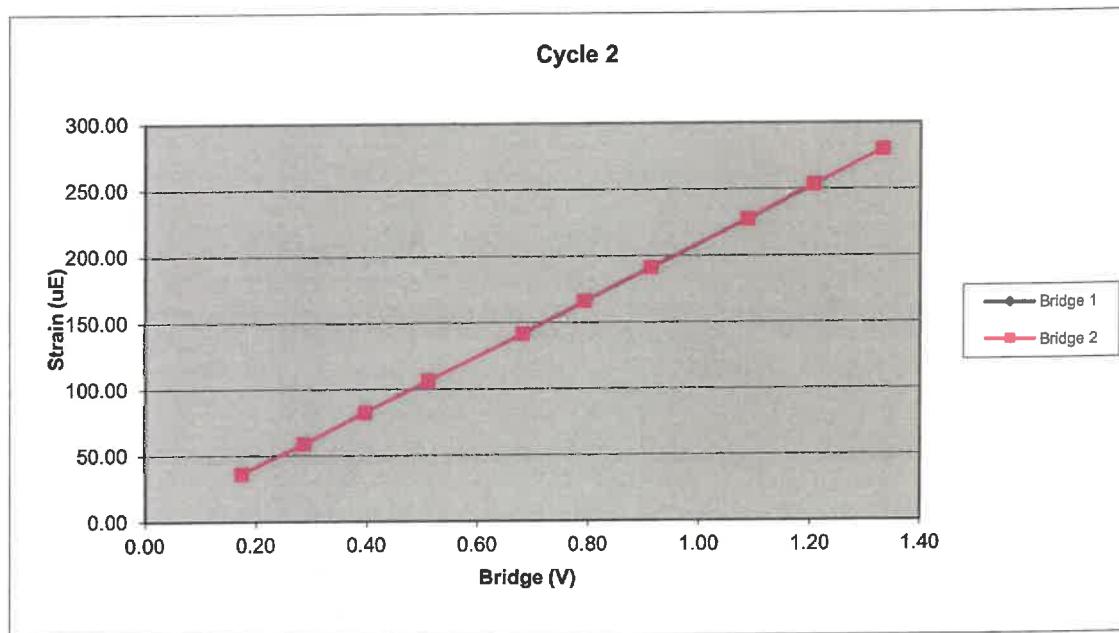
Force Strain Calibration	
EA (Kips)	36385.07
Offset	114.40
Correlation	0.999973



203AWJ		Cycle 2		
Sample	Force (lb)	Strain (μ E)	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	1314.77	35.40	0.17	0.17
3	2166.52	58.06	0.28	0.28
4	3009.50	81.68	0.40	0.39
5	3885.33	105.73	0.51	0.51
6	5194.73	140.93	0.68	0.68
7	6053.99	165.43	0.79	0.79
8	6954.28	190.27	0.91	0.91
9	8292.35	226.71	1.09	1.09
10	9204.43	252.85	1.21	1.21
11	10152.30	279.20	1.33	1.33

Bridge 1	Bridge 2
Force Calibration (lb/V)	7627.71
Offset	-7.28
Correlation	0.999999
Strain Calibration (μ E/V)	210.48
Offset	-1.73
Correlation	0.999979
Force Calibration (lb/V)	7632.02
Offset	-3.86
Correlation	0.999999
Strain Calibration (μ E/V)	210.60
Offset	-1.64
Correlation	0.999984

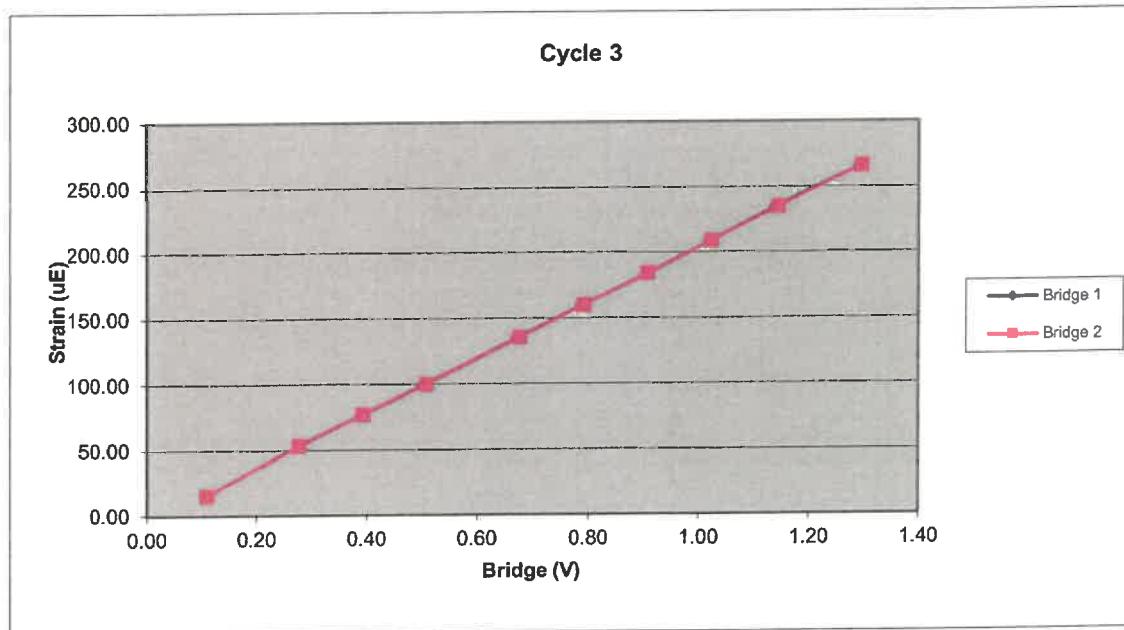
Force Strain Calibration
EA (Kips)
Offset
Correlation



203AWJ		Cycle 3		
Sample	Force (lb)	Strain (μE)	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	816.08	14.67	0.11	0.11
3	2104.72	52.88	0.28	0.28
4	2987.66	76.61	0.39	0.39
5	3851.02	99.83	0.50	0.51
6	5140.54	135.37	0.67	0.67
7	6035.47	159.90	0.79	0.79
8	6921.92	183.83	0.91	0.91
9	7791.12	208.45	1.02	1.02
10	8726.70	234.43	1.14	1.14
11	9881.90	265.78	1.30	1.30

Bridge 1	Bridge 2
Force Calibration (lb/V)	7634.36
Offset	-0.70
Correlation	0.999997
Strain Calibration ($\mu\text{E}/\text{V}$)	210.43
Offset	-6.40
Correlation	0.999951
Force Calibration (lb/V)	7626.44
Offset	-7.63
Correlation	0.999999
Strain Calibration ($\mu\text{E}/\text{V}$)	210.21
Offset	-6.59
Correlation	0.999954

Force Strain Calibration	
EA (Kips)	36276.49
Offset	231.85
Correlation	0.999963



Bridge Excitation (V) 5
Shunt Resistor (ohm) 60.4k

Calibration Factors	203AWJ		
Bridge 1 (μ E/V)	210.30	Bridge 2 (μ E/V)	210.14
EA Factor (Kips)	36299.67	Area (in ²)	1.21

Calibrated by: Sean Bonner
Calibrated Date: 5/23/2023

Pile Dynamics Inc
30725 Aurora Rd
Solon, OH 44139

Traceable to N.I.S.T.



Pile Dynamics, Inc.

PDI Certificate of Calibration

PDI Accelerometer Calibration

Model Kicher Serial # K4664

Reviewed
6/15/2021
JWL

Cal Date: 24May2023Cal Due: 23May2025Temperature: 73.4 deg. FHumidity 41%

Calibrated at
Pile Dynamics, Inc.
30725 Aurora Road
Cleveland, OH 44139

Manufactured by Pile Dynamics, Inc.

Procedure used: MAC Accelerometer Calibration Procedure 8G-4 Revision # 20210801

Equipment was found to be:

 in tolerance As Received _____ out of tolerance As Received in tolerance As Returned _____ out of tolerance As ReturnedPDI Calibration: 371.8 mv/5000g

Calibration Standards Utilized

MAC PDA 8G, serial number 5161 LE, verified on 22 December 2022

Calibration performed by:

William Johnson, Technician

Reviewed by:

Bob Sprenger, Product Support Manager

Accelerometer Calibration Certificate

Pile Dynamics, Inc.



Calibrated by Pile Dynamics, Inc.
Calibration performed on 24May2023

Serial No: K4664 Temperature: 73.4 °C

Model: PR Humidity: 41%

Calibrated on: Channel 3 on 8G 5161 LE

PDA CALIBRATION FACTOR

371.8 mv/5000g
(74.4 μ v/g)
 $R^2: 0.999908$ [Chip programmed]

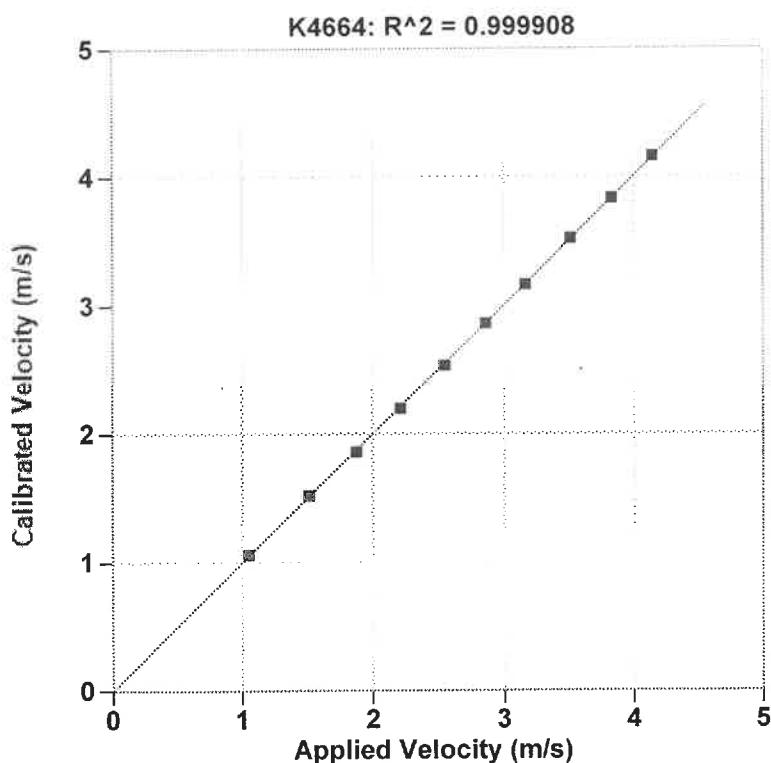
Operator: William Johnson

Ref Acc 1: 72517!
1049 g's/volt Cal on: 24Mar2022

Ref Acc 2: 72505!
1035 g's/volt Cal on: 24Mar2022

Signed

Reference accelerometer calibrations are traceable to
the United States National Institute of Standards and
Technology (NIST).



Reference Velocity	S/N K4664 Velocity
m/s	m/s
1.050	1.058
1.517	1.521
1.873	1.860
2.209	2.198
2.548	2.532
2.860	2.859
3.163	3.161
3.512	3.521
3.832	3.832
4.145	4.157

Maximum Acceleration: 913 g's



Quality Assurance for Deep Foundations

Pile Dynamics, Inc.

PDI Certificate of Calibration

PDI Accelerometer Calibration

Model Kicher Serial # K4665

Reviewed
JWL
6/5/2023

Cal Date: 24May2023

Cal Due: 23May2025

Temperature: 73.4 deg. F

Humidity 41%

Calibrated at
Pile Dynamics, Inc.
30725 Aurora Road
Cleveland, OH 44139

Manufactured by Pile Dynamics, Inc.

Procedure used: MAC Accelerometer Calibration Procedure 8G-4 Revision # 20210801

Equipment was found to be:

in tolerance As Received _____ out of tolerance As Received

in tolerance As Returned _____ out of tolerance As Returned

PDI Calibration: 371.2 mv/5000g

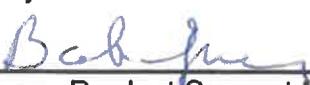
Calibration Standards Utilized

MAC PDA 8G, serial number 5161 LE, verified on 22 December 2022

Calibration performed by:


William Johnson, Technician

Reviewed by:


Bob Sprenger, Product Support Manager

Accelerometer Calibration Certificate

Pile Dynamics, Inc.



Calibrated by Pile Dynamics, Inc.
Calibration performed on 24May2023

Serial No: K4665 Temperature: 73.4 °C

Model: PR Humidity: 41%

Calibrated on: Channel 3 on 8G 5161 LE

PDA CALIBRATION FACTOR

371.2 mv/5000g
(74.2 μ v/g)
 $R^2: 0.999920$ [Chip programmed]

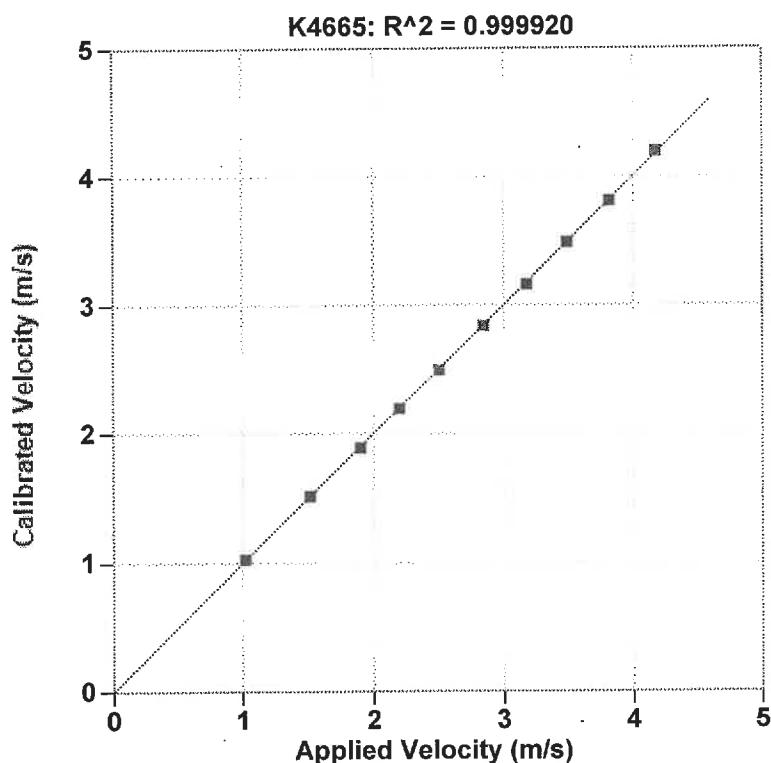
Operator: William Johnson


Signed

Ref Acc 1: 72517!
1049 g's/volt Cal on: 24Mar2022

Ref Acc 2: 72505!
1035 g's/volt Cal on: 24Mar2022

Reference accelerometer calibrations are traceable to
the United States National Institute of Standards and
Technology (NIST).



Reference Velocity m/s	S/N K4665 Velocity m/s
1.019	1.030
1.514	1.517
1.897	1.888
2.196	2.194
2.500	2.495
2.845	2.840
3.176	3.164
3.488	3.490
3.815	3.813
4.176	4.195

Maximum Acceleration: 918 g's

SPT Energy Evaluation Form

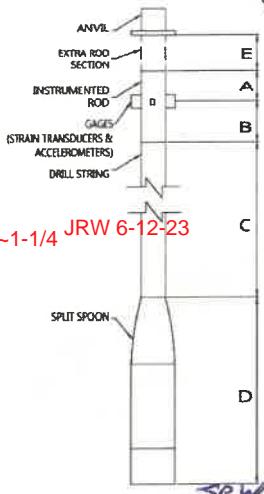
Document Control Number: CRN-23-0040-00



Project: TVA CRN GEOTECHNICAL INV. OAK RIDGE, TN Date (s): 6/8/23
 Project No.: 22350835A Weather: CLEAR 70°
 Boring No.: TEST HOLE 2 Drill Rod Type: 5' LONG AWS

On-site Personnel 6/8/23
 Drilling Company: F. SAW SE. ME
 Rig Oper./Helper: F. CRANE / A. BLANKENSHIP
 Engr/Geologist: J. BAINES
 PDA Operator: J. WILLIAMSON

Rod Info
 (E) Rod Length Above 0.40 ft
 Instr. Rod (if applicable): 2.0 ft
 (A) + (B) Instr. Rod Length: 0.40 ft
 (A + E) Impact to Gages 1.65 ft
 (B) Instr. Rod Below Gages 0.75 ft
 (D) Spoon Length: 2.84 ft
 Instr. Rod Inside Dia.: ~1 1/4 in. ~1-1/4 JRW 6-12-23
 Instr. Rod Outside Dia.: 1-7/8 in.
 Instr. Rod Area: 1.21 in²
 Instr. Rod S/N: 203 AWS
 PDA Make/Model: PDI/PAX
 PDA Serial No.: 3933L
 Calib. Pulse Test (y/n): Y



Rig/Hammer Info
 Drill Rig Make/Model: DIEDRICH D-50
 Carrier Type: TRAILER
 Rig Serial No.: 316
 Hammer Type/Model: AUTO / DIEDRICH
 Hammer Serial No.: 316 316 SW
 Hammer Drop System: CHAIN LIFT w/ FREE FALL
 Lubrication Condition: GREASED PER MAN. RECS.
 Manufacturer Recommended
 Operation Rate (bpm): 50-55
 Drop Height from calibration record (in.): 30.0 JRW 6/12/23
 Calibration hammer weight (kips): (lbs) 139.66 JRW 6/12/23
 Anvil Dimension (in.): (ft) 2.4 JRW 6/12/23
 Drilling Method: 3-1/4" HSA

Gage Information			FACTOR
	Gage	Serial No.	Calibration Date
Accel.	A3	K4664	371.8
	A4	K4665	371.2
Strain	F3	203 AWS-1	210.30
	F4	203 AWS-2	210.14

Date of Test	Test Depth Increment (ft)	Test Time Start / Stop (Military)	Length of Drill String (ft)	(LE) Length Below Gages (ft)	Avg. Meas. Rate (BPM)	SPT Blow Counts					Drop Height in Tolerance (y/n)
						6 in.	12 in.	18 in.	extra	N-value	
6/8/23	28.5-30.0	11:57	30	37.59	~50	11	17	21	1	38	Y
	31.0-32.50	12:09	32 SW	35.59	~50	5	14	19	0	33	Y
	33.50-35.00	12:09 6/8/23	35 34	36.59							
	33.50-35.00	13:12		37.59	~50	4	11	16	0	27	Y
	36.00-37.50	13:22	36 SW	39.59	~50	7	12	19	0	31	Y
	38.5-40.0	13:37	38 39	42.59	~51	5	11	17	0	28	Y

Comments: (1) If there are any nonconformances or deficiencies identified during the testing, immediately pause the drilling and testing activities and notify the Site Manager and describe them in the space below; (2) Note any unusual hammer operating conditions that affect the hammer performance, or changes in operating conditions (e.g. verticality, weather, or lubrication between trials); (3) Note any changes in rod diameter along drill string and record locations of short rod sections; (4) Prepare a sketch or take a picture of the instrumented drill rod assembly and indicate the relative location and orientation of the strain gauges, accelerometers, and LE Datum; (5) Note: Identify all attached pages, including photographs, with the Project No., Boring No., and date.

28.5-30.0 FT SAMPLE - FIRST SEVERAL BLOWS HAD LOW ENERGY (50-60%) REMAINING BLOWS OF ALL OTHER DATA HAD ENERGY ENERGY VALUES RANKING FROM APPROX. 85-95% DRILLER STATED THIS IS LIKELY DUE TO HYDRAULIC FLUID IN HAMMER WARMING UP, REG ALSO ALSO HAD RECENT MAINTENANCE, SYSTEM COULD HAVE HAD AIR

BUBBLES THAT WORKED ITSELF OUT. EACH SAMPLE CLASSIFIED AS A LEAN CLAY (CL).

Note: Measurements shall be made to nearest 0.01 ft or 1/8 in. as applicable.

Joseph Williamson

Prepared By (print/signature)
SPT Energy Lead

6/13/23

Date

Reviewed By (print/signature)

Site Manager

06/14/2023

Date

JRW
6/9/23
See note
below.



Printed: 13-June-2023

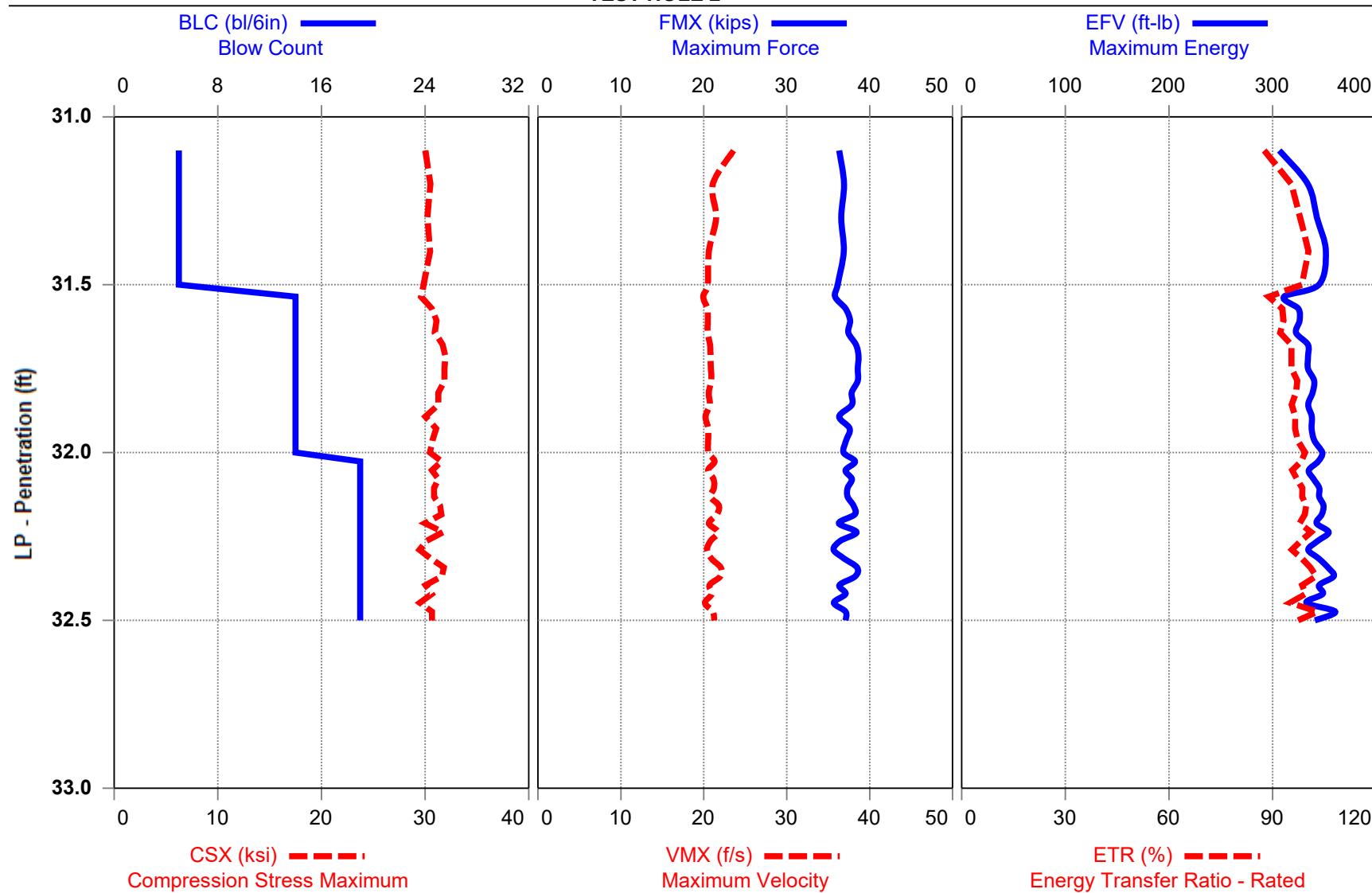
S&ME, Inc. - PDIPILOT2 Ver 2022.1.62.0 - Case Method & iCAP® Results

Test started: 08-June-2023



DIEDRICH D-50 (SN 316) - 31.0-32.5 FEET

TEST HOLE 2



DIEDRICH D-50 (SN 316)

JRW

TEST HOLE 2

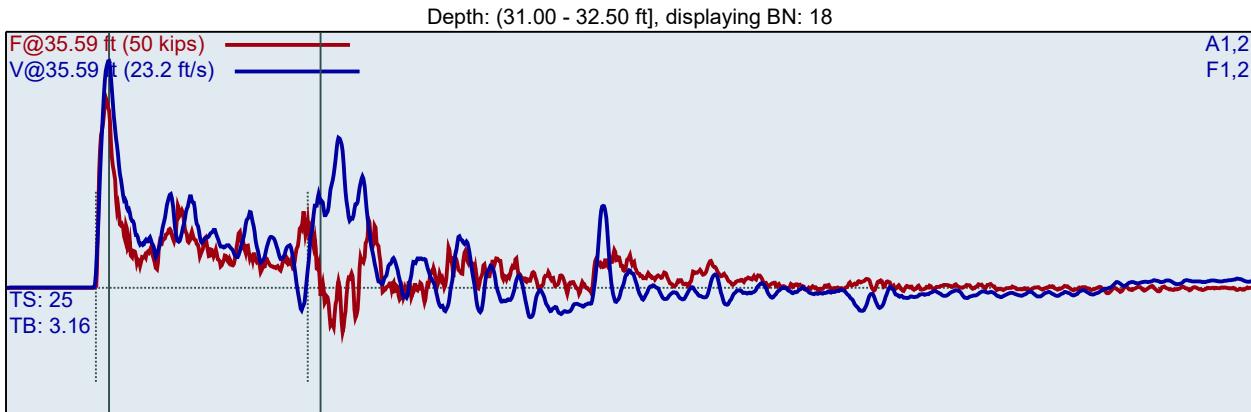
AR: 1.21 in²

LE: 35.59 ft

WS: 16807.9 ft/s

SN 316 SPT Energy Measurements
Interval start: 6/8/2023

SP: 0.492 k/ft³
EM: 30000 ksi



F1 : [203 AWJ-1] 210.3 PDICAL (1) FF1
F2 : [203 AWJ-2] 210.14 PDICAL (1) FF1

A1 (PR): [K4664] 371.8 mv/6.4v/5000g (1) VF1
A2 (PR): [K4665] 371.2 mv/6.4v/5000g (1) VF1

BPM: Blows/Minute

CSX: Compression Stress Maximum

FMX: Maximum Force

DFN: Final Displacement

VMX: Maximum Velocity

EFV: Maximum Energy

DMX: Maximum Displacement

ETR: Energy Transfer Ratio - Rated

BL#	BC /6"	LP ft	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
1	5	31.10	1.9	36	23.6	1.88	30.0	1.22	306	87.5
2	5	31.20	49.3	37	21.1	1.24	30.5	1.20	334	95.4
3	5	31.30	49.9	37	21.5	1.22	30.2	1.20	343	97.9
4	5	31.40	50.8	37	20.6	1.20	30.5	1.19	351	100.4
5	5	31.50	51.0	36	20.5	1.20	29.9	1.20	345	98.4
6	14	31.54	50.2	36	19.9	0.63	29.6	0.42	311	88.8
7	14	31.57	50.4	37	20.5	0.57	30.7	0.43	325	92.8
8	14	31.61	50.5	38	20.5	0.53	31.1	0.43	326	93.1
9	14	31.64	50.3	37	20.5	0.50	30.9	0.43	323	92.2
10	14	31.68	50.0	38	20.7	0.51	31.7	0.43	334	95.4
11	14	31.71	50.4	39	20.8	0.47	32.0	0.41	334	95.4
12	14	31.75	50.3	39	20.9	0.44	31.9	0.43	334	95.4
13	14	31.79	50.1	39	20.9	0.46	31.9	0.43	340	97.1
14	14	31.82	50.0	38	20.6	0.46	31.3	0.39	339	96.7
15	14	31.86	50.8	38	20.7	0.45	31.3	0.44	334	95.5
16	14	31.89	50.3	36	20.2	0.46	30.0	0.39	338	96.5
17	14	31.93	51.0	38	20.5	0.44	31.1	0.43	338	96.4
18	14	31.96	49.6	37	20.5	0.44	30.7	0.42	340	97.2
19	14	32.00	50.5	37	20.6	0.46	30.5	0.43	348	99.3
20	19	32.03	50.1	38	21.3	0.41	31.6	0.32	344	98.2
21	19	32.05	50.8	37	20.5	0.41	30.7	0.32	335	95.6
22	19	32.08	49.8	38	21.2	0.42	31.3	0.31	339	97.0
23	19	32.11	50.9	37	21.2	0.42	30.9	0.32	345	98.6
24	19	32.13	49.2	37	20.8	0.44	30.9	0.31	345	98.5
25	19	32.16	50.2	38	21.8	0.40	31.4	0.32	349	99.7
26	19	32.18	50.2	38	21.6	0.40	31.6	0.32	347	99.3
27	19	32.21	50.3	36	20.6	0.41	30.0	0.31	342	97.8

28	19	32.24	49.5	38	21.7	0.40	31.7	0.32	354	101.1
29	19	32.26	50.3	36	20.8	0.41	30.1	0.31	344	98.1
30	19	32.29	50.5	36	20.4	0.39	29.5	0.31	334	95.5
31	19	32.32	49.6	37	20.9	0.40	30.5	0.32	345	98.5
32	19	32.34	50.7	38	22.0	0.40	31.8	0.32	353	100.9
33	19	32.37	49.9	38	22.0	0.40	31.6	0.32	359	102.5
34	19	32.39	50.3	36	20.7	0.39	30.0	0.31	345	98.5
35	19	32.42	50.0	37	21.0	0.38	30.7	0.32	348	99.5
36	19	32.45	50.6	36	20.1	0.37	29.5	0.32	333	95.0
37	19	32.47	49.8	37	21.1	0.40	30.7	0.32	360	102.9
38	19	32.50	49.8	37	21.3	0.36	30.7	0.32	341	97.3
Average		50.2		37	20.9	0.44	30.9	0.36	340	97.2
Std Dev		0.4		1	0.5	0.06	0.7	0.05	10	2.9
Maximum		51.0		39	22.0	0.63	32.0	0.44	360	102.9
Minimum		49.2		36	19.9	0.36	29.5	0.31	311	88.8
N-value: 33										

Sample Interval Time: 44.14 seconds.



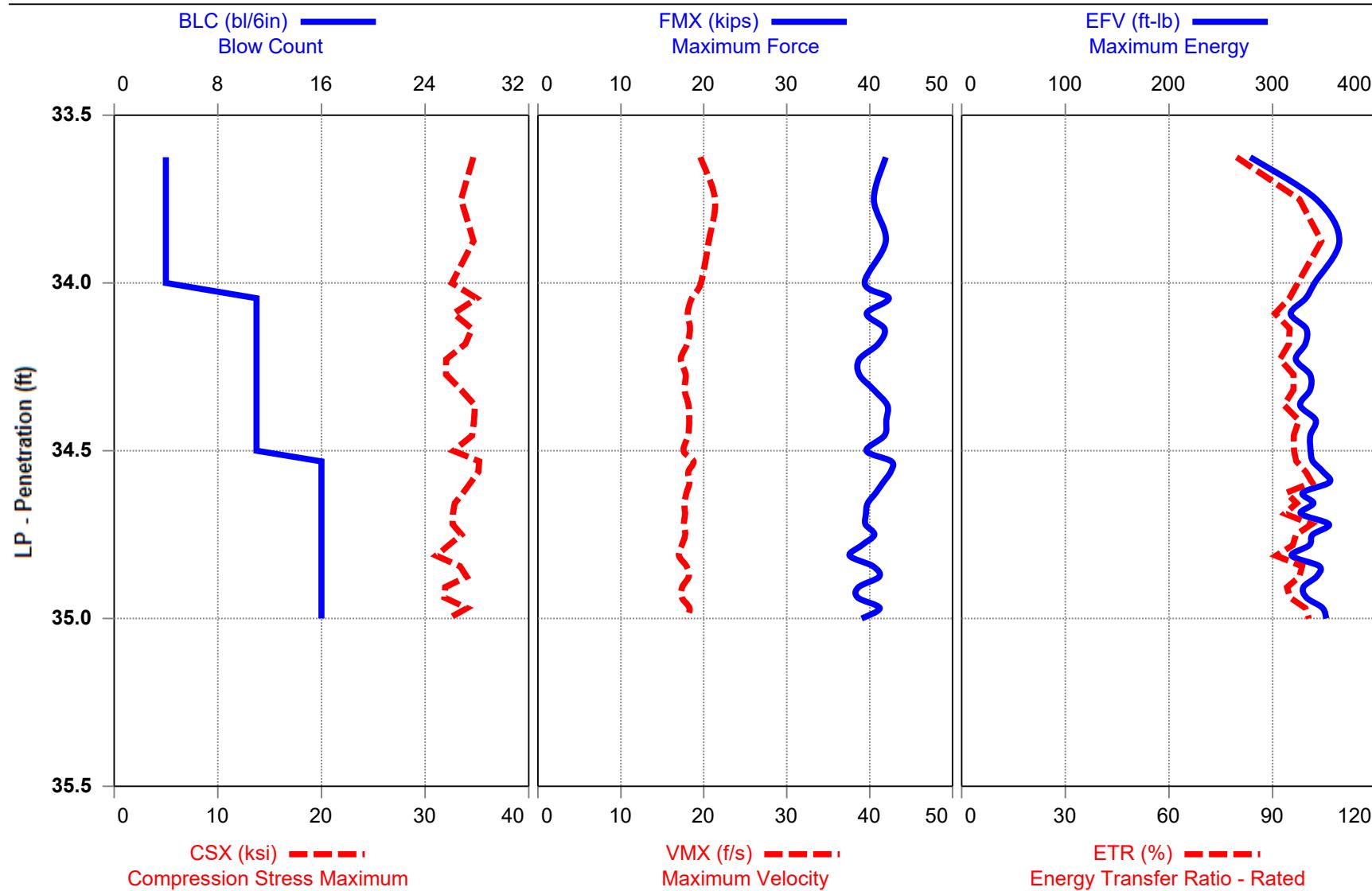
Printed: 13-June-2023

S&ME, Inc. - PDIPILOT2 Ver 2022.1.62.0 - Case Method & iCAP® Results

Test started: 08-June-2023



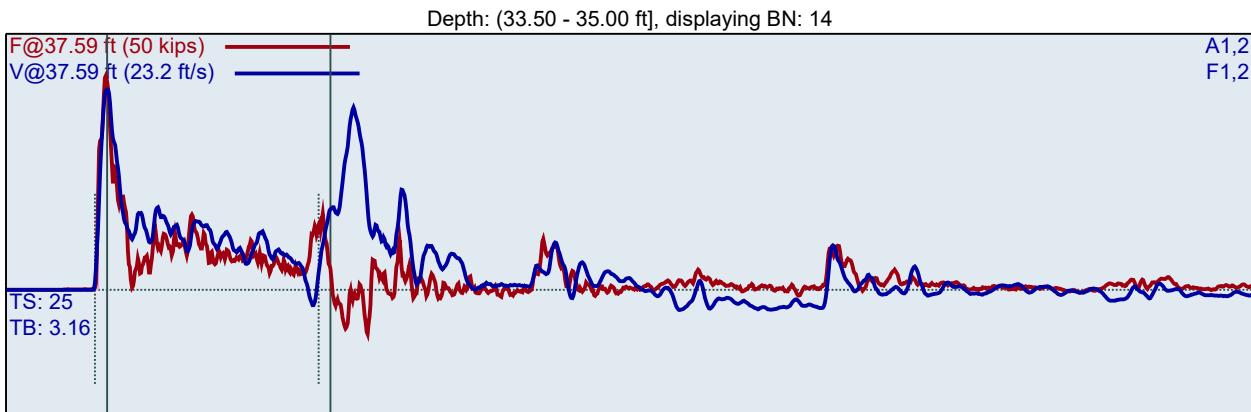
DIEDRICH D-50 (SN 316) - 33.5-35.0 FEET
TEST HOLE 2



DIEDRICH D-50 (SN 316)
JRW
TEST HOLE 2
AR: 1.21 in²
LE: 37.59 ft
WS: 16807.9 ft/s

SN 316 SPT Energy Measurements
Interval start: 6/8/2023

SP: 0.492 k/ft³
EM: 30000 ksi



F1 : [203 AWJ-1] 210.3 PDICAL (1) FF1
F2 : [203 AWJ-2] 210.14 PDICAL (1) FF1

A1 (PR): [K4664] 371.8 mv/6.4v/5000g (1) VF1
A2 (PR): [K4665] 371.2 mv/6.4v/5000g (1) VF1

BL#	BC /6"	LP ft	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
1	4	33.63	1.9	42	19.6	1.65	34.7	1.48	278	79.5
2	4	33.75	50.3	40	21.4	1.50	33.5	1.50	342	97.7
3	4	33.88	51.2	42	20.6	1.50	34.7	1.50	364	104.1
4	4	34.00	50.7	39	19.7	1.50	32.6	1.50	340	97.2
5	11	34.05	50.4	42	18.5	0.64	35.0	0.55	332	94.8
6	11	34.09	50.7	40	18.1	0.64	32.8	0.55	317	90.7
7	11	34.14	50.4	42	18.3	0.63	34.5	0.54	332	94.9
8	11	34.18	50.4	41	18.0	0.63	33.9	0.54	331	94.7
9	11	34.23	51.3	39	17.2	0.64	32.0	0.55	322	92.1
10	11	34.27	49.7	39	17.8	0.61	32.0	0.55	336	96.0
11	11	34.32	50.8	41	17.7	0.58	33.5	0.54	336	96.0
12	11	34.36	50.9	42	18.2	0.56	34.8	0.54	326	93.2
13	11	34.41	50.0	42	18.2	0.57	34.7	0.54	341	97.6
14	11	34.45	50.6	42	18.1	0.55	34.5	0.54	336	96.1
15	11	34.50	51.2	40	17.6	0.62	32.7	0.55	337	96.2
16	16	34.53	49.6	43	18.8	0.52	35.2	0.37	339	96.8
17	16	34.56	50.4	43	18.1	0.54	35.1	0.37	349	99.6
18	16	34.59	50.3	42	18.3	0.53	34.4	0.37	355	101.4
19	16	34.63	50.7	41	17.9	0.45	33.7	0.38	329	94.0
20	16	34.66	50.7	40	17.7	0.49	32.9	0.37	339	96.9
21	16	34.69	50.0	40	17.7	0.45	32.7	0.37	327	93.5
22	16	34.72	50.3	40	17.6	0.49	32.7	0.38	354	101.2
23	16	34.75	50.4	41	17.8	0.48	33.5	0.37	339	96.7
24	16	34.78	50.6	39	17.4	0.48	32.3	0.37	335	95.8
25	16	34.81	51.1	38	17.0	0.46	31.1	0.37	318	91.0
26	16	34.84	50.0	40	17.9	0.49	33.4	0.37	345	98.5
27	16	34.88	50.8	41	18.2	0.47	34.0	0.37	342	97.7
28	16	34.91	50.3	39	17.4	0.43	31.9	0.37	330	94.2
29	16	34.94	49.7	39	17.4	0.42	31.9	0.37	333	95.0
30	16	34.97	50.7	41	18.3	0.44	34.1	0.37	348	99.5
31	16	35.00	50.1	39	18.0	0.44	32.3	0.37	352	100.5

S&ME, Inc.
SPT Analyzer Results

Page 4 of 9
PDA-S Ver. 2022.35.2 - Printed: 6/13/2023

Average	50.4	40	17.9	0.53	33.4	0.44	336	96.1
Std Dev	0.4	1	0.4	0.07	1.2	0.08	10	2.8
Maximum	51.3	43	18.8	0.64	35.2	0.55	355	101.4
Minimum	49.6	38	17.0	0.42	31.1	0.37	317	90.7

N-value: 27

Sample Interval Time: 35.60 seconds.



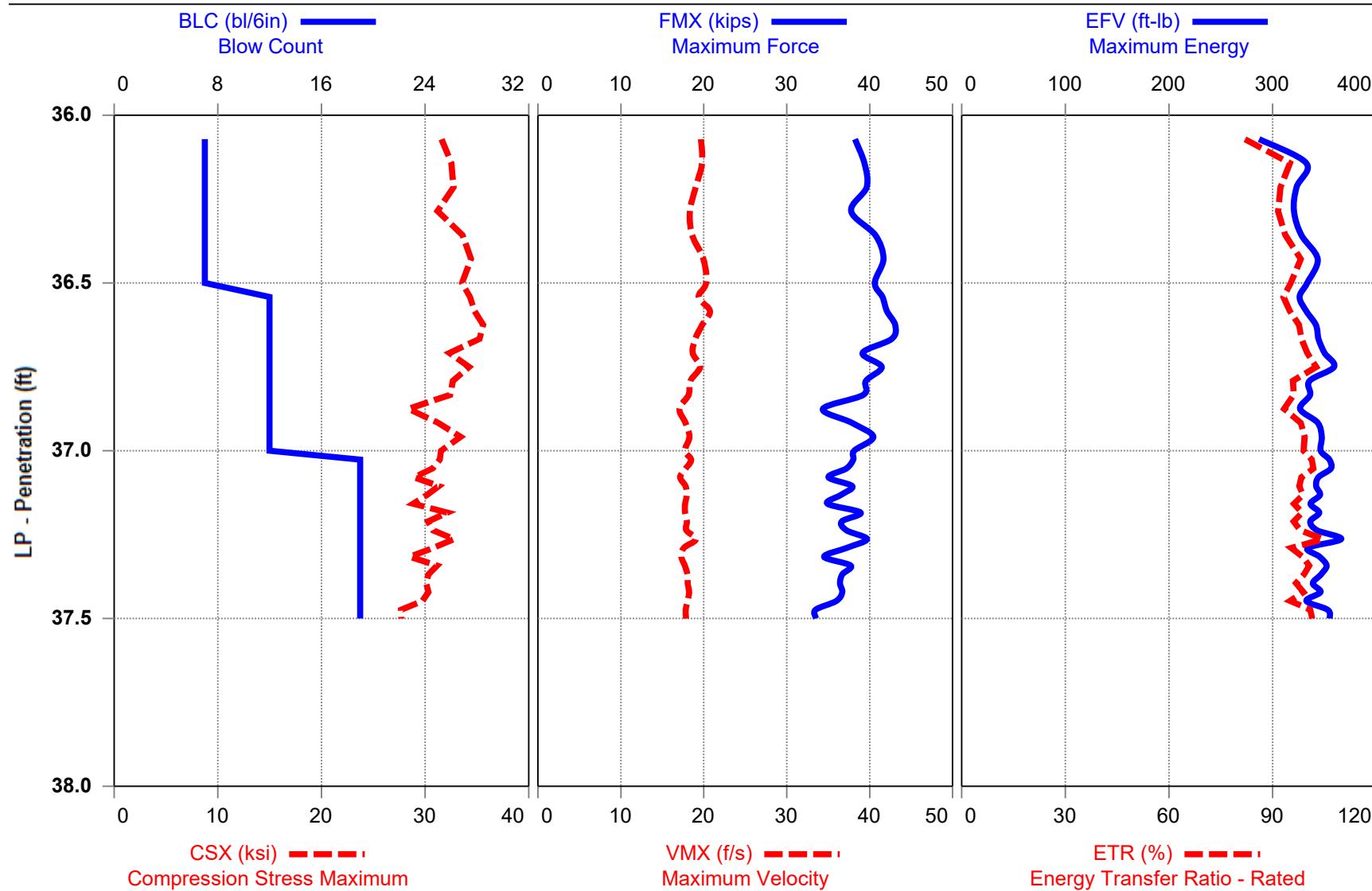
Printed: 13-June-2023

S&ME, Inc. - PDIPILOT2 Ver 2022.1.62.0 - Case Method & iCAP® Results

Test started: 08-June-2023



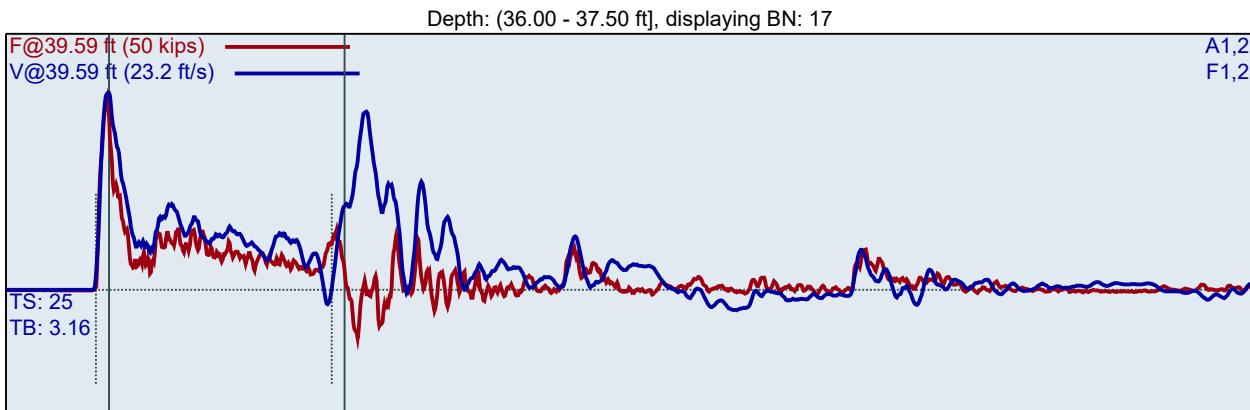
DIEDRICH D-50 (SN 316) - 36.0-37.5 FEET
TEST HOLE 2



DIEDRICH D-50 (SN 316)
JRW
TEST HOLE 2
AR: 1.21 in²
LE: 39.59 ft
WS: 16807.9 ft/s

SN 316 SPT Energy Measurements
Interval start: 6/8/2023

SP: 0.492 k/ft³
EM: 30000 ksi



F1 : [203 AWJ-1] 210.3 PDICAL (1) FF1
F2 : [203 AWJ-2] 210.14 PDICAL (1) FF1

A1 (PR): [K4664] 371.8 mv/6.4v/5000g (1) VF1
A2 (PR): [K4665] 371.2 mv/6.4v/5000g (1) VF1

BL#	BC /6"	LP ft	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
1	7	36.07	1.9	38	19.7	1.10	31.6	0.86	287	82.0
2	7	36.14	50.6	39	19.8	0.97	32.5	0.86	332	95.0
3	7	36.21	51.8	40	19.0	0.88	32.8	0.86	323	92.3
4	7	36.29	49.9	38	18.3	0.87	31.2	0.86	320	91.6
5	7	36.36	50.7	41	18.6	0.86	33.6	0.86	328	93.6
6	7	36.43	50.5	42	20.0	0.86	34.4	0.86	343	98.1
7	7	36.50	50.9	41	20.3	0.86	33.6	0.86	333	95.2
8	12	36.54	50.9	42	19.4	0.63	34.3	0.50	326	93.1
9	12	36.58	50.3	42	20.7	0.71	34.8	0.50	332	94.9
10	12	36.63	50.6	43	19.8	0.74	35.6	0.50	342	97.6
11	12	36.67	50.8	43	19.0	0.72	35.3	0.50	344	98.3
12	12	36.71	50.8	39	18.7	0.70	32.4	0.50	350	100.0
13	12	36.75	49.7	41	19.5	0.68	34.3	0.50	359	102.6
14	12	36.79	51.4	40	18.4	0.65	32.7	0.50	335	95.8
15	12	36.83	51.1	39	18.2	0.68	32.4	0.50	336	96.0
16	12	36.88	50.2	34	17.1	0.58	28.4	0.50	326	93.3
17	12	36.92	50.5	38	17.8	0.64	31.3	0.50	343	98.1
18	12	36.96	50.7	40	18.3	0.57	33.4	0.50	347	99.2
19	12	37.00	51.0	38	17.7	0.62	31.5	0.50	346	98.9
20	19	37.03	50.1	38	18.5	0.55	31.4	0.32	355	101.3
21	19	37.05	51.0	37	17.8	0.54	30.7	0.32	356	101.8
22	19	37.08	51.6	35	17.1	0.58	28.9	0.32	344	98.3
23	19	37.11	50.1	38	17.8	0.51	31.3	0.32	342	97.7
24	19	37.13	50.6	37	18.0	0.53	30.2	0.32	346	98.7
25	19	37.16	50.7	35	17.7	0.49	28.9	0.32	336	96.1
26	19	37.18	50.7	39	17.7	0.48	32.2	0.32	345	98.5
27	19	37.21	51.1	37	18.0	0.45	30.3	0.32	336	96.0
28	19	37.24	50.5	37	17.9	0.46	30.8	0.32	343	98.0
29	19	37.26	49.9	40	19.1	0.50	32.8	0.32	366	104.6
30	19	37.29	51.7	37	17.6	0.44	30.8	0.32	334	95.4
31	19	37.32	50.2	35	17.3	0.46	28.5	0.32	345	98.7

S&ME, Inc.
SPT Analyzer Results

Page 6 of 9
PDA-S Ver. 2022.35.2 - Printed: 6/13/2023

32	19	37.34	50.1	38	17.7	0.47	31.2	0.32	352	100.5
33	19	37.37	51.1	37	18.0	0.44	30.3	0.32	347	99.0
34	19	37.39	50.1	36	18.1	0.38	30.1	0.31	339	96.7
35	19	37.42	51.0	37	18.2	0.45	30.3	0.32	346	98.9
36	19	37.45	50.3	36	18.1	0.38	29.7	0.31	333	95.0
37	19	37.47	50.8	33	17.8	0.54	27.7	0.32	353	100.9
38	19	37.50	51.2	34	17.9	0.53	27.7	0.32	355	101.4
Average		50.7	38	18.2	0.55	31.3	0.39	344	98.2	
Std Dev		0.5	3	0.8	0.10	2.1	0.09	9	2.6	
Maximum		51.7	43	20.7	0.74	35.6	0.50	366	104.6	
Minimum		49.7	33	17.1	0.38	27.7	0.31	326	93.1	
N-value: 31										

Sample Interval Time: 43.73 seconds.



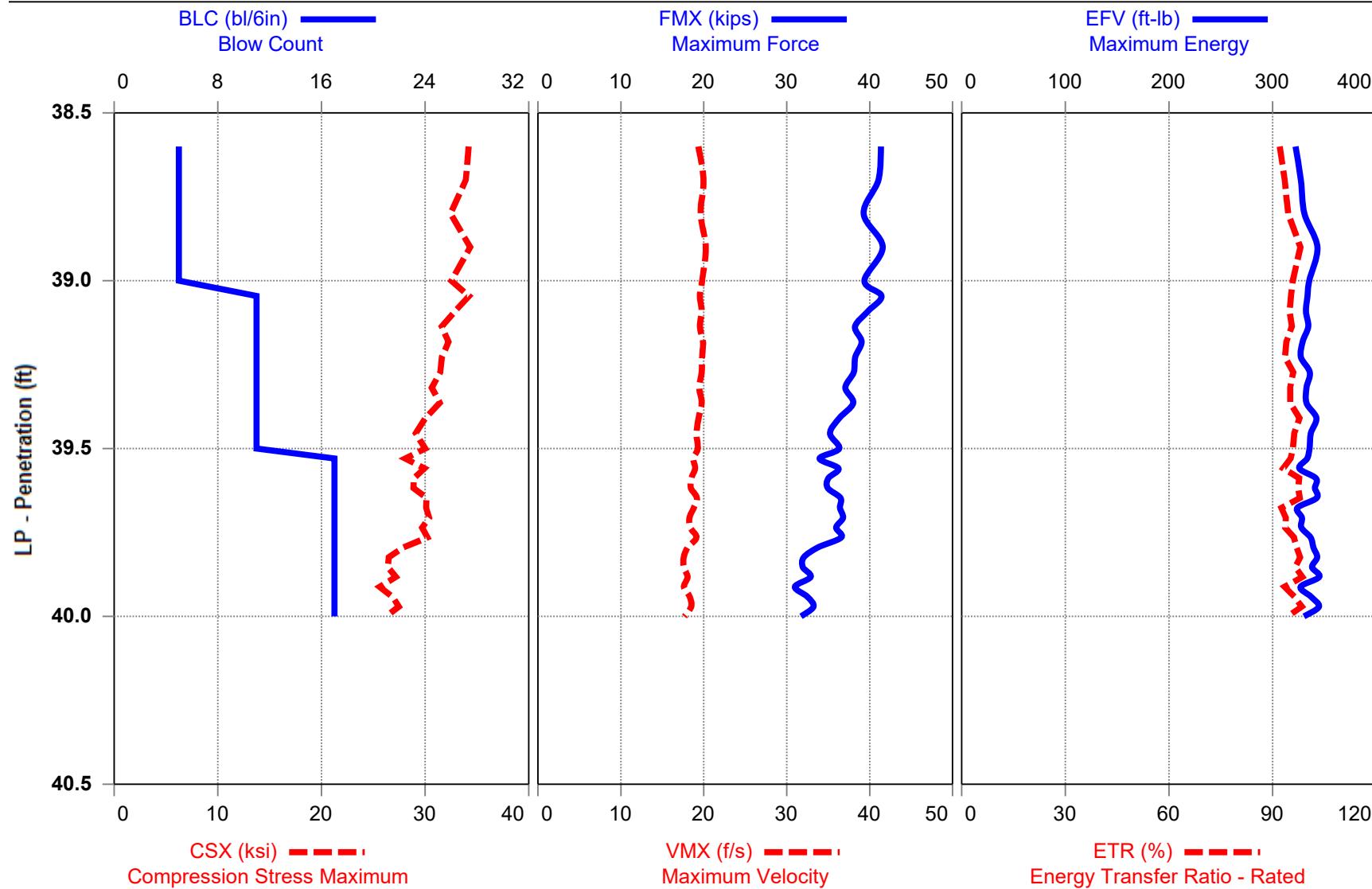
Printed: 13-June-2023

S&ME, Inc. - PDIPILOT2 Ver 2022.1.62.0 - Case Method & iCAP® Results

Test started: 08-June-2023



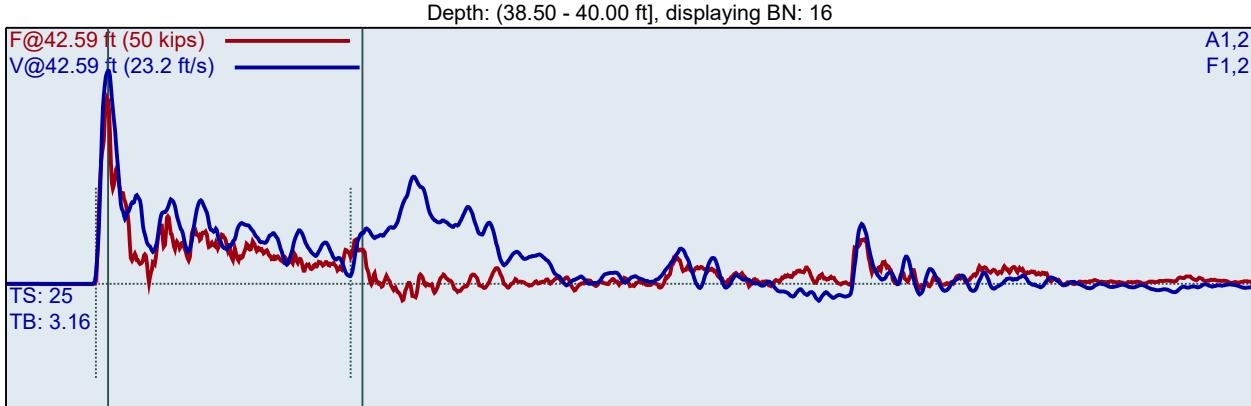
DIEDRICH D-50 (SN316) - 38.5-40.0 FEET
TEST HOLE 2



DIEDRICH D-50 (SN 316)
JRW
TEST HOLE 2
AR: 1.21 in²
LE: 42.59 ft
WS: 16807.9 ft/s

SN 316 SPT Energy Measurements
Interval start: 6/8/2023

SP: 0.492 k/ft³
EM: 30000 ksi



F1 : [203 AWJ-1] 210.3 PDICAL (1) FF1
F2 : [203 AWJ-2] 210.14 PDICAL (1) FF1

A1 (PR): [K4664] 371.8 mv/6.4v/5000g (1) VF1
A2 (PR): [K4665] 371.2 mv/6.4v/5000g (1) VF1

BL#	BC /6"	LP ft	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
1	5	38.60	1.9	41	19.4	1.43	34.2	1.20	322	92.0
2	5	38.70	50.6	41	20.0	1.50	33.9	1.20	327	93.5
3	5	38.80	50.4	39	19.6	1.36	32.5	1.20	331	94.5
4	5	38.90	50.4	42	20.2	1.20	34.4	1.20	343	98.0
5	5	39.00	51.7	39	19.8	1.20	32.5	1.20	335	95.8
6	11	39.05	49.9	41	19.5	0.72	34.2	0.53	334	95.3
7	11	39.09	50.6	40	19.8	0.67	32.9	0.54	332	94.9
8	11	39.14	51.3	38	19.5	0.67	31.6	0.55	334	95.5
9	11	39.18	50.8	39	19.9	0.65	32.3	0.55	329	93.9
10	11	39.23	50.6	38	19.8	0.62	31.6	0.54	327	93.5
11	11	39.27	50.7	38	19.7	0.64	31.5	0.55	336	95.9
12	11	39.32	51.4	37	19.5	0.63	30.6	0.54	333	95.0
13	11	39.36	50.5	38	19.7	0.65	31.4	0.54	333	95.0
14	11	39.41	50.5	36	19.4	0.64	30.0	0.55	342	97.7
15	11	39.45	51.0	35	19.1	0.60	29.1	0.53	337	96.2
16	11	39.50	51.0	36	19.3	0.61	30.0	0.55	335	95.8
17	17	39.53	50.7	34	18.7	0.61	28.1	0.36	333	95.2
18	17	39.56	50.8	36	19.0	0.55	29.9	0.35	326	93.0
19	17	39.59	50.8	35	18.5	0.58	28.9	0.38	342	97.6
20	17	39.62	50.3	35	18.5	0.57	28.9	0.34	341	97.4
21	17	39.65	50.7	36	19.2	0.54	30.1	0.36	342	97.8
22	17	39.68	50.8	36	18.8	0.48	30.1	0.36	324	92.5
23	17	39.71	50.6	37	18.3	0.50	30.4	0.35	328	93.8
24	17	39.74	50.4	36	18.4	0.49	29.7	0.36	328	93.6
25	17	39.76	50.0	37	19.1	0.50	30.2	0.35	337	96.2
26	17	39.79	50.8	34	18.1	0.51	27.9	0.36	339	96.9
27	17	39.82	50.8	32	17.6	0.55	26.5	0.35	343	98.0
28	17	39.85	50.5	32	17.6	0.52	26.4	0.35	338	96.5
29	17	39.88	49.8	33	18.0	0.53	27.2	0.35	345	98.6
30	17	39.91	51.1	31	17.6	0.49	25.6	0.35	327	93.4
31	17	39.94	50.5	33	18.3	0.50	26.9	0.36	337	96.3

S&ME, Inc.
SPT Analyzer Results

Page 8 of 9
PDA-S Ver. 2022.35.2 - Printed: 6/13/2023

32	17	39.97	50.3	33	18.5	0.51	27.5	0.35	345	98.4
33	17	40.00	51.3	32	17.7	0.52	26.2	0.35	330	94.3
	Average	50.7	36	18.8	0.57	29.5	0.43	335	95.7	
	Std Dev	0.4	3	0.7	0.07	2.1	0.09	6	1.7	
	Maximum	51.4	41	19.9	0.72	34.2	0.55	345	98.6	
	Minimum	49.8	31	17.6	0.48	25.6	0.34	324	92.5	

N-value: 28

Sample Interval Time: 37.81 seconds.

Summary of SPT Test Results

Project: DIEDRICH D-50 (SN 316), Test Date: 6/8/2023

SPT Test Results Summary											CSX: Compression Stress Maximum	DFN: Final Displacement	EFV: Maximum Energy	ETR: Energy Transfer Ratio - Rated
Instr. Length ft	Blows Applied /6"	Start Depth ft	Final Depth ft	N Value	N60 Value	Average BPM bpm	Average FMX kips	Average VMX ft/s	Average DMX in	Average CSX ksi	Average DFN in	Average EFV ft-lb	Average ETR %	
35.59	5-14-19	31.00	32.50	33	53	50.2	37	20.9	0.44	30.9	0.36	340	97.2	
37.59	4-11-16	33.50	35.00	27	43	50.4	40	17.9	0.53	33.4	0.44	336	96.1	
39.59	7-12-19	36.00	37.50	31	50	50.7	38	18.2	0.55	31.3	0.39	344	98.2	
42.59	5-11-17	38.50	40.00	28	45	50.7	36	18.8	0.57	29.5	0.43	335	95.7	
Overall Average Values:					50.5	38	19.0	0.52	31.2	0.40	339	96.8		
Standard Deviation:					0.5	3	1.3	0.09	2.1	0.09	10	2.7		
Overall Maximum Value:					51.7	43	22.0	0.74	35.6	0.55	366	104.6		
Overall Minimum Value:					49.2	31	17.0	0.36	25.6	0.31	311	88.8		

CME-550X SN 299403

JRW

TEST HOLE B

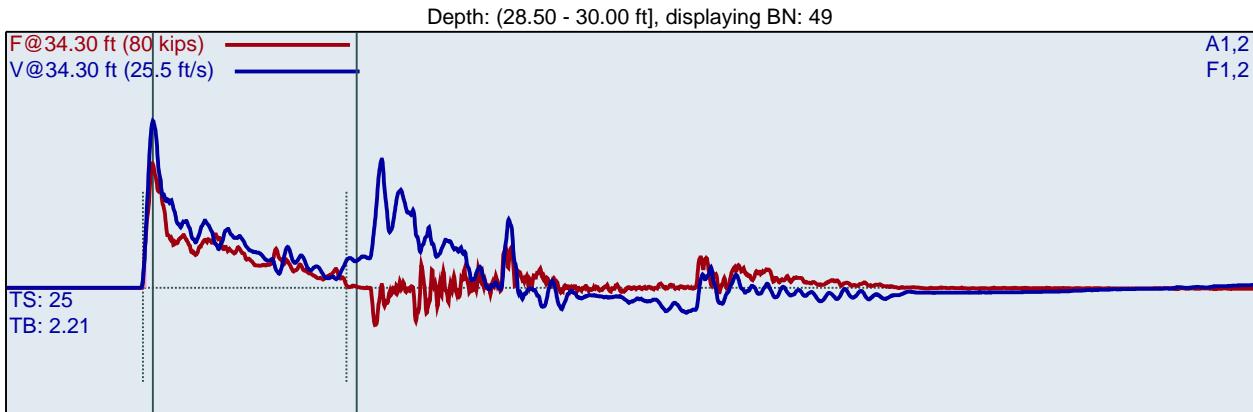
AR: 1.76 in²

LE: 34.30 ft

WS: 16807.9 ft/s

ANNUAL ENERGY MEASUREMENTS
Interval start: 1/3/2024

SP: 0.492 k/ft³
EM: 30000 ksi



F1 : [102 BW-1] 216.4 PDICAL (1) FF1
F2 : [102 BW-2] 217.5 PDICAL (1) FF1

A1 (PR): [K10181] 394.1 mv/6.4v/5000g (1) VF1
A2 (PR): [K10182] 380.7 mv/6.4v/5000g (1) VF1

BPM: Blows/Minute

CSX: Compression Stress Maximum

FMX: Maximum Force

DFN: Final Displacement

VMX: Maximum Velocity

EFV: Maximum Energy

DMX: Maximum Displacement

ETR: Energy Transfer Ratio - Rated

LP ft	BL#	BC /6"	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
28.54	1	14	1.9	37	18.2	0.76	20.8	0.43	308	88.1
28.57	2	14	59.7	41	18.7	0.65	23.0	0.43	322	91.9
28.61	3	14	56.6	39	17.7	0.59	22.4	0.43	320	91.3
28.64	4	14	56.7	39	17.0	0.56	22.4	0.43	317	90.6
28.68	5	14	56.7	40	17.6	0.55	22.8	0.43	322	92.1
28.71	6	14	56.6	40	17.5	0.56	22.8	0.43	319	91.3
28.75	7	14	56.5	39	16.7	0.59	22.0	0.43	318	90.8
28.79	8	14	56.8	38	15.9	0.55	21.6	0.43	311	88.9
28.82	9	14	56.3	40	17.4	0.55	22.8	0.43	318	90.9
28.86	10	14	56.4	40	17.2	0.53	22.7	0.43	320	91.3
28.89	11	14	56.7	38	16.1	0.52	21.8	0.43	313	89.5
28.93	12	14	56.4	38	15.8	0.51	21.5	0.43	313	89.3
28.96	13	14	56.7	39	16.3	0.47	22.1	0.43	314	89.7
29.00	14	14	56.1	38	16.1	0.47	21.8	0.43	314	89.8
29.03	15	17	56.7	38	15.6	0.48	21.5	0.35	314	89.6
29.06	16	17	56.4	39	16.2	0.48	22.4	0.35	314	89.8
29.09	17	17	56.7	38	16.1	0.48	21.3	0.35	311	88.9
29.12	18	17	56.2	40	16.4	0.47	22.8	0.35	318	90.8
29.15	19	17	56.7	40	16.4	0.45	22.5	0.35	314	89.7
29.18	20	17	56.2	40	16.5	0.46	22.5	0.35	317	90.5
29.21	21	17	56.6	41	16.9	0.46	23.0	0.35	318	90.8
29.24	22	17	56.3	38	16.3	0.45	21.6	0.35	312	89.1
29.26	23	17	56.3	36	15.8	0.44	20.7	0.35	306	87.4
29.29	24	17	56.6	38	16.5	0.45	21.7	0.35	313	89.4
29.32	25	17	56.3	39	16.4	0.44	22.0	0.35	316	90.3
29.35	26	17	56.4	40	16.8	0.44	22.4	0.35	316	90.3
29.38	27	17	56.6	40	16.6	0.44	22.5	0.35	316	90.3

29.41	28	17	55.9	39	16.7	0.45	22.4	0.35	321	91.7
29.44	29	17	56.3	38	16.3	0.43	21.4	0.35	311	88.9
29.47	30	17	56.5	39	16.7	0.43	22.3	0.35	319	91.2
29.50	31	17	56.2	39	16.8	0.43	22.4	0.35	318	90.7
29.53	32	20	56.1	36	15.9	0.43	20.4	0.30	307	87.7
29.55	33	20	56.3	39	16.7	0.43	22.3	0.30	320	91.5
29.58	34	20	56.3	38	16.8	0.43	21.5	0.30	317	90.6
29.60	35	20	56.3	38	16.4	0.43	21.7	0.30	317	90.7
29.63	36	20	55.9	38	16.3	0.41	21.7	0.30	308	88.1
29.65	37	20	56.6	41	17.0	0.43	23.1	0.30	325	92.8
29.68	38	20	55.9	40	16.9	0.41	22.9	0.30	322	92.0
29.70	39	20	56.3	41	17.4	0.42	23.5	0.30	327	93.3
29.73	40	20	56.4	41	17.2	0.42	23.4	0.30	322	91.9
29.75	41	20	56.4	38	16.3	0.42	21.6	0.30	315	89.9
29.78	42	20	56.0	39	16.4	0.41	22.2	0.30	317	90.5
29.80	43	20	56.4	37	15.7	0.42	20.9	0.30	313	89.6
29.83	44	20	56.4	37	15.6	0.41	21.0	0.30	315	90.0
29.85	45	20	55.8	41	17.0	0.42	23.4	0.30	327	93.3
29.88	46	20	56.1	41	17.0	0.43	23.2	0.30	326	93.2
29.90	47	20	56.3	40	16.9	0.41	22.9	0.30	317	90.7
29.93	48	20	56.2	35	14.3	0.40	20.1	0.30	304	86.9
29.95	49	20	56.0	39	16.6	0.41	22.1	0.30	316	90.2
29.98	50	20	56.0	38	16.0	0.41	21.4	0.30	317	90.7
30.00	51	20	56.4	38	16.1	0.41	21.6	0.30	310	88.5
Average		56.3	39	16.4	0.43	22.1	0.32	316	90.3	
Std Dev		0.2	1	0.6	0.02	0.8	0.03	5	1.5	
Maximum		56.7	41	17.4	0.48	23.5	0.35	327	93.3	
Minimum		55.8	35	14.3	0.40	20.1	0.30	304	86.9	

N-value: 37

Sample Interval Time: 53.08 seconds.

CME-550X SN 299403

JRW

TEST HOLE B

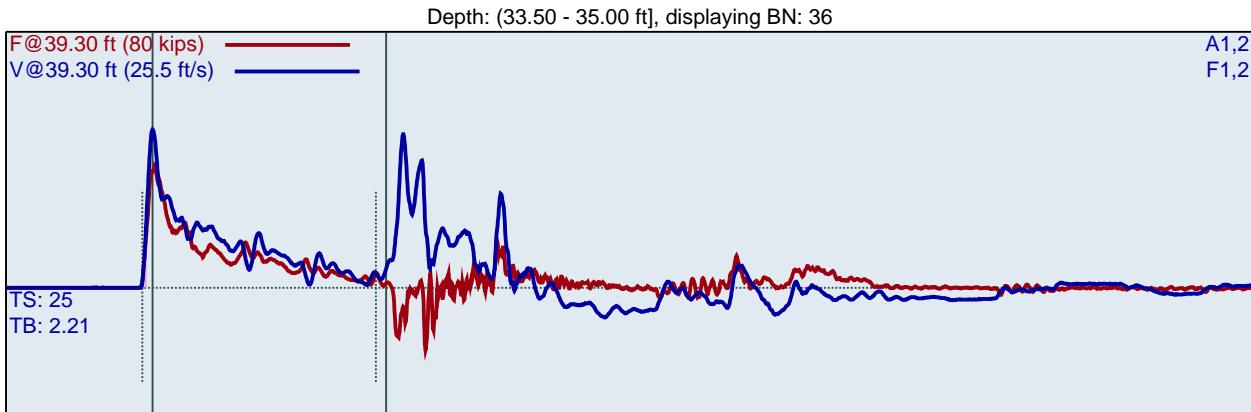
AR: 1.76 in²

LE: 39.30 ft

WS: 16807.9 ft/s

ANNUAL ENERGY MEASUREMENTS
Interval start: 1/3/2024

SP: 0.492 k/ft³
EM: 30000 ksi



F1 : [102 BW-1] 216.4 PDICAL (1) FF1
F2 : [102 BW-2] 217.5 PDICAL (1) FF1

A1 (PR): [K10181] 394.1 mv/6.4v/5000g (1) VF1
A2 (PR): [K10182] 380.7 mv/6.4v/5000g (1) VF1

LP ft	BL#	BC /6"	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
33.53	1	17	1.9	38	16.8	0.71	21.4	0.35	319	91.1
33.56	2	17	56.5	36	15.7	0.59	20.2	0.35	308	88.1
33.59	3	17	56.4	38	17.3	0.56	21.8	0.35	320	91.4
33.62	4	17	56.3	40	17.8	0.53	22.6	0.35	329	94.1
33.65	5	17	56.2	38	17.3	0.49	21.6	0.35	315	90.1
33.68	6	17	56.4	40	18.2	0.50	22.5	0.35	329	94.1
33.71	7	17	56.4	41	18.4	0.48	23.3	0.35	333	95.2
33.74	8	17	56.3	38	17.6	0.45	21.7	0.35	319	91.0
33.76	9	17	56.5	40	18.1	0.45	22.8	0.35	327	93.3
33.79	10	17	55.7	39	18.0	0.45	22.2	0.35	324	92.7
33.82	11	17	56.5	37	17.4	0.45	21.1	0.35	319	91.1
33.85	12	17	56.6	40	18.3	0.45	22.8	0.36	326	93.0
33.88	13	17	56.1	41	18.4	0.45	23.2	0.36	329	94.1
33.91	14	17	56.3	41	18.5	0.45	23.4	0.35	332	94.9
33.94	15	17	56.0	39	17.8	0.42	22.2	0.35	316	90.1
33.97	16	17	56.3	38	17.4	0.43	21.7	0.35	323	92.2
34.00	17	17	56.4	39	17.9	0.42	22.1	0.35	321	91.6
34.02	18	21	55.8	38	17.8	0.43	21.7	0.28	323	92.2
34.05	19	21	56.3	38	17.5	0.44	21.6	0.29	319	91.1
34.07	20	21	56.2	38	17.1	0.43	21.7	0.29	319	91.1
34.10	21	21	56.0	37	17.1	0.42	21.1	0.28	309	88.4
34.12	22	21	56.3	35	15.3	0.41	20.0	0.29	305	87.0
34.14	23	21	56.1	36	16.4	0.41	20.2	0.29	303	86.7
34.17	24	21	56.1	37	17.0	0.42	21.3	0.28	313	89.5
34.19	25	21	55.7	39	17.6	0.41	22.0	0.29	321	91.8
34.21	26	21	56.4	39	17.9	0.42	22.1	0.29	324	92.7
34.24	27	21	56.2	38	17.4	0.40	21.6	0.29	312	89.2
34.26	28	21	55.9	37	17.3	0.42	21.1	0.29	319	91.1
34.29	29	21	55.9	41	17.7	0.42	23.2	0.29	329	93.9
34.31	30	21	56.2	40	17.5	0.41	22.7	0.29	322	92.1
34.33	31	21	56.2	42	17.6	0.42	23.7	0.29	326	93.3

34.36	32	21	56.3	39	16.7	0.42	22.2	0.29	314	89.7
34.38	33	21	56.0	38	16.6	0.41	21.8	0.29	316	90.3
34.40	34	21	56.2	39	16.5	0.41	22.1	0.29	319	91.2
34.43	35	21	56.1	40	17.0	0.41	23.0	0.29	323	92.2
34.45	36	21	55.8	38	15.8	0.41	21.7	0.29	317	90.7
34.48	37	21	56.0	36	16.1	0.40	20.5	0.29	306	87.4
34.50	38	21	56.2	38	15.0	0.41	21.3	0.29	313	89.4
34.52	39	21	55.9	39	16.7	0.41	22.4	0.29	324	92.5
34.55	40	21	56.0	40	17.1	0.41	22.5	0.29	322	91.9
34.57	41	21	56.1	42	17.4	0.41	23.7	0.29	324	92.6
34.60	42	21	56.1	40	17.4	0.41	22.6	0.28	320	91.3
34.62	43	21	56.1	38	16.2	0.40	21.4	0.29	308	88.0
34.64	44	21	55.9	39	15.9	0.41	22.2	0.29	320	91.4
34.67	45	21	56.2	38	16.0	0.40	21.5	0.28	313	89.5
34.69	46	21	56.0	40	17.1	0.41	22.5	0.29	326	93.2
34.71	47	21	56.1	42	17.4	0.39	24.0	0.29	325	92.7
34.74	48	21	55.9	41	17.6	0.41	23.4	0.29	324	92.6
34.76	49	21	55.9	39	16.9	0.41	22.1	0.29	320	91.5
34.79	50	21	56.2	36	15.4	0.41	20.5	0.29	307	87.7
34.81	51	21	56.0	41	17.5	0.42	23.4	0.29	328	93.6
34.83	52	21	55.8	41	17.9	0.41	23.4	0.29	326	93.2
34.86	53	21	56.2	38	16.5	0.40	21.5	0.29	315	90.0
34.88	54	21	55.9	39	17.6	0.41	22.4	0.29	321	91.8
34.90	55	21	56.3	39	17.2	0.41	21.9	0.29	319	91.1
34.93	56	21	56.1	40	17.5	0.41	22.6	0.29	325	92.8
34.95	57	21	56.2	38	17.1	0.41	21.5	0.28	316	90.4
34.98	58	21	55.8	37	16.5	0.41	21.2	0.29	315	90.0
35.00	59	21	56.1	36	16.0	0.40	20.6	0.29	303	86.5
Average			56.1	39	16.9	0.41	22.0	0.29	318	90.8
Std Dev			0.2	2	0.7	0.01	1.0	0.00	7	2.0
Maximum			56.4	42	17.9	0.44	24.0	0.29	329	93.9
Minimum			55.7	35	15.0	0.39	20.0	0.28	303	86.5

N-value: 42

Sample Interval Time: 61.90 seconds.

CME-550X SN 299403

JRW

TEST HOLE B

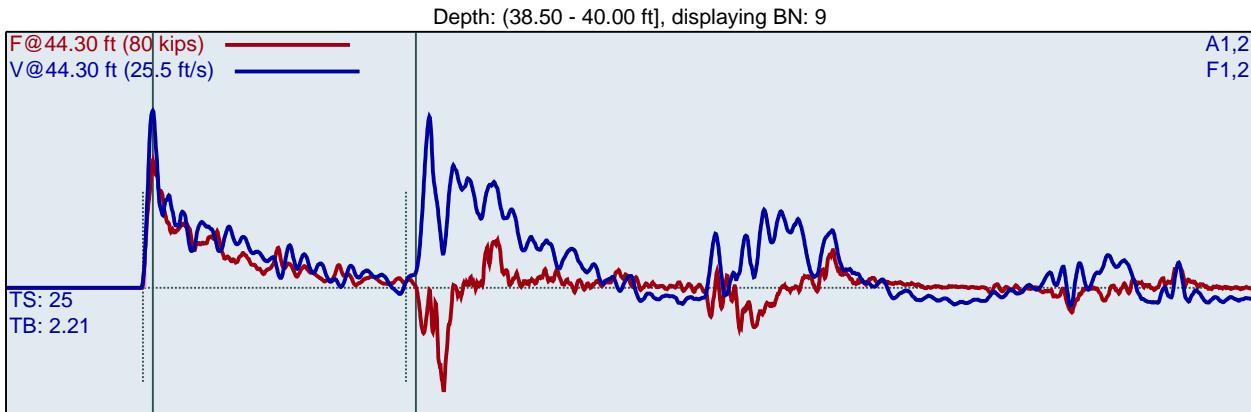
AR: 1.76 in²

LE: 44.30 ft

WS: 16807.9 ft/s

ANNUAL ENERGY MEASUREMENTS
Interval start: 1/3/2024

SP: 0.492 k/ft³
EM: 30000 ksi



F1 : [102 BW-1] 216.4 PDICAL (1) FF1
F2 : [102 BW-2] 217.5 PDICAL (1) FF1

A1 (PR): [K10181] 394.1 mv/6.4v/5000g (1) VF1
A2 (PR): [K10182] 380.7 mv/6.4v/5000g (1) VF1

LP ft	BL#	BC /6"	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
38.58	1	6	1.9	39	17.8	1.21	22.2	1.00	322	91.9
38.67	2	6	56.9	40	17.7	1.07	22.5	1.00	325	92.8
38.75	3	6	57.0	38	17.2	1.02	21.7	1.00	316	90.4
38.83	4	6	57.4	41	18.8	1.05	23.3	1.00	332	95.0
38.92	5	6	57.0	39	17.5	1.04	22.0	1.00	318	90.9
39.00	6	6	57.2	40	18.5	1.01	22.8	1.00	324	92.5
39.04	7	13	57.3	38	17.4	0.78	21.7	0.46	313	89.4
39.08	8	13	57.2	40	17.9	0.72	22.6	0.46	319	91.3
39.12	9	13	57.2	40	17.6	0.65	22.6	0.46	318	90.8
39.15	10	13	57.5	39	17.5	0.62	22.2	0.46	317	90.4
39.19	11	13	57.0	42	18.7	0.58	23.8	0.46	330	94.3
39.23	12	13	57.5	39	17.4	0.54	22.3	0.46	313	89.3
39.27	13	13	57.1	39	17.1	0.52	22.1	0.46	311	89.0
39.31	14	13	57.1	39	16.9	0.50	22.0	0.46	304	87.0
39.35	15	13	57.6	39	17.0	0.48	21.9	0.45	307	87.9
39.38	16	13	56.8	40	17.6	0.50	22.7	0.46	317	90.7
39.42	17	13	57.1	41	18.3	0.49	23.5	0.47	322	92.1
39.46	18	13	57.3	41	17.9	0.49	23.0	0.47	320	91.3
39.50	19	13	57.4	38	16.9	0.49	21.8	0.46	307	87.8
39.54	20	14	57.0	40	17.7	0.47	22.7	0.43	317	90.7
39.57	21	14	57.1	38	16.9	0.49	21.6	0.43	311	88.8
39.61	22	14	57.4	40	17.9	0.47	22.8	0.43	314	89.8
39.64	23	14	57.2	39	16.9	0.45	22.0	0.43	309	88.2
39.68	24	14	57.1	39	17.1	0.52	22.0	0.43	315	89.9
39.71	25	14	57.2	41	18.0	0.49	23.2	0.43	322	91.9
39.75	26	14	57.1	40	17.7	0.48	22.8	0.43	316	90.2
39.79	27	14	57.1	40	17.7	0.49	22.6	0.43	317	90.6
39.82	28	14	57.0	40	17.5	0.51	22.7	0.43	319	91.3
39.86	29	14	57.4	39	17.4	0.47	22.3	0.43	312	89.0
39.89	30	14	57.1	41	18.3	0.50	23.4	0.43	325	92.9
39.93	31	14	56.9	40	17.5	0.48	22.5	0.43	316	90.3

GRL Engineers, Inc.
SPT Analyzer Results

Page 6 of 9
PDA-S Ver. 2022.35.2 - Printed: 1/4/2024

39.96	32	14	57.2	42	18.8	0.48	24.0	0.43	329	94.1
40.00	33	14	57.2	40	17.6	0.44	22.5	0.43	316	90.4
<hr/>										
	Average		57.2	40	17.6	0.52	22.6	0.44	316	90.3
	Std Dev		0.2	1	0.5	0.08	0.6	0.02	6	1.7
	Maximum		57.6	42	18.8	0.78	24.0	0.47	330	94.3
	Minimum		56.8	38	16.9	0.44	21.6	0.43	304	87.0

N-value: 27

Sample Interval Time: 33.54 seconds.

CME-550X SN 299403

JRW

TEST HOLE B

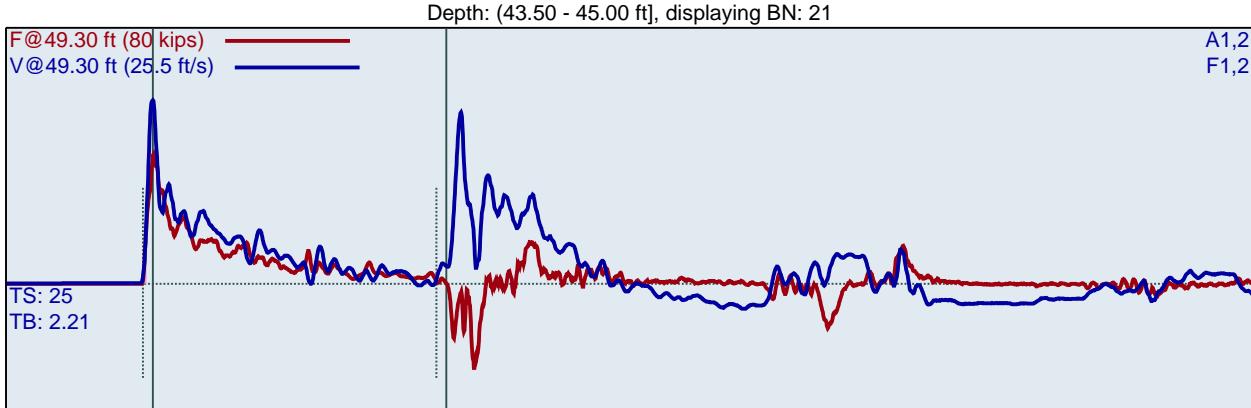
AR: 1.76 in²

LE: 49.30 ft

WS: 16807.9 ft/s

ANNUAL ENERGY MEASUREMENTS
Interval start: 1/3/2024

SP: 0.492 k/ft³
EM: 30000 ksi



F1 : [102 BW-1] 216.4 PDICAL (1) FF1
F2 : [102 BW-2] 217.5 PDICAL (1) FF1

A1 (PR): [K10181] 394.1 mv/6.4v/5000g (1) VF1
A2 (PR): [K10182] 380.7 mv/6.4v/5000g (1) VF1

LP ft	BL#	BC /6"	BPM bpm	FMX kips	VMX ft/s	DMX in	CSX ksi	DFN in	EFV ft-lb	ETR %
43.54	1	13	1.9	34	15.5	0.73	19.5	0.46	302	86.4
43.58	2	13	57.4	36	15.9	0.62	20.4	0.46	314	89.8
43.62	3	13	57.4	38	16.5	0.57	21.4	0.47	317	90.6
43.65	4	13	57.3	42	18.9	0.54	24.1	0.46	335	95.7
43.69	5	13	57.7	42	19.0	0.53	24.0	0.46	334	95.6
43.73	6	13	57.6	38	17.3	0.50	21.8	0.46	322	92.0
43.77	7	13	57.4	41	18.2	0.50	23.2	0.46	321	91.6
43.81	8	13	57.4	35	16.0	0.50	20.2	0.46	309	88.3
43.85	9	13	57.7	39	17.3	0.49	22.4	0.46	317	90.7
43.88	10	13	57.4	41	18.7	0.50	23.4	0.46	326	93.0
43.92	11	13	57.7	41	18.5	0.49	23.4	0.46	327	93.4
43.96	12	13	57.3	41	18.4	0.49	23.1	0.47	331	94.6
44.00	13	13	57.2	40	18.0	0.48	22.8	0.46	326	93.2
44.03	14	15	57.8	42	19.3	0.51	23.8	0.40	336	95.9
44.07	15	15	57.3	41	19.0	0.49	23.3	0.40	331	94.6
44.10	16	15	57.7	40	18.3	0.48	22.9	0.40	321	91.7
44.13	17	15	57.5	42	18.8	0.49	23.6	0.40	328	93.6
44.17	18	15	57.6	39	17.6	0.48	22.4	0.40	315	89.9
44.20	19	15	57.5	43	19.8	0.50	24.5	0.40	333	95.2
44.23	20	15	57.8	42	19.2	0.49	24.1	0.40	330	94.3
44.27	21	15	57.3	41	18.3	0.47	23.0	0.40	324	92.4
44.30	22	15	57.6	40	17.8	0.47	22.5	0.40	319	91.0
44.33	23	15	57.3	43	19.6	0.50	24.6	0.40	336	95.9
44.37	24	15	57.7	39	17.5	0.47	22.1	0.40	315	90.1
44.40	25	15	57.4	42	19.3	0.47	23.8	0.40	330	94.2
44.43	26	15	57.3	44	19.6	0.49	24.8	0.40	339	96.8
44.47	27	15	57.9	39	17.6	0.45	22.3	0.40	315	89.9
44.50	28	15	57.2	40	18.2	0.45	22.5	0.40	320	91.3
44.53	29	17	57.7	41	18.6	0.47	23.4	0.36	330	94.4
44.56	30	17	57.3	38	17.0	0.44	21.7	0.35	309	88.3
44.59	31	17	57.3	38	17.2	0.45	21.3	0.35	310	88.5

44.62	32	17	57.4	37	17.6	0.45	21.2	0.36	312	89.3
44.65	33	17	57.6	42	19.0	0.48	24.1	0.35	335	95.7
44.68	34	17	57.3	40	18.0	0.45	23.0	0.36	322	92.1
44.71	35	17	57.4	39	17.4	0.45	22.2	0.35	315	89.9
44.74	36	17	57.3	40	18.3	0.46	22.7	0.36	327	93.4
44.76	37	17	57.5	41	18.8	0.47	23.1	0.36	326	93.3
44.79	38	17	57.2	42	19.4	0.48	24.0	0.35	333	95.3
44.82	39	17	57.4	40	18.5	0.47	22.9	0.35	323	92.2
44.85	40	17	57.3	40	18.0	0.47	22.7	0.35	322	91.9
44.88	41	17	57.0	39	17.5	0.45	22.3	0.35	315	90.1
44.91	42	17	57.6	40	17.8	0.47	22.5	0.36	319	91.0
44.94	43	17	57.5	39	17.5	0.46	22.0	0.35	311	88.8
44.97	44	17	57.1	41	18.8	0.50	23.5	0.34	331	94.5
45.00	45	17	18.4	41	18.9	0.50	23.4	0.35	345	98.6
Average			56.2	40	18.4	0.47	23.0	0.38	324	92.6
Std Dev			6.8	2	0.8	0.02	0.9	0.02	9	2.6
Maximum			57.9	44	19.8	0.51	24.8	0.40	345	98.6
Minimum			18.4	37	17.0	0.44	21.2	0.34	309	88.3

N-value: 32

Sample Interval Time: 48.11 seconds.

Summary of SPT Test Results

Project: CME-550X SN 299403, Test Date: 1/3/2024

SPT Test Results Summary											CSX: Compression Stress Maximum		
SPT Test Results Summary											DFN: Final Displacement		
SPT Test Results Summary											EFV: Maximum Energy		
SPT Test Results Summary											ETR: Energy Transfer Ratio - Rated		
Instr. Length ft	Start Depth ft	Final Depth ft	Blows Applied /6"	N Value	N60 Value	Average BPM bpm	Average FMX kips	Average VMX ft/s	Average DMX in	Average CSX ksi	Average DFN in	Average EFV ft-lb	Average ETR %
34.30	28.50	30.00	14-17-20	37	56	56.3	39	16.4	0.43	22.1	0.32	316	90.3
39.30	33.50	35.00	17-21-21	42	63	56.1	39	16.9	0.41	22.0	0.29	318	90.8
44.30	38.50	40.00	6-13-14	27	40	57.2	40	17.6	0.52	22.6	0.44	316	90.3
49.30	43.50	45.00	13-15-17	32	48	56.2	40	18.4	0.47	23.0	0.38	324	92.6
Overall Average Values:				56.4	39	17.2	0.45	22.4	0.35	319	91.0		
Standard Deviation:				3.3	2	1.0	0.06	1.0	0.06	8	2.2		
Overall Maximum Value:				57.9	44	19.8	0.78	24.8	0.47	345	98.6		
Overall Minimum Value:				18.4	35	14.3	0.39	20.0	0.28	303	86.5		

Appendix VI – Laboratory Test Data Sheets – Split-Spoon Samples



INDEX PROPERTIES VERSUS DEPTH

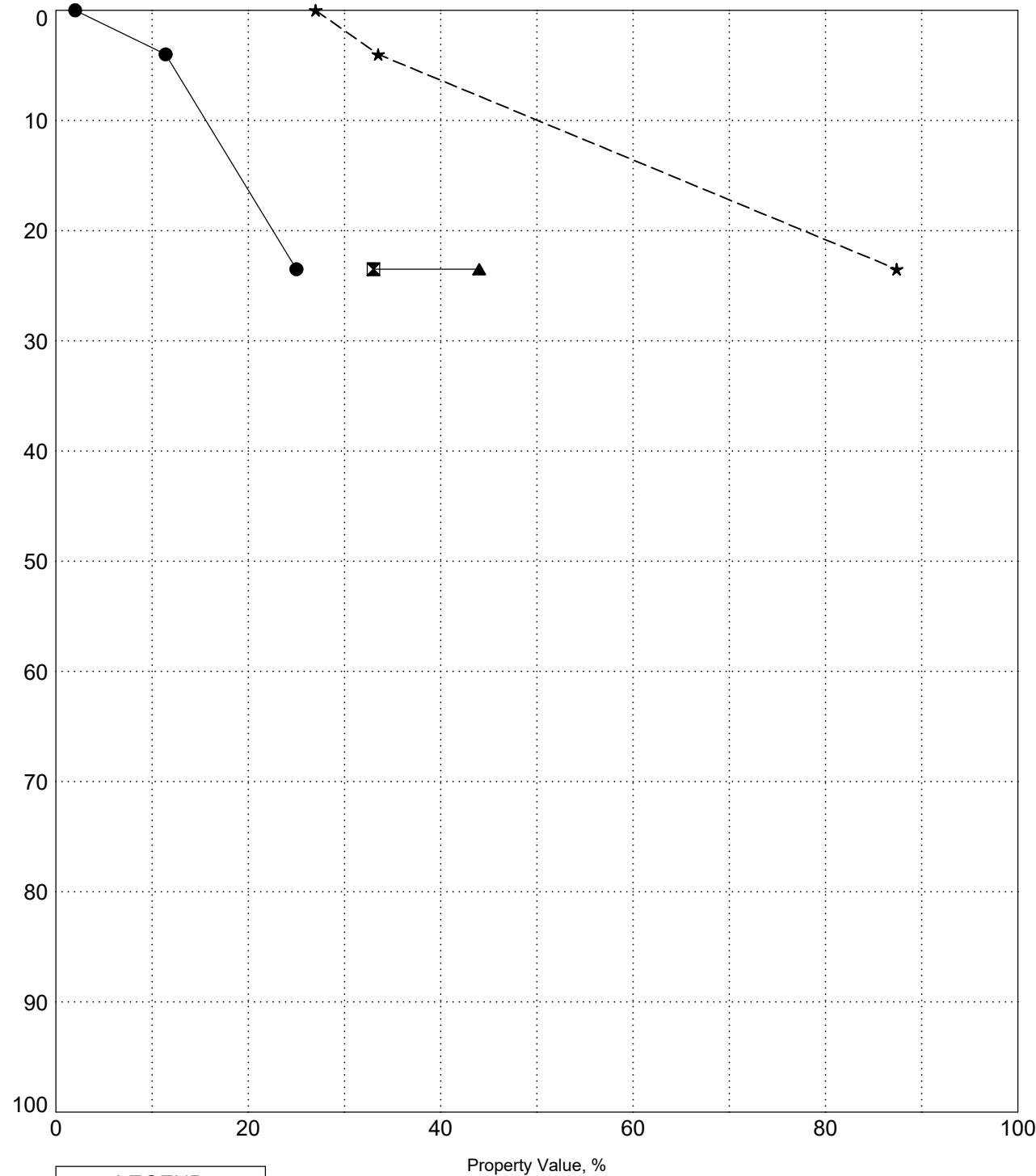
PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING EB-1C

SURFACE ELEVATION: 460.2



LEGEND	
●	Water Content
■	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

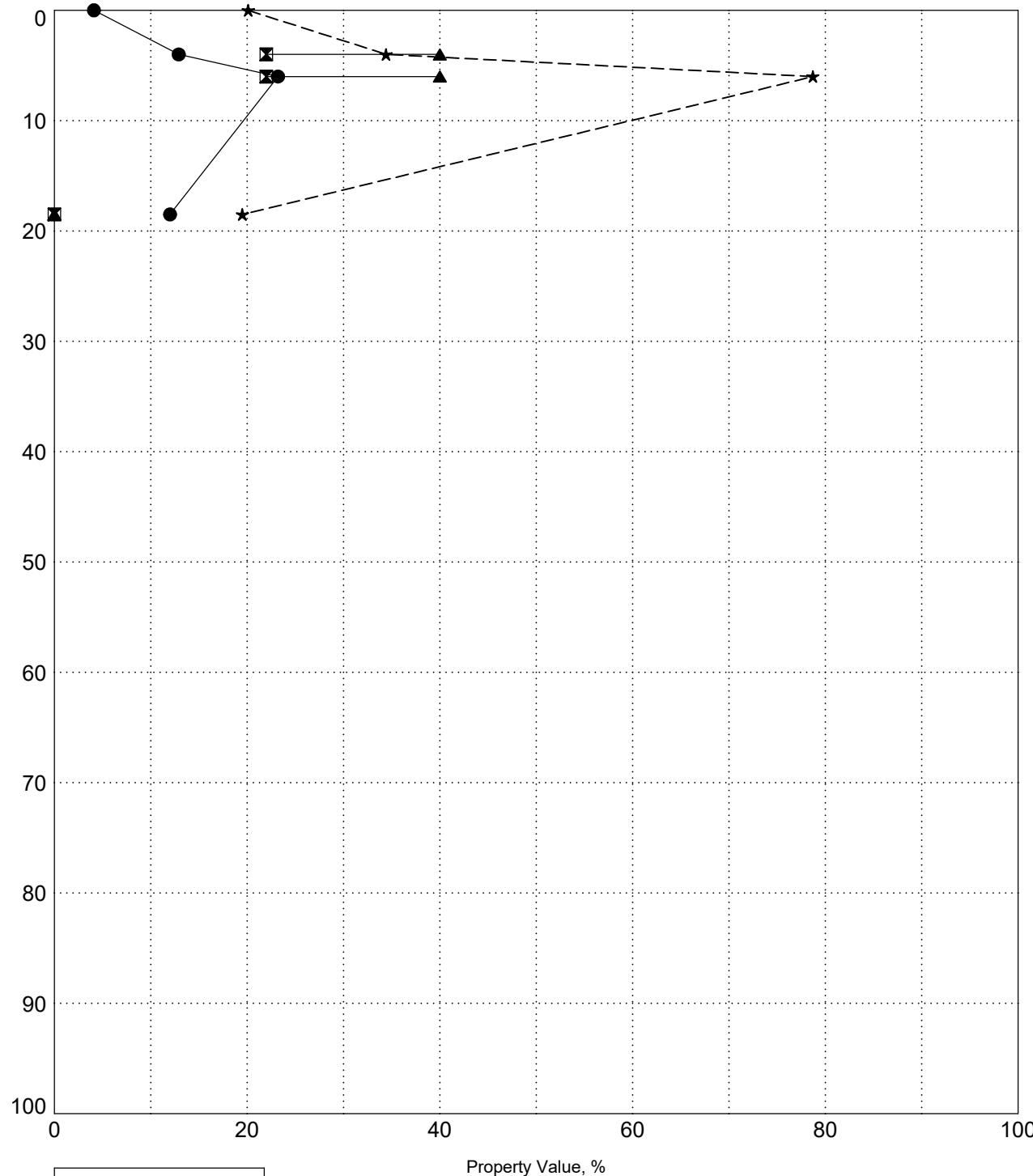
PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING EB-2C

SURFACE ELEVATION: 461.1



LEGEND	
●	Water Content
◻	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

PROJECT ID P042443 (S&ME 23610178A)

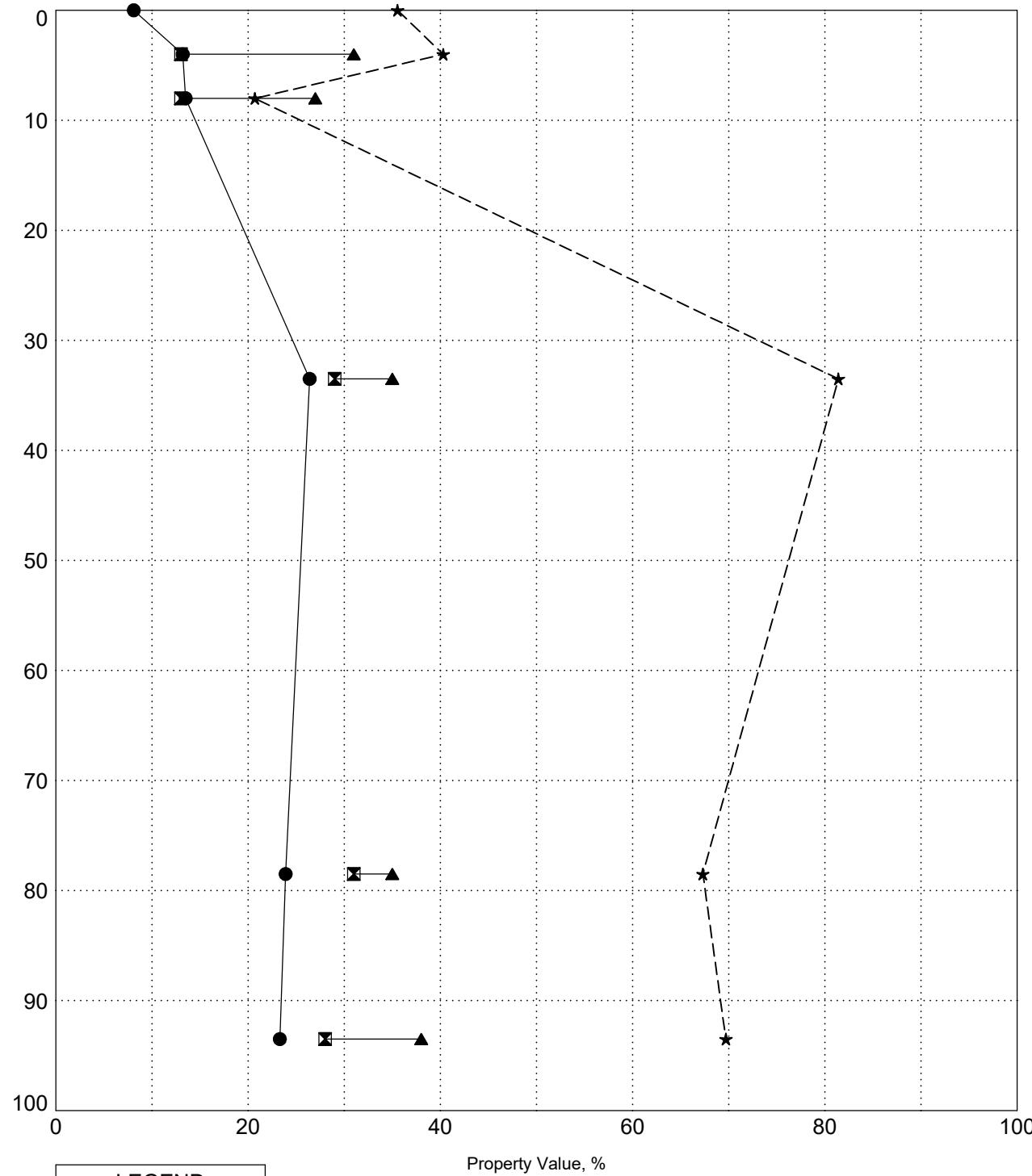
PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING EB-3C

SURFACE ELEVATION: 453.7

INDEX PROPS 23610178A CONNECTOR BRIDGE OVER I-77.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 1/12/24



LEGEND	
●	Water Content
◻	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

PROJECT ID P042443 (S&ME 23610178A)

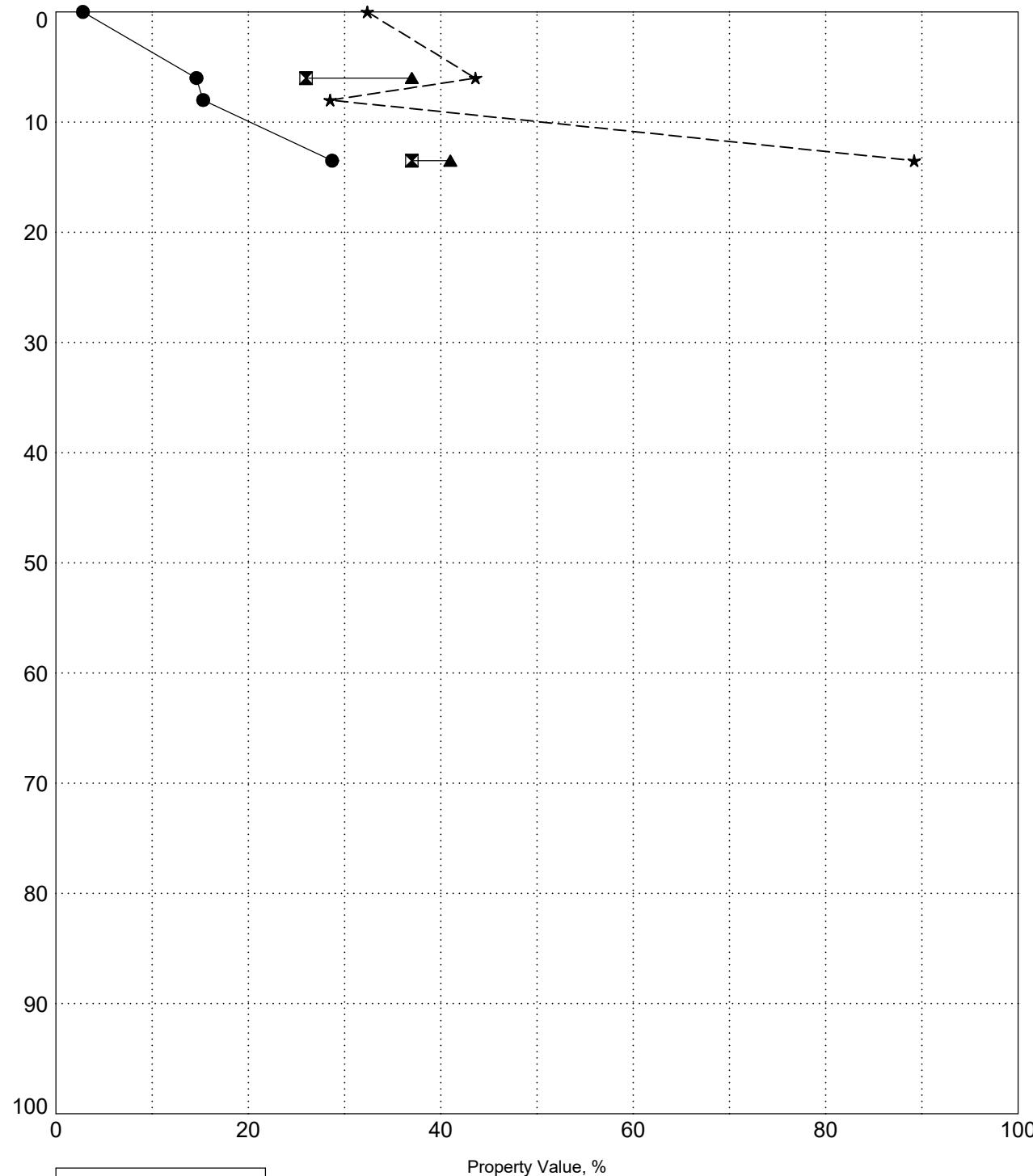
PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING EB-4C

SURFACE ELEVATION: 456.3

INDEX PROPS 23610178A CONNECTOR BRIDGE OVER I-77.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 1/12/24



LEGEND	
●	Water Content
■	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

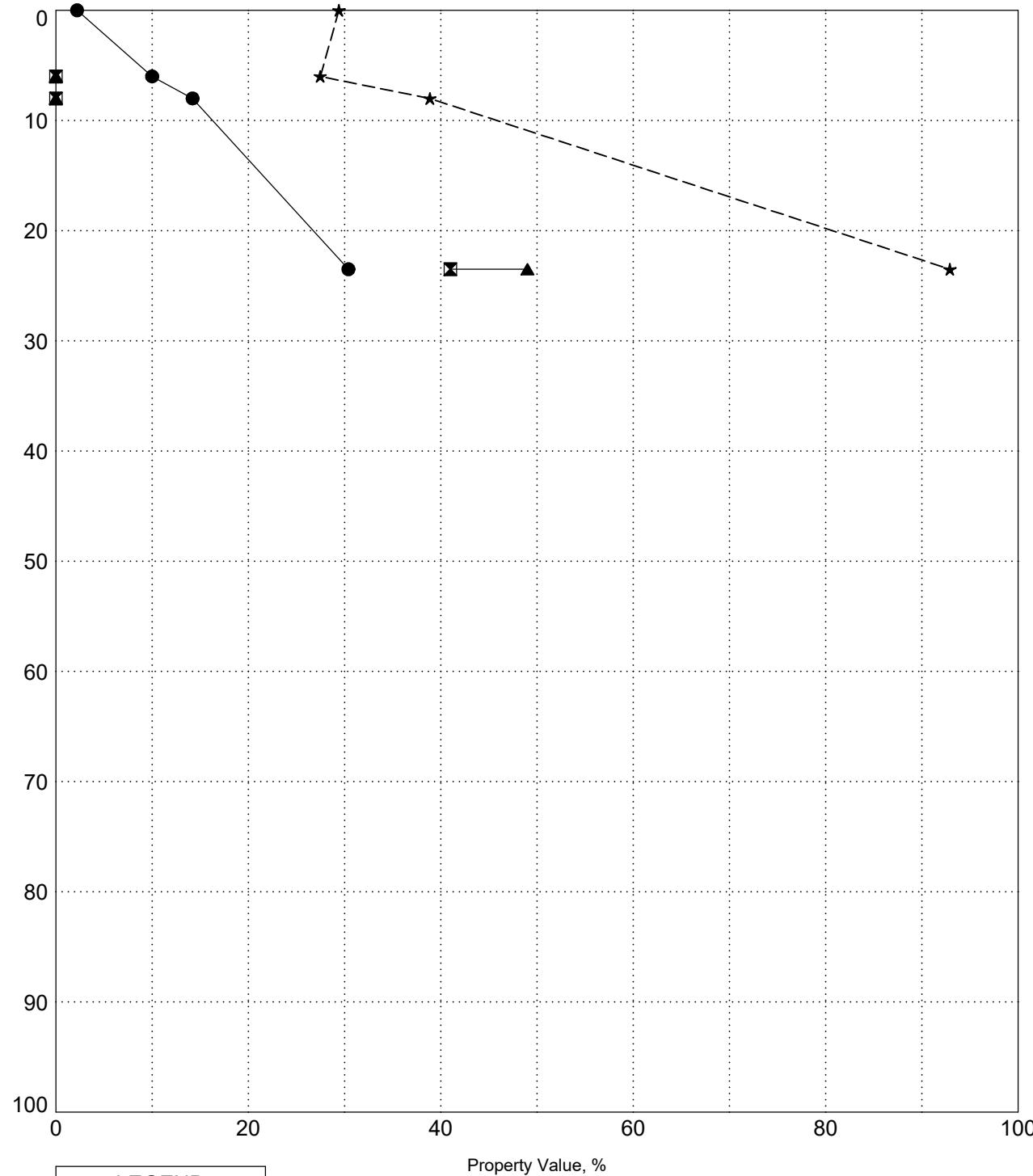
PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING EB-5C

SURFACE ELEVATION: 466.5



LEGEND	
●	Water Content
■	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

PROJECT ID P042443 (S&ME 23610178A)

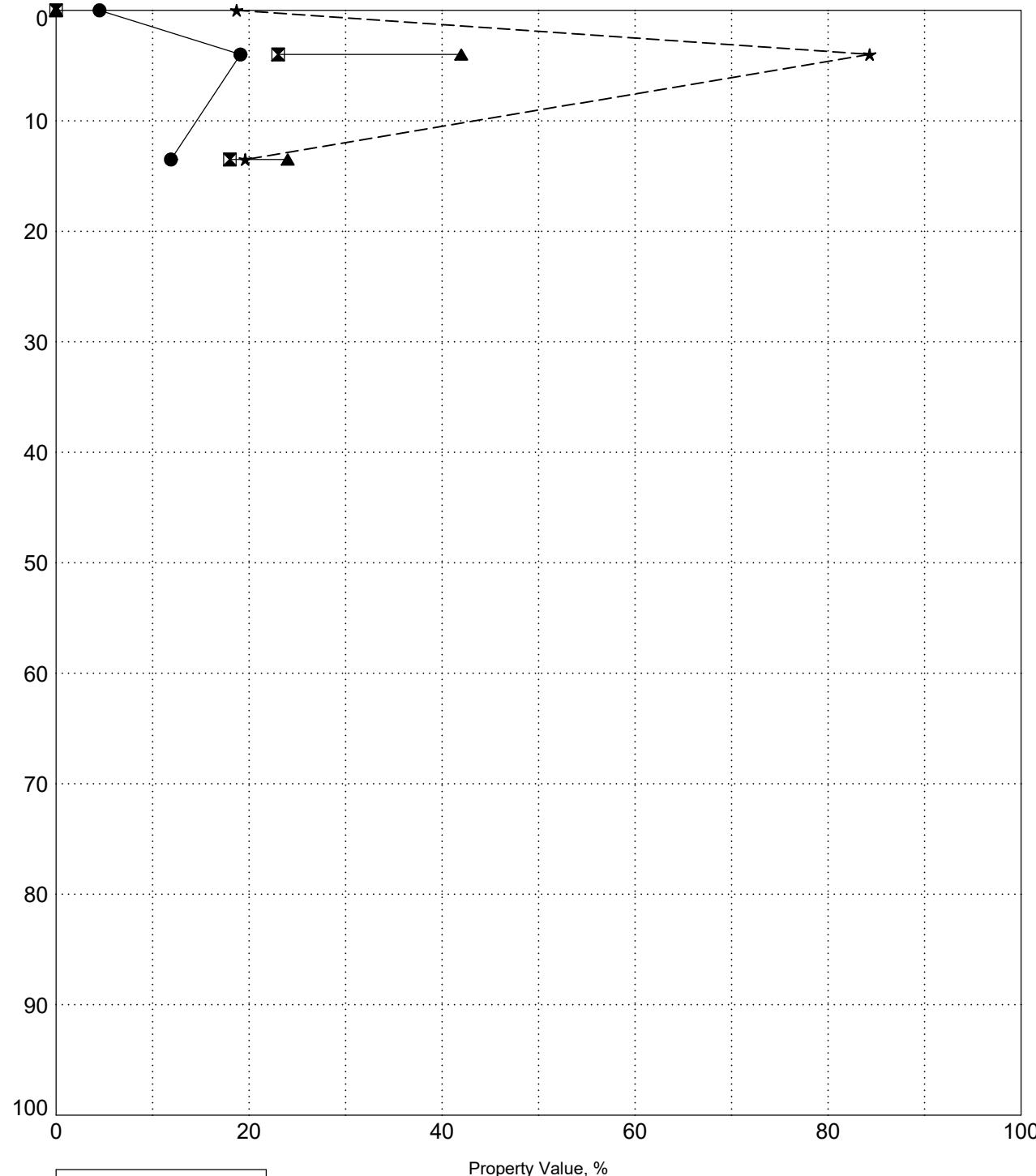
PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING EB-6C

SURFACE ELEVATION: 456.0

INDEX PROPS 23610178A CONNECTOR BRIDGE OVER I-77.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 1/12/24



LEGEND	
●	Water Content
◻	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

PROJECT ID P042443 (S&ME 23610178A)

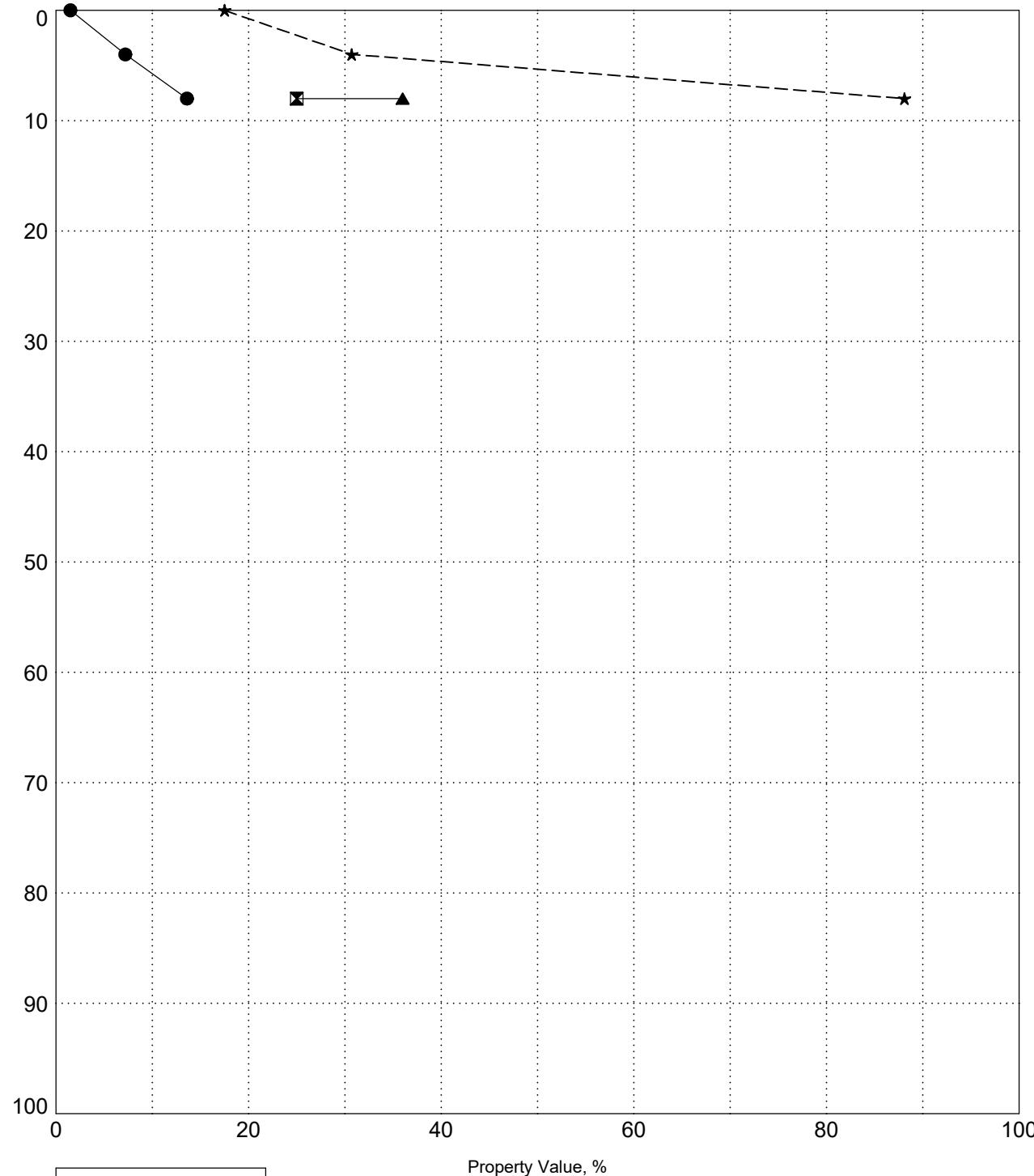
PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING EM-1

SURFACE ELEVATION: 458.6

INDEX PROPS 23610178A CONNECTOR BRIDGE OVER I-77.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 1/12/24



LEGEND	
●	Water Content
◻	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

PROJECT ID P042443 (S&ME 23610178A)

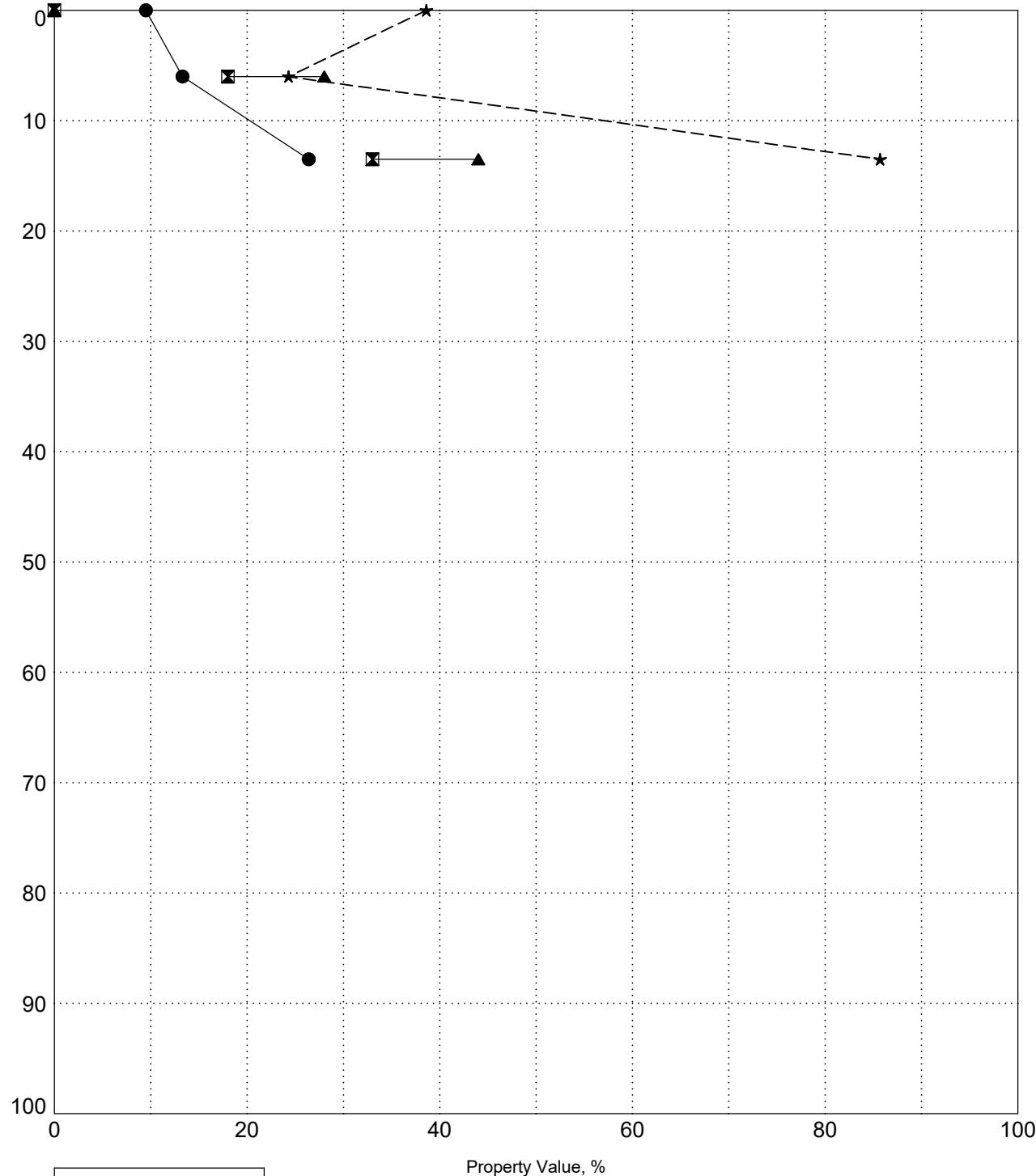
PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING EM-2

SURFACE ELEVATION: 452.4

INDEX PROPS 23610178A CONNECTOR BRIDGE OVER I-77.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 1/12/24



LEGEND	
●	Water Content
◻	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

PROJECT ID P042443 (S&ME 23610178A)

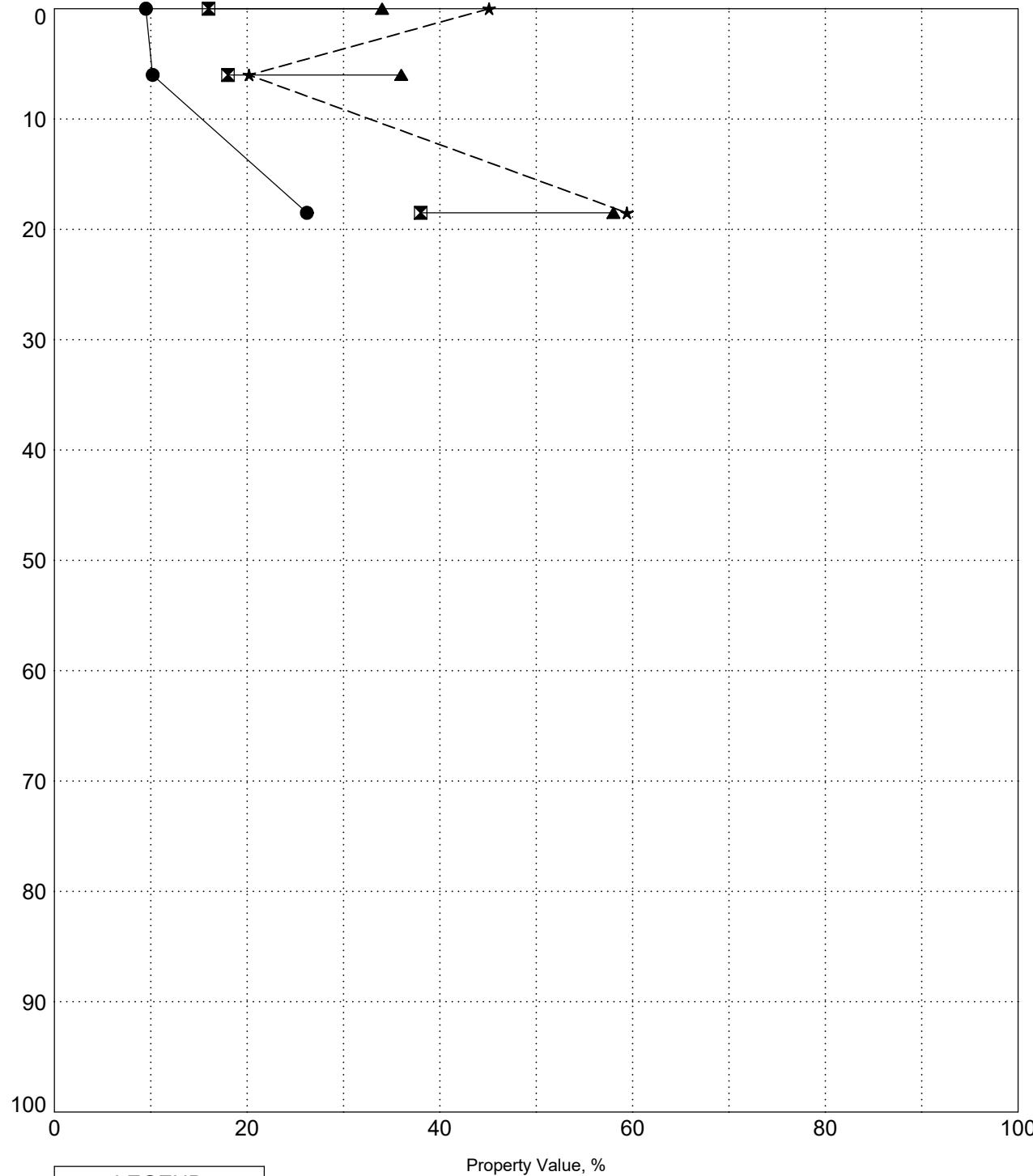
PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING IB- 1C

SURFACE ELEVATION: 455.3

INDEX PROPS 23610178A CONNECTOR BRIDGE OVER I-77.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 1/12/24



LEGEND	
●	Water Content
◻	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

PROJECT ID P042443 (S&ME 23610178A)

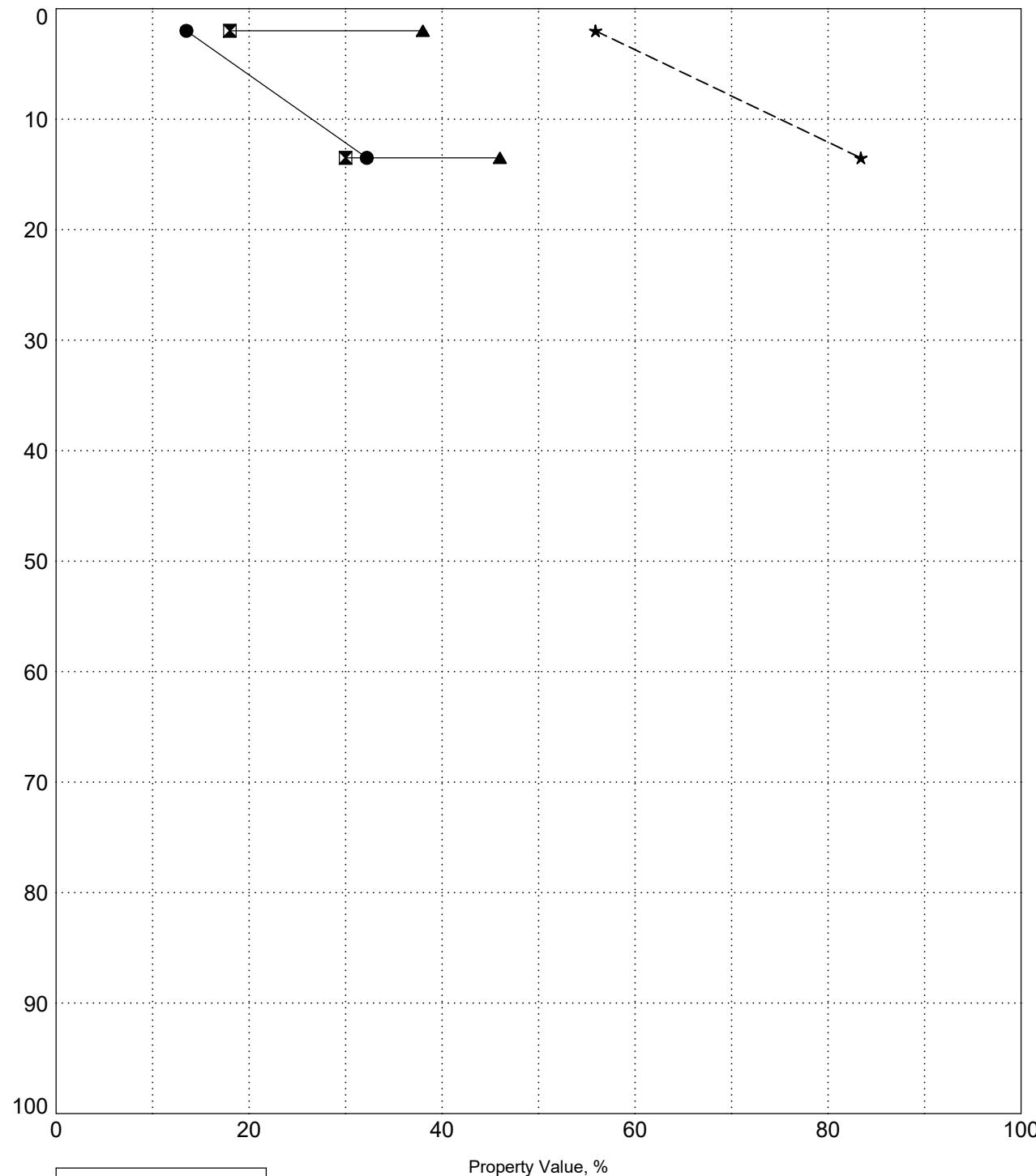
PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING IB- 2C

SURFACE ELEVATION: 455.8

INDEX PROPS 23610178A CONNECTOR BRIDGE OVER I-77.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 1/12/24



LEGEND	
●	Water Content
◻	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

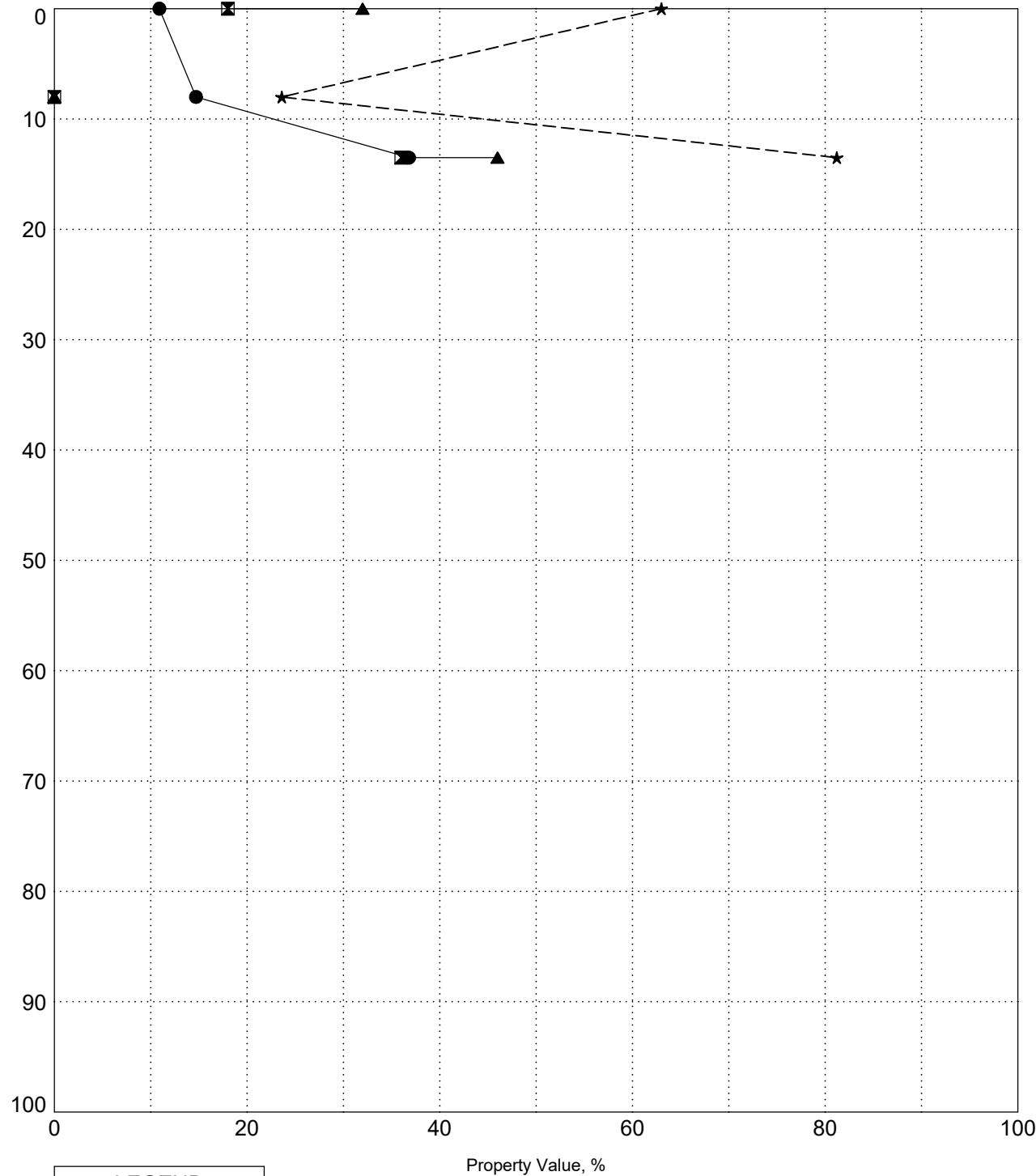
PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING IB- 3C

SURFACE ELEVATION: 455.3



LEGEND	
●	Water Content
■	Plastic Limit
▲	Liquid Limit
★	Fines

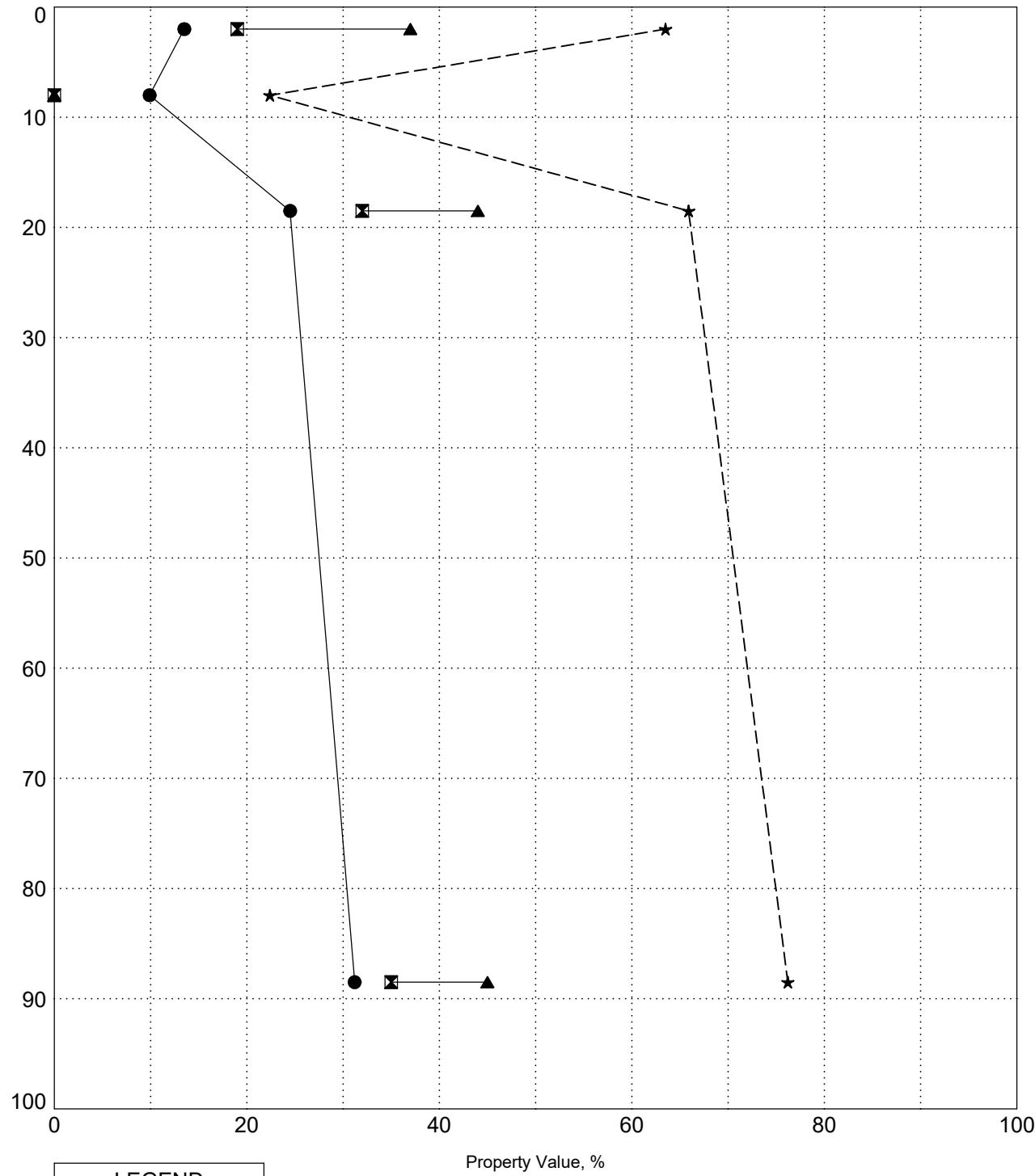
PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING IB- 4C

SURFACE ELEVATION: 455.5



LEGEND	
●	Water Content
◻	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

PROJECT ID P042443 (S&ME 23610178A)

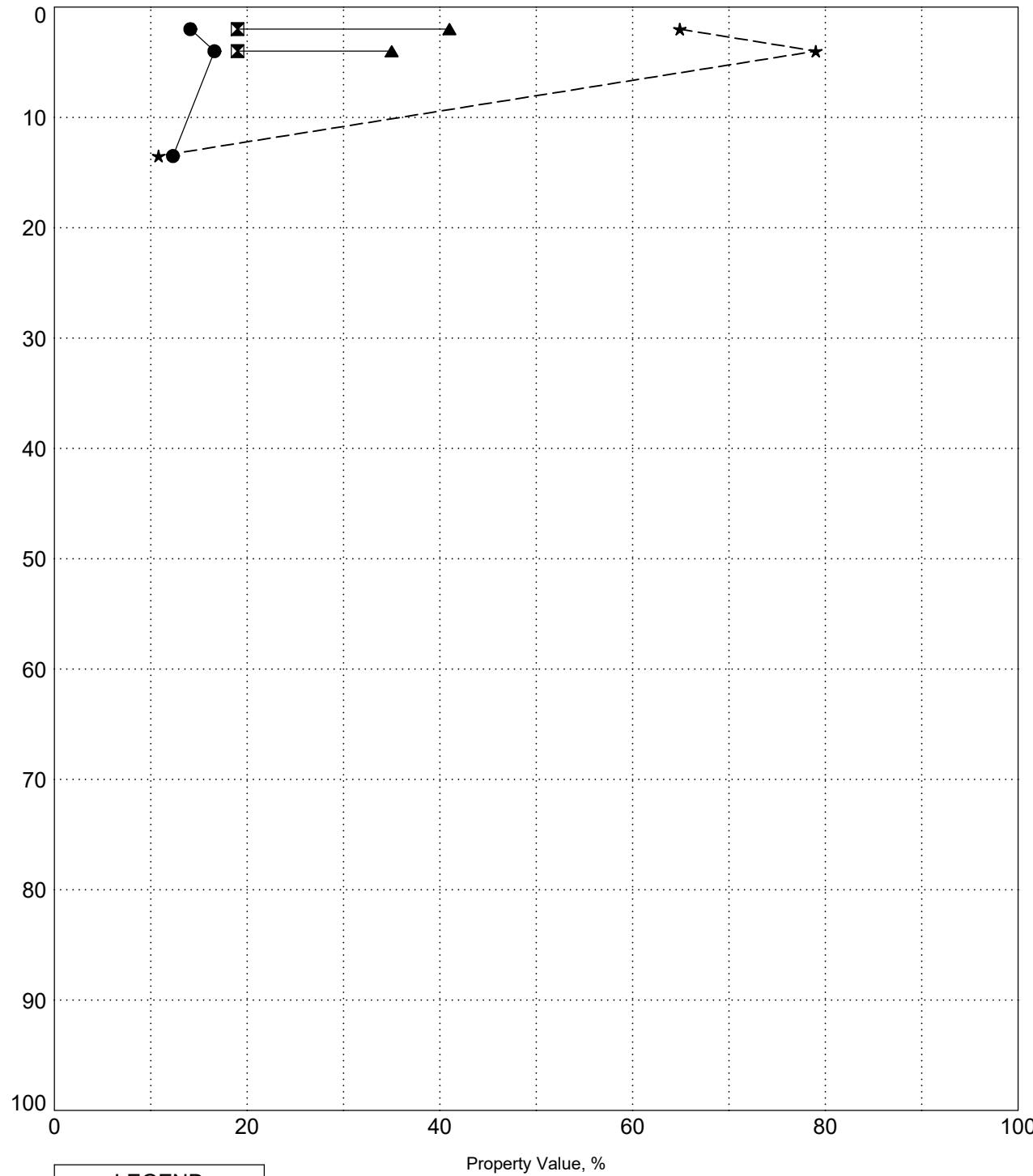
PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING IB- 5C

SURFACE ELEVATION: 456.0

INDEX PROPS 23610178A CONNECTOR BRIDGE OVER I-77.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 1/12/24



LEGEND	
●	Water Content
■	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

PROJECT ID P042443 (S&ME 23610178A)

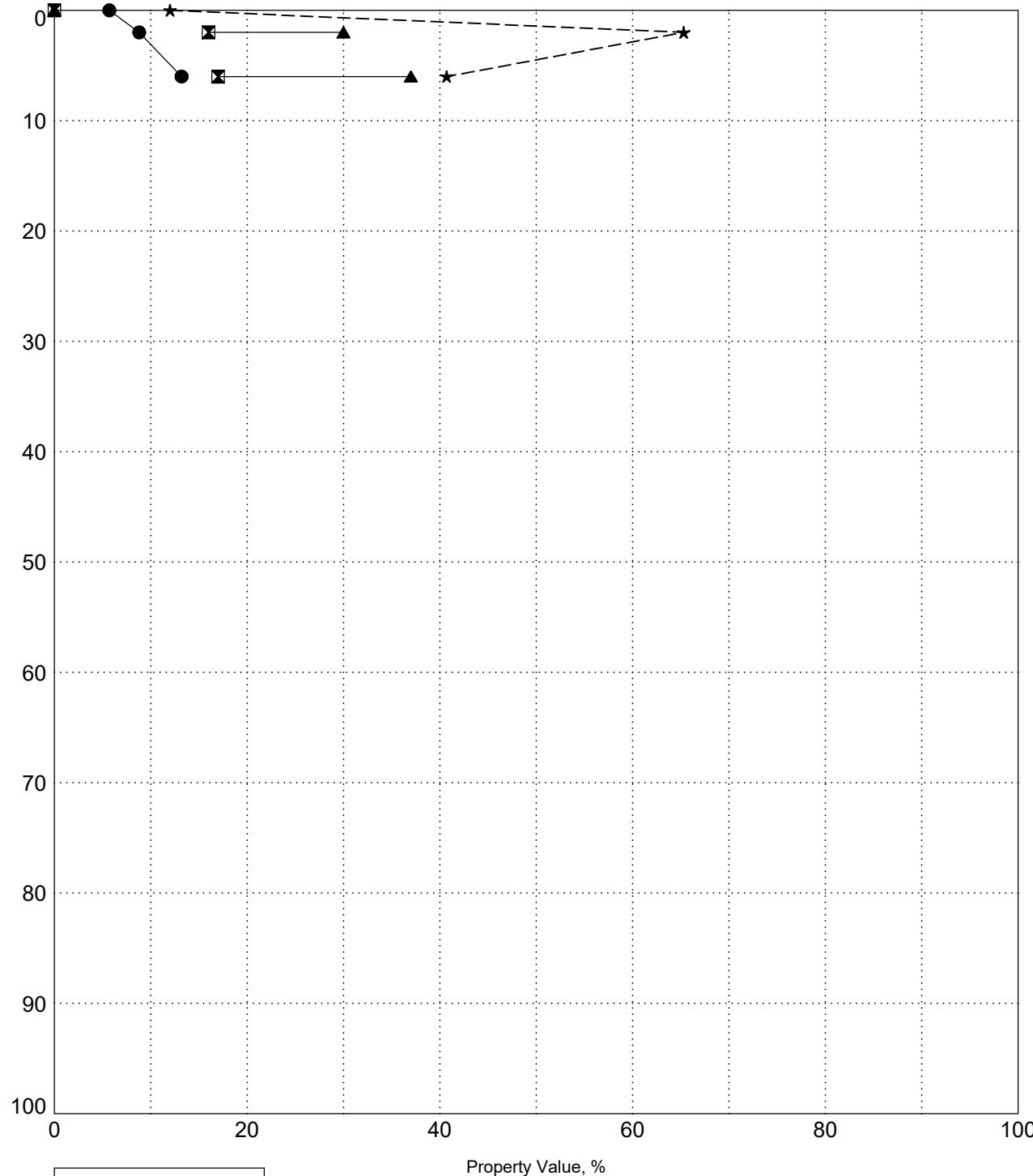
PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

SURFACE ELEVATION: 455.6

BORING IB- 6C

INDEX PROPS 23610178A CONNECTOR BRIDGE OVER I-77.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 1/12/24



LEGEND	
●	Water Content
■	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

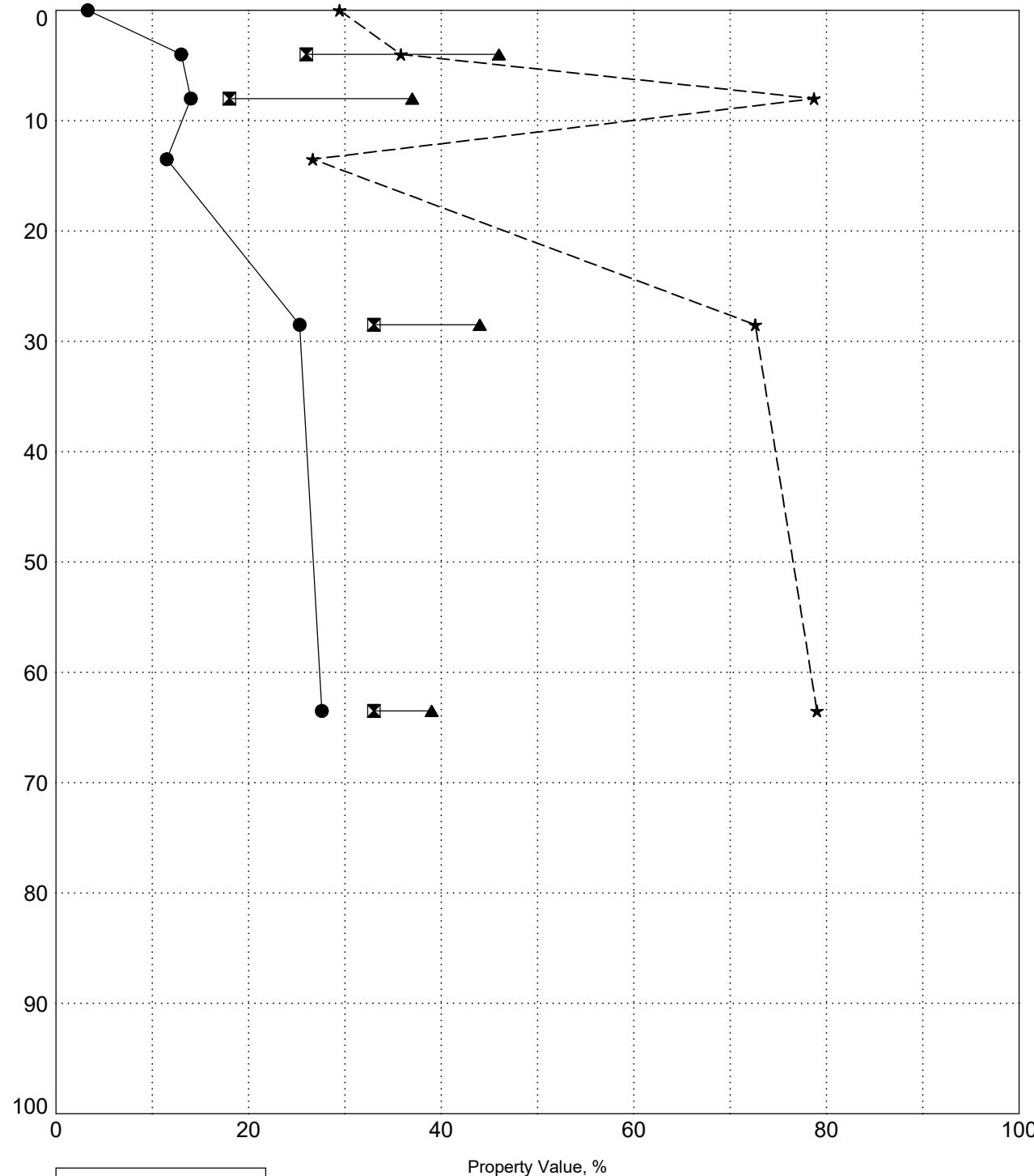
PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING IB- 7C

SURFACE ELEVATION: 460.9



LEGEND	
●	Water Content
◻	Plastic Limit
▲	Liquid Limit
★	Fines

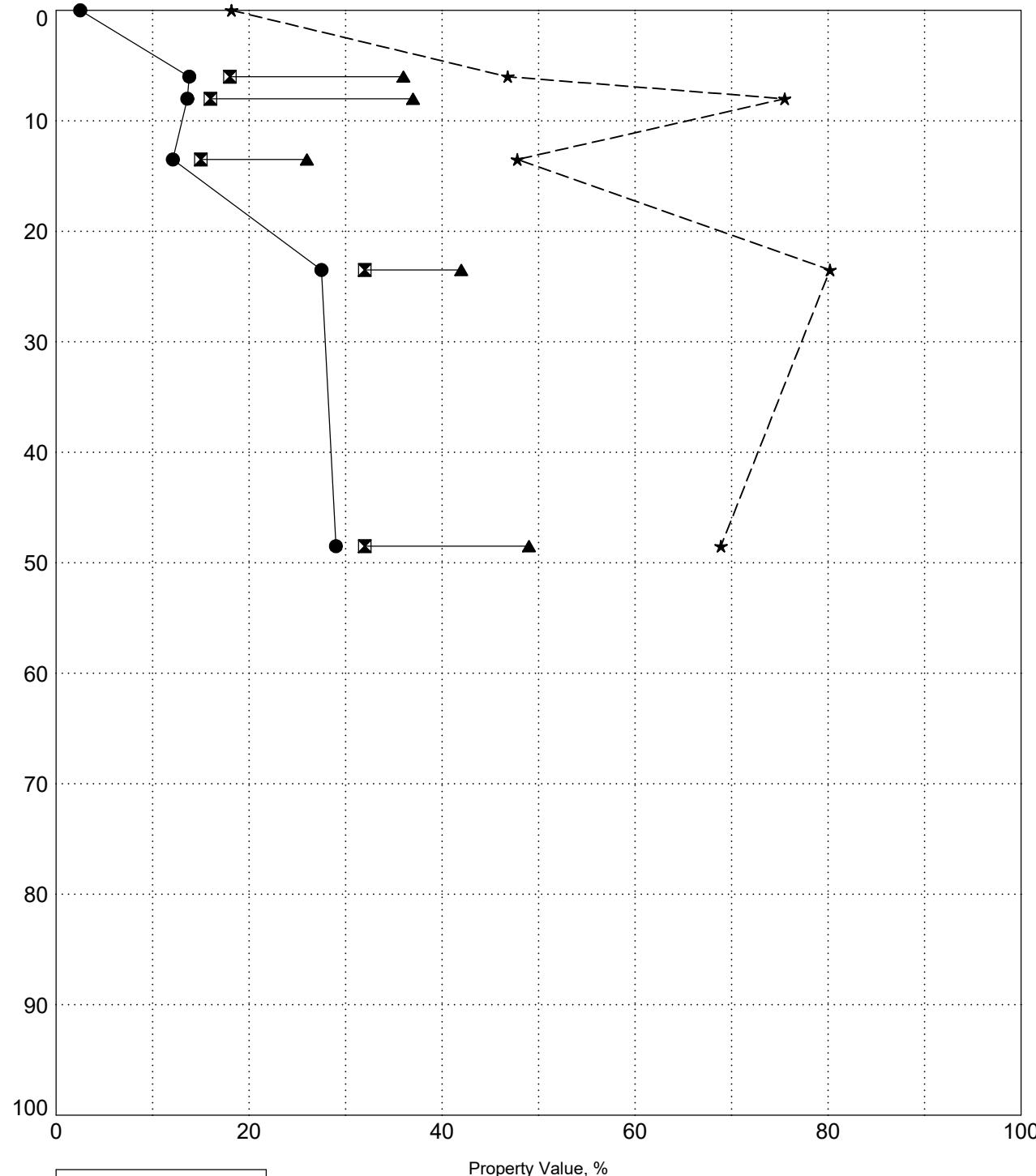
PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING IB- 8C

SURFACE ELEVATION: 464.0



LEGEND	
●	Water Content
◻	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

PROJECT ID P042443 (S&ME 23610178A)

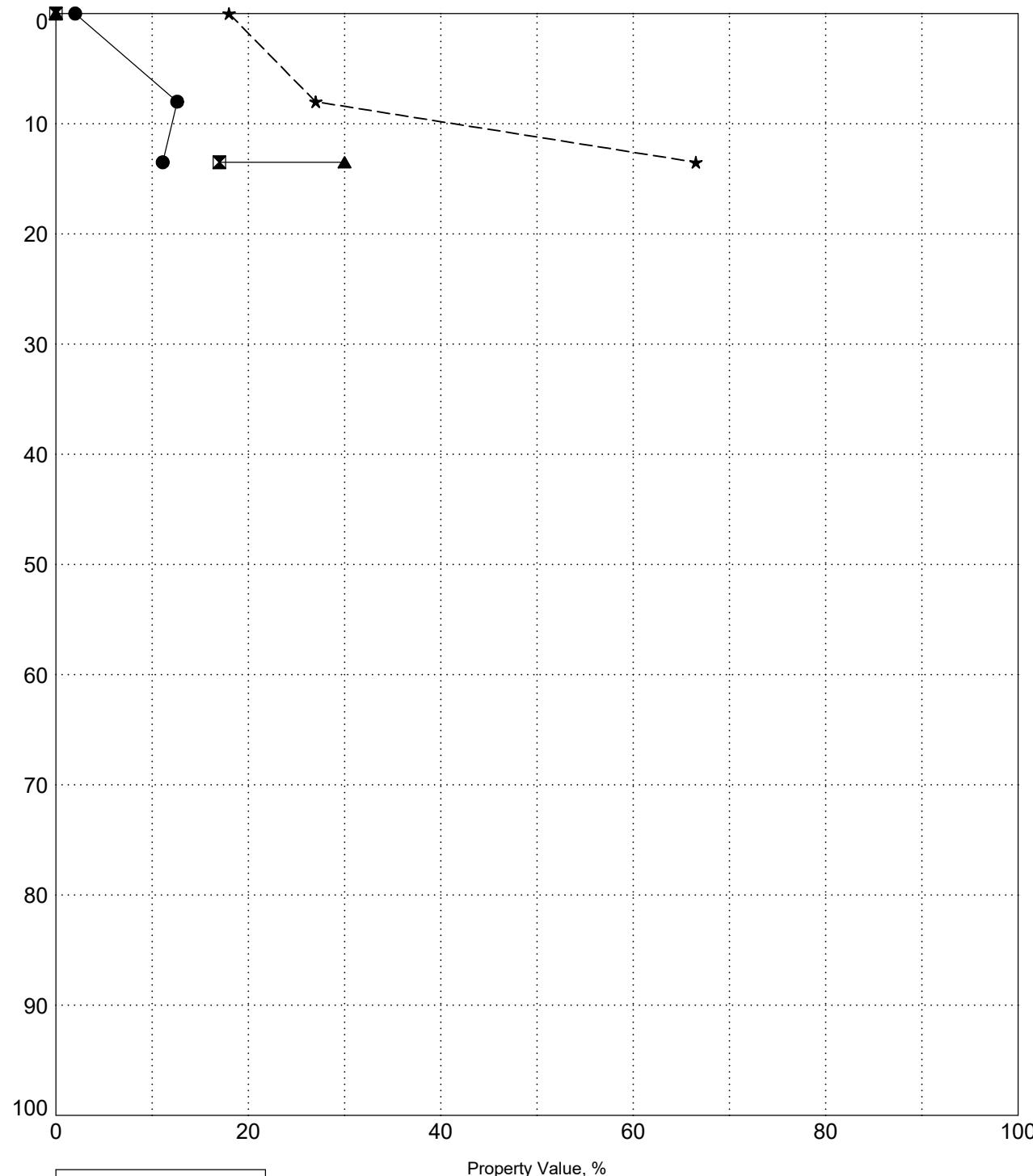
PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING IB- 9C

SURFACE ELEVATION: 464.9

INDEX PROPS 23610178A CONNECTOR BRIDGE OVER I-77.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 1/12/24



LEGEND	
●	Water Content
■	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

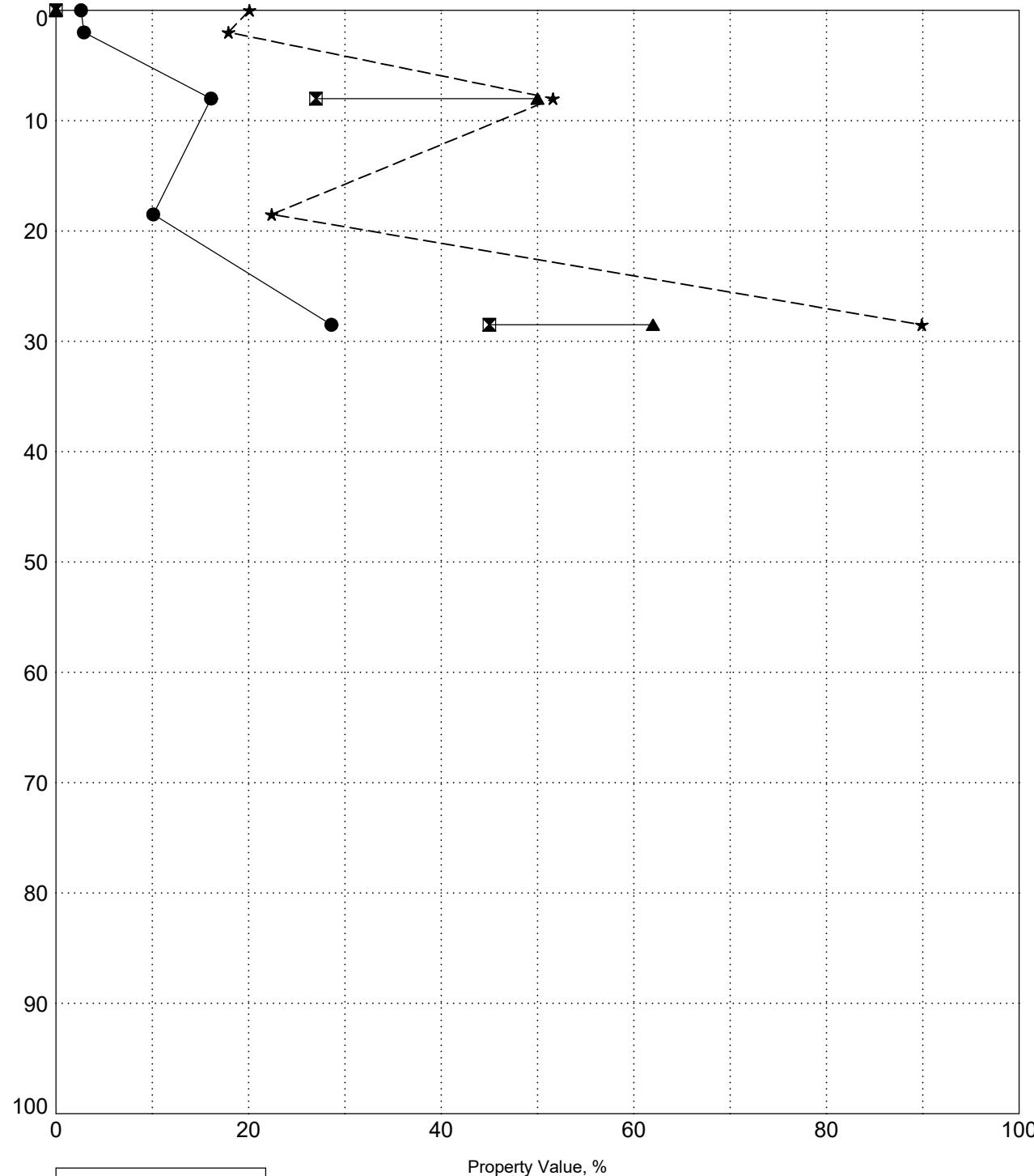
PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING IB-10C

SURFACE ELEVATION: 465.7



LEGEND	
●	Water Content
◻	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

PROJECT ID P042443 (S&ME 23610178A)

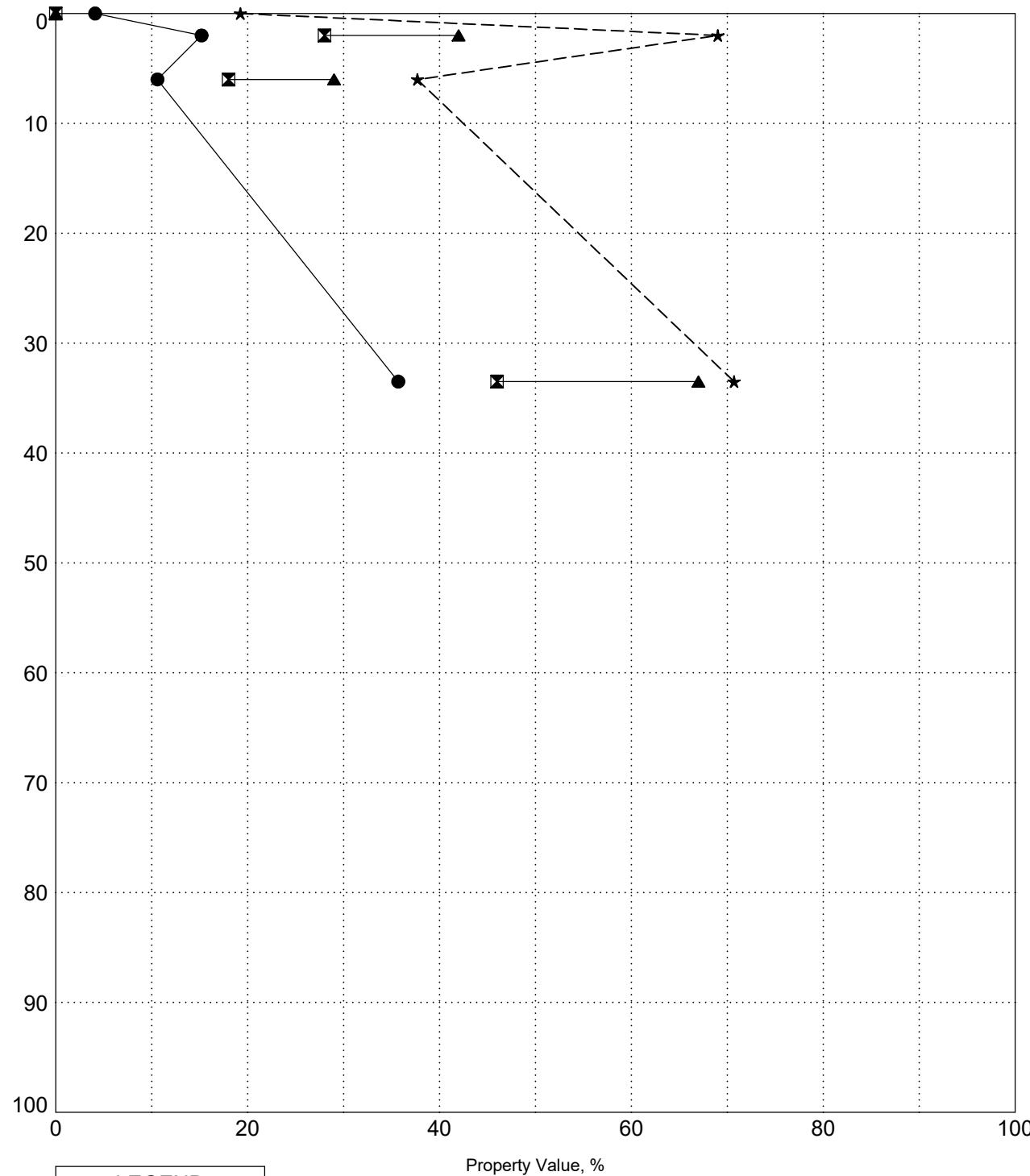
PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

SURFACE ELEVATION: 455.9

BORING IB-11C

INDEX PROPS 23610178A CONNECTOR BRIDGE OVER I-77.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 1/12/24



LEGEND	
●	Water Content
■	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

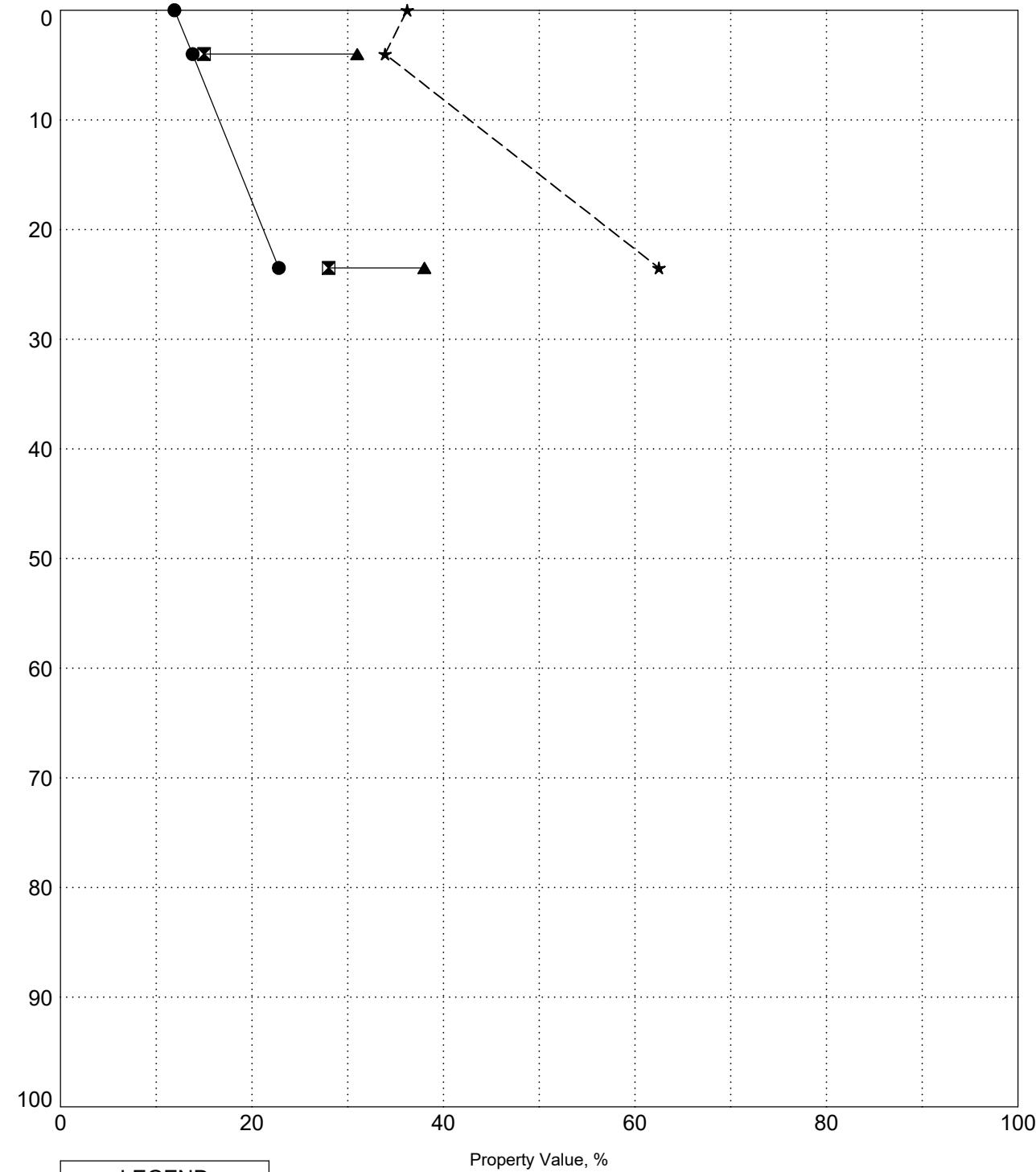
PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

SURFACE ELEVATION: 452.2

BORING W-1



LEGEND	
●	Water Content
◻	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

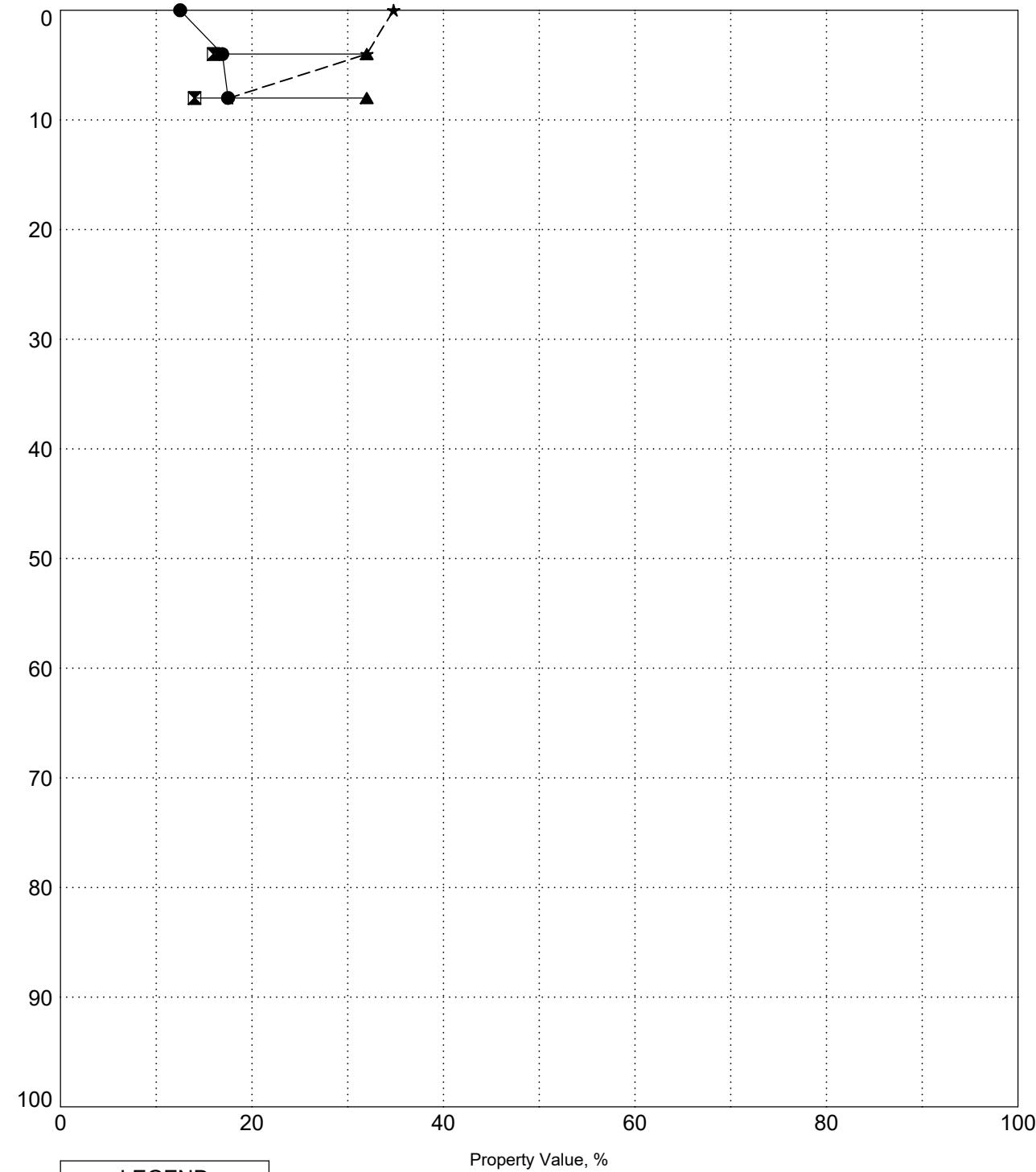
PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

SURFACE ELEVATION: 451.8

BORING W-2



LEGEND	
●	Water Content
◻	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

PROJECT ID P042443 (S&ME 23610178A)

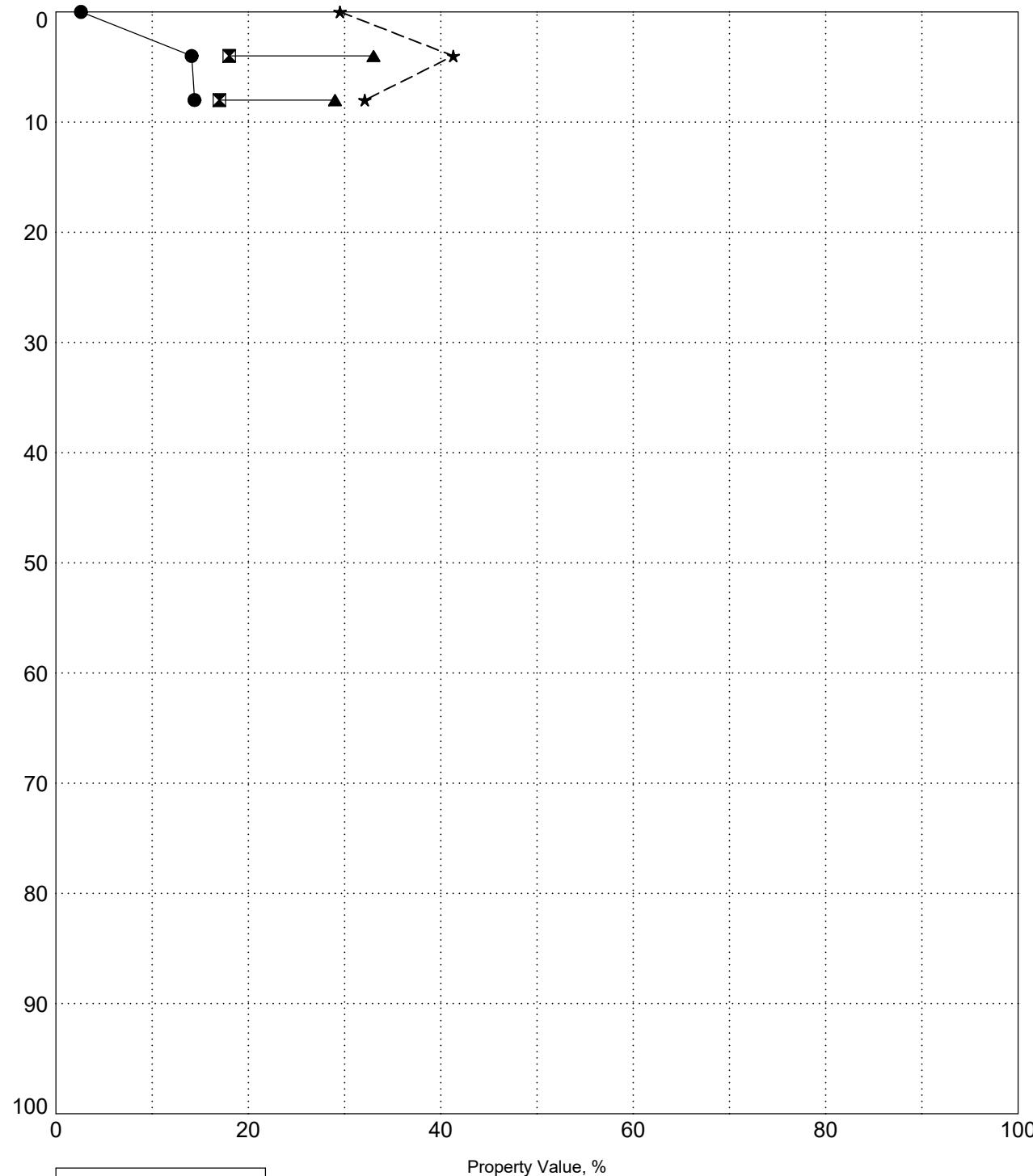
PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

SURFACE ELEVATION: 458.1

BORING W-3

INDEX PROPS 23610178A CONNECTOR BRIDGE OVER I-77.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 1/12/24



LEGEND	
●	Water Content
◻	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

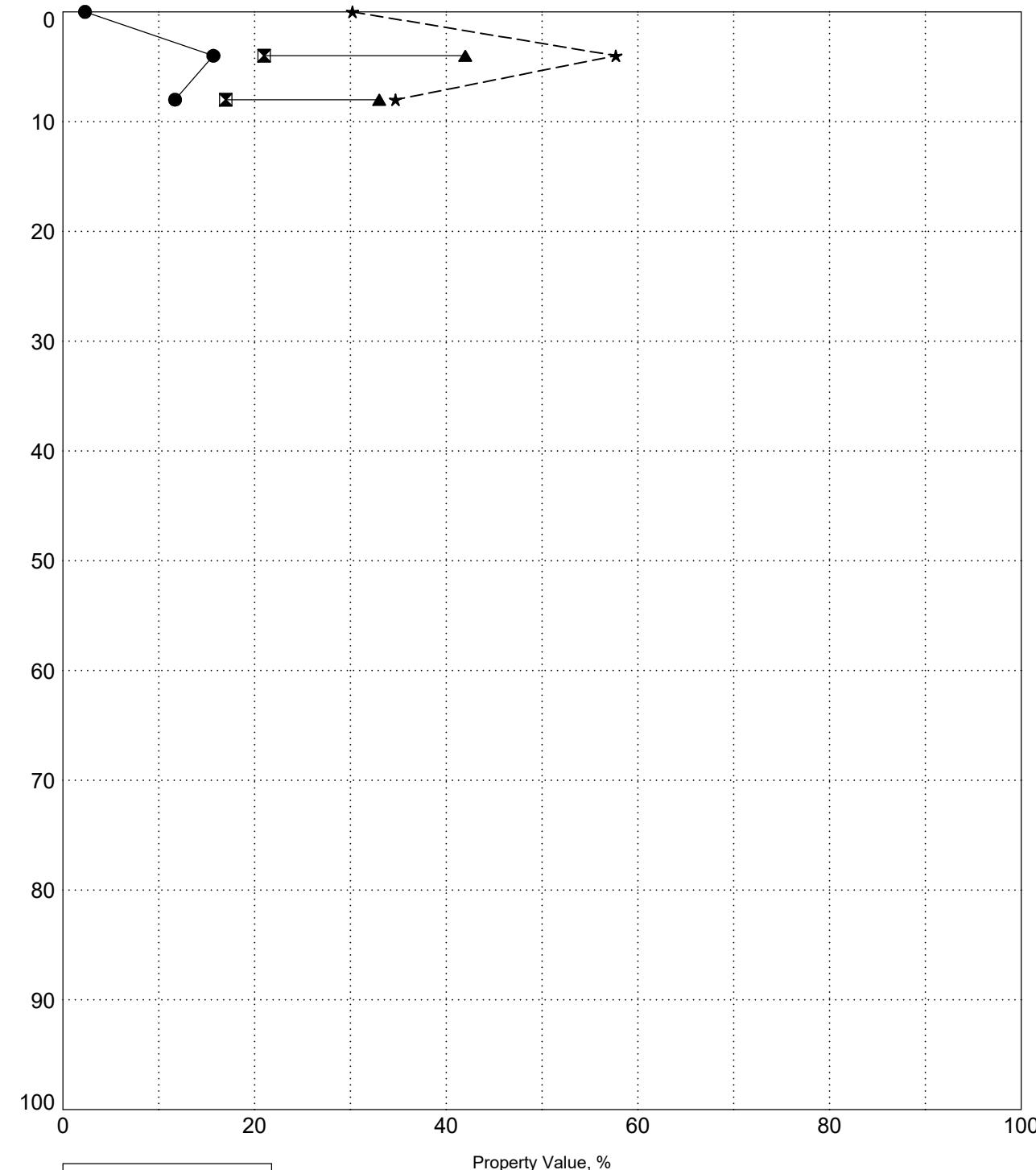
PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING W-4

SURFACE ELEVATION: 459.1



LEGEND	
●	Water Content
■	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

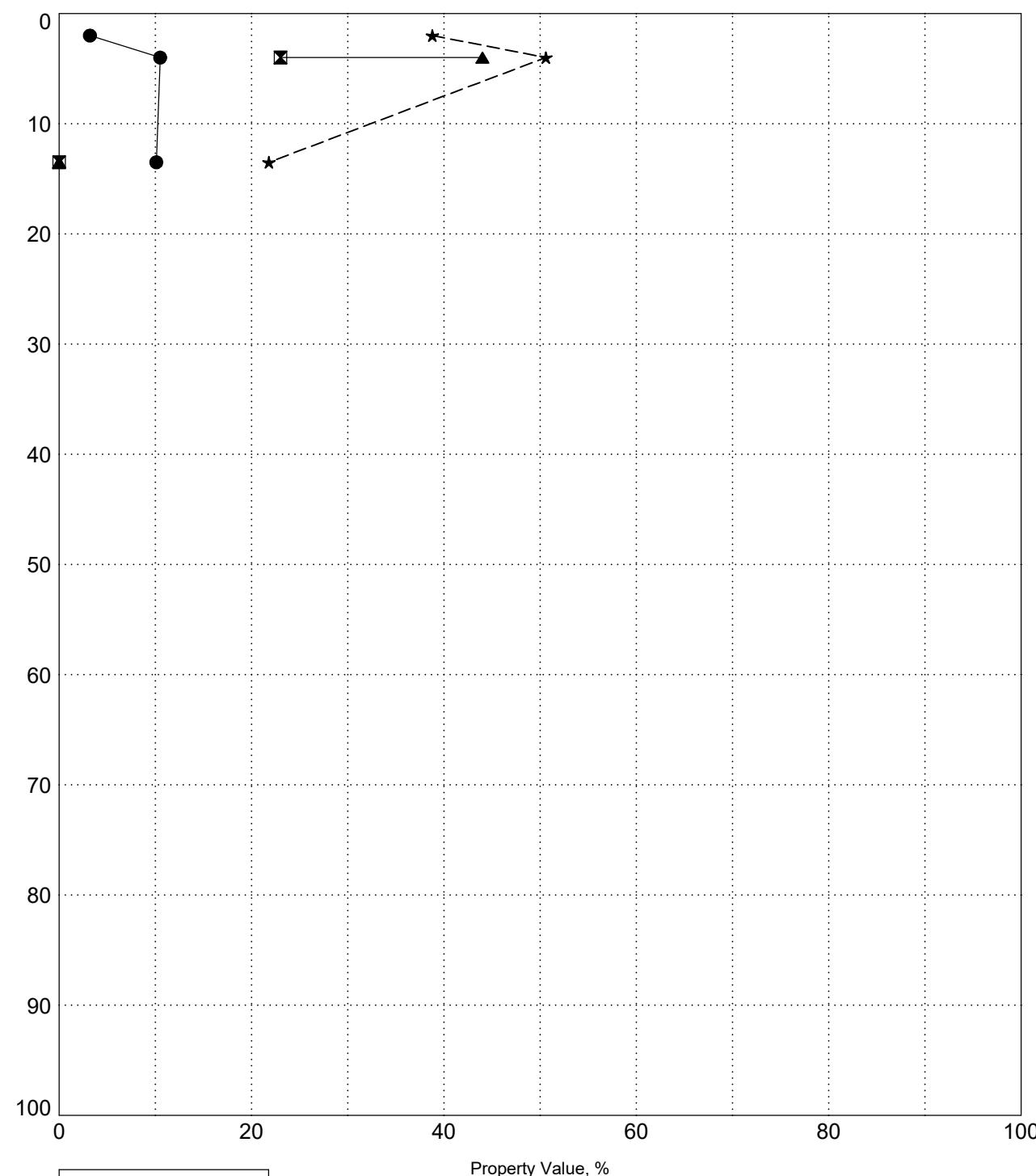
PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

SURFACE ELEVATION: 460.9

BORING W-5



LEGEND	
●	Water Content
◻	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

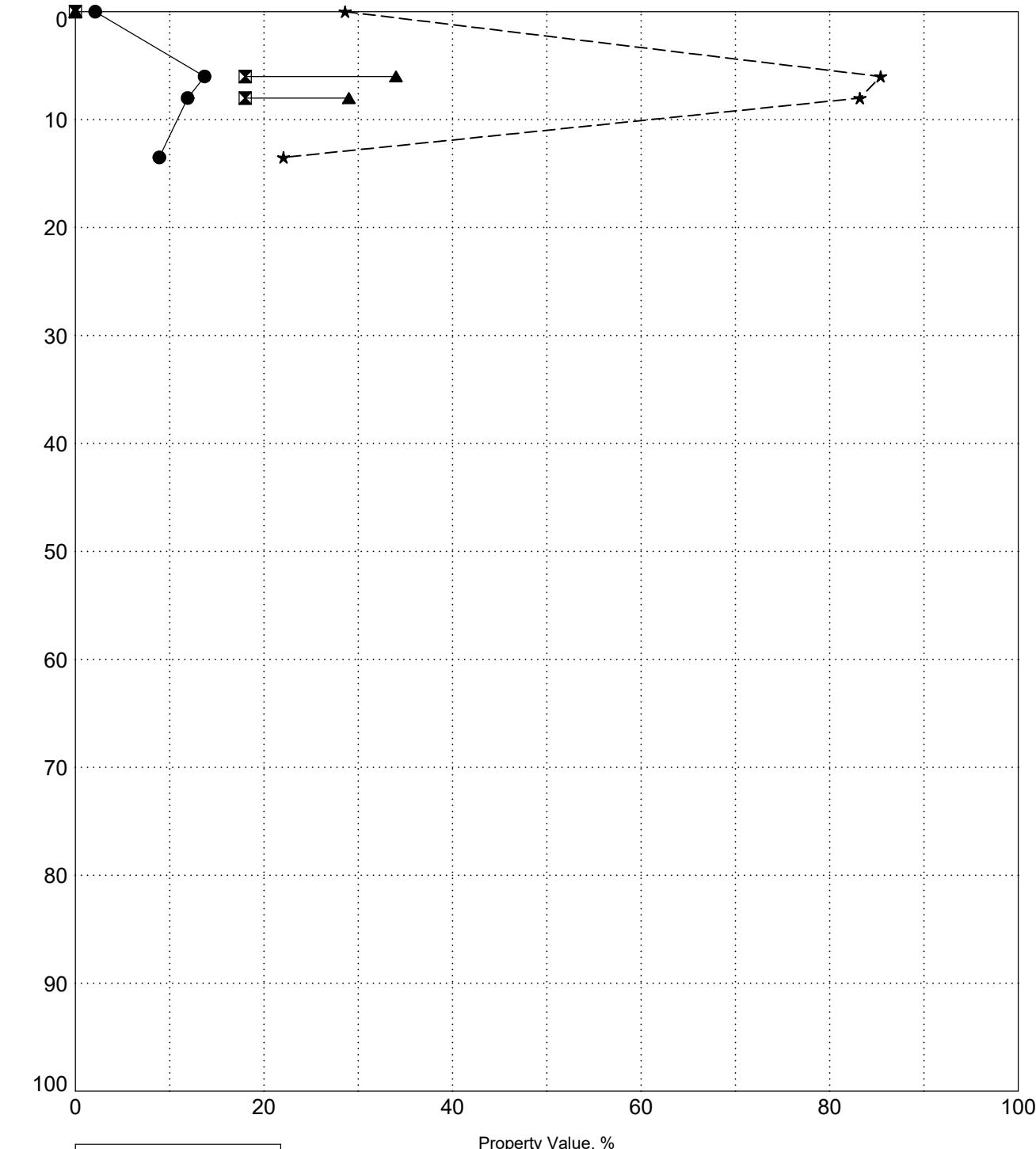
PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

BORING W-6

SURFACE ELEVATION: 460.9



LEGEND	
●	Water Content
■	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

PROJECT ID P042443 (S&ME 23610178A)

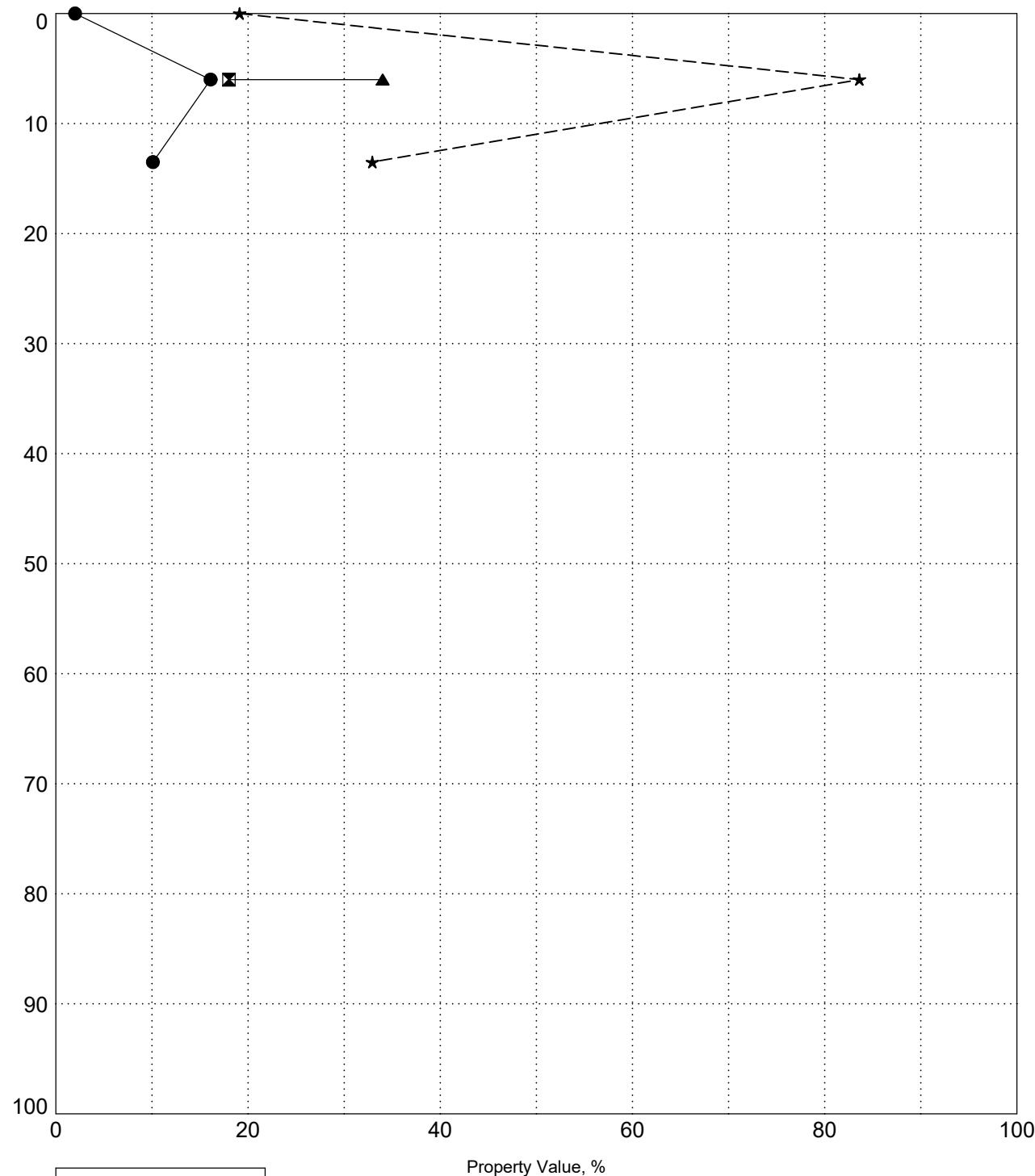
PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

SURFACE ELEVATION: 461.7

BORING W-7

INDEX PROPS 23610178A CONNECTOR BRIDGE OVER I-77.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 1/12/24



LEGEND	
●	Water Content
✖	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

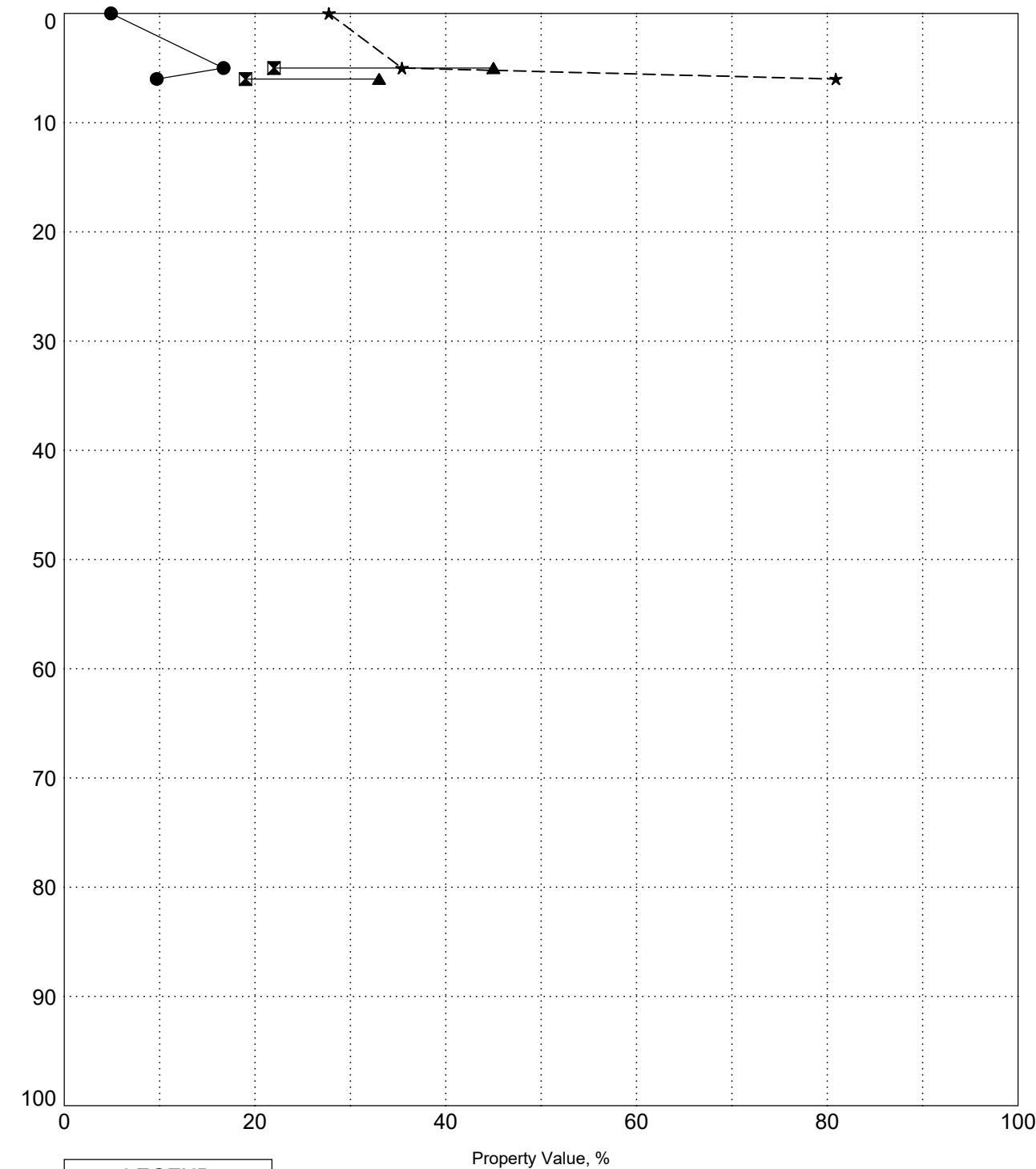
PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland

SURFACE ELEVATION: 461.6

BORING W-8



LEGEND	
●	Water Content
■	Plastic Limit
▲	Liquid Limit
★	Fines

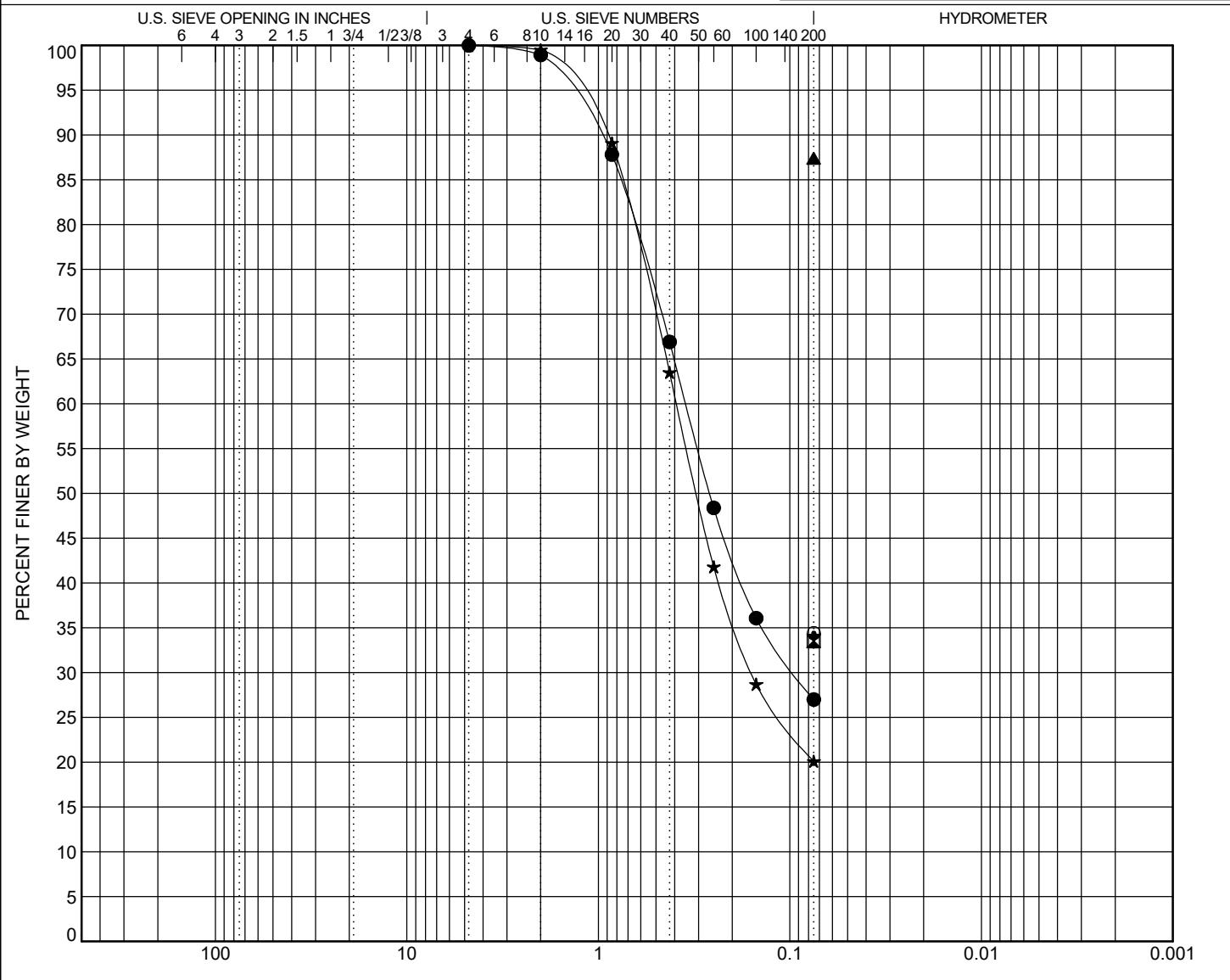


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



BOREHOLE	DEPTH	Classification					LL	PL	PI	Cc	Cu
● EB-1C	0.0	Silty SAND (SM)									
☒ EB-1C	4.0	Clayey SAND (SC)									
▲ EB-1C	23.5	SILT with Sand (ML)					44	33	11		
★ EB-2C	0.0	Silty SAND (SM)									
○ EB-2C	4.0	Clayey SAND (SC)					40	22	18		
BOREHOLE	DEPTH	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay		
● EB-1C	0.0	4.75	0.349	0.094		0.0	73.0		27.0		
☒ EB-1C	4.0	0.075							33.5		
▲ EB-1C	23.5	0.075							87.4		
★ EB-2C	0.0	4.75	0.39	0.158		0.0	79.9		20.1		
○ EB-2C	4.0	0.075							34.4		

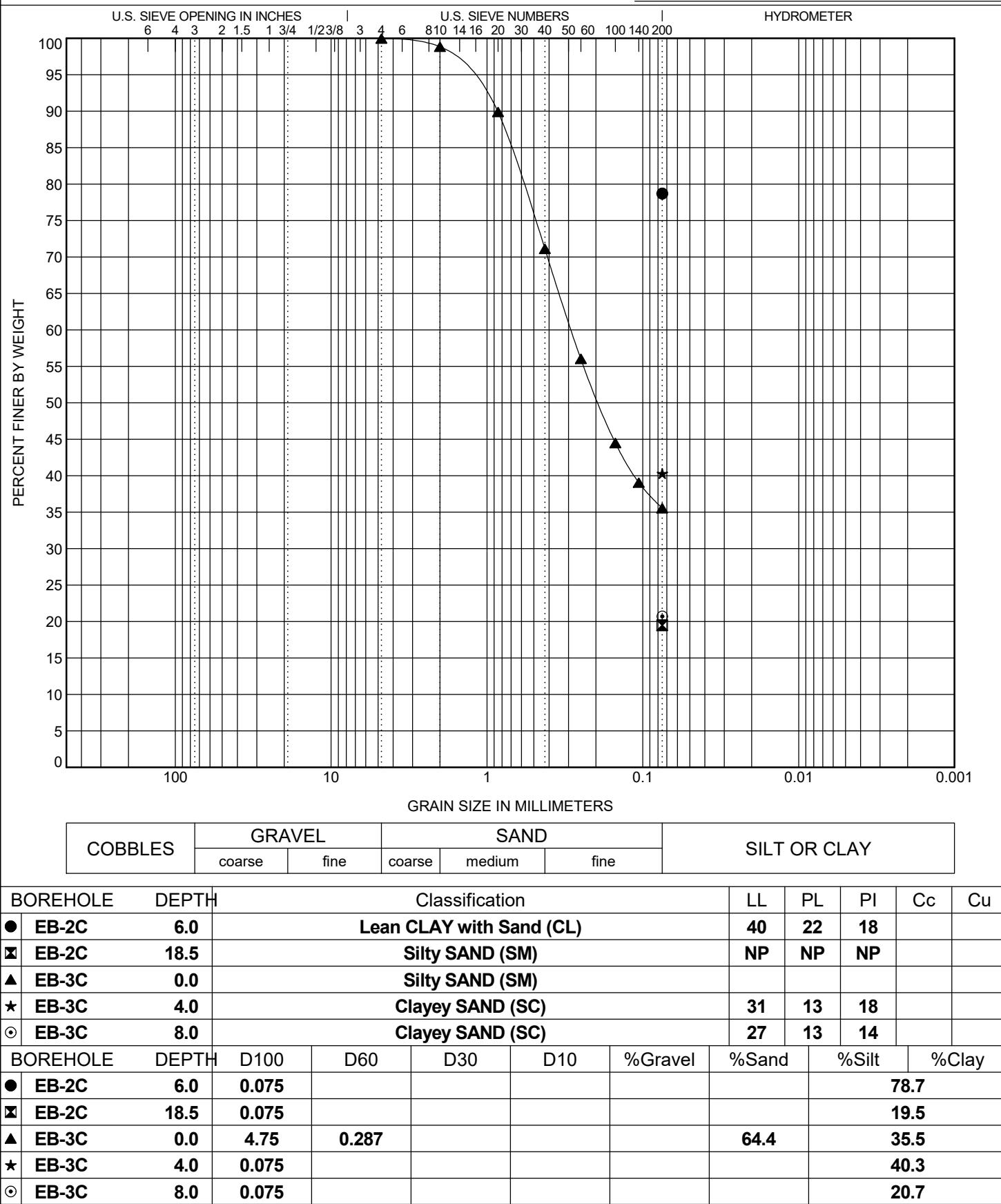


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



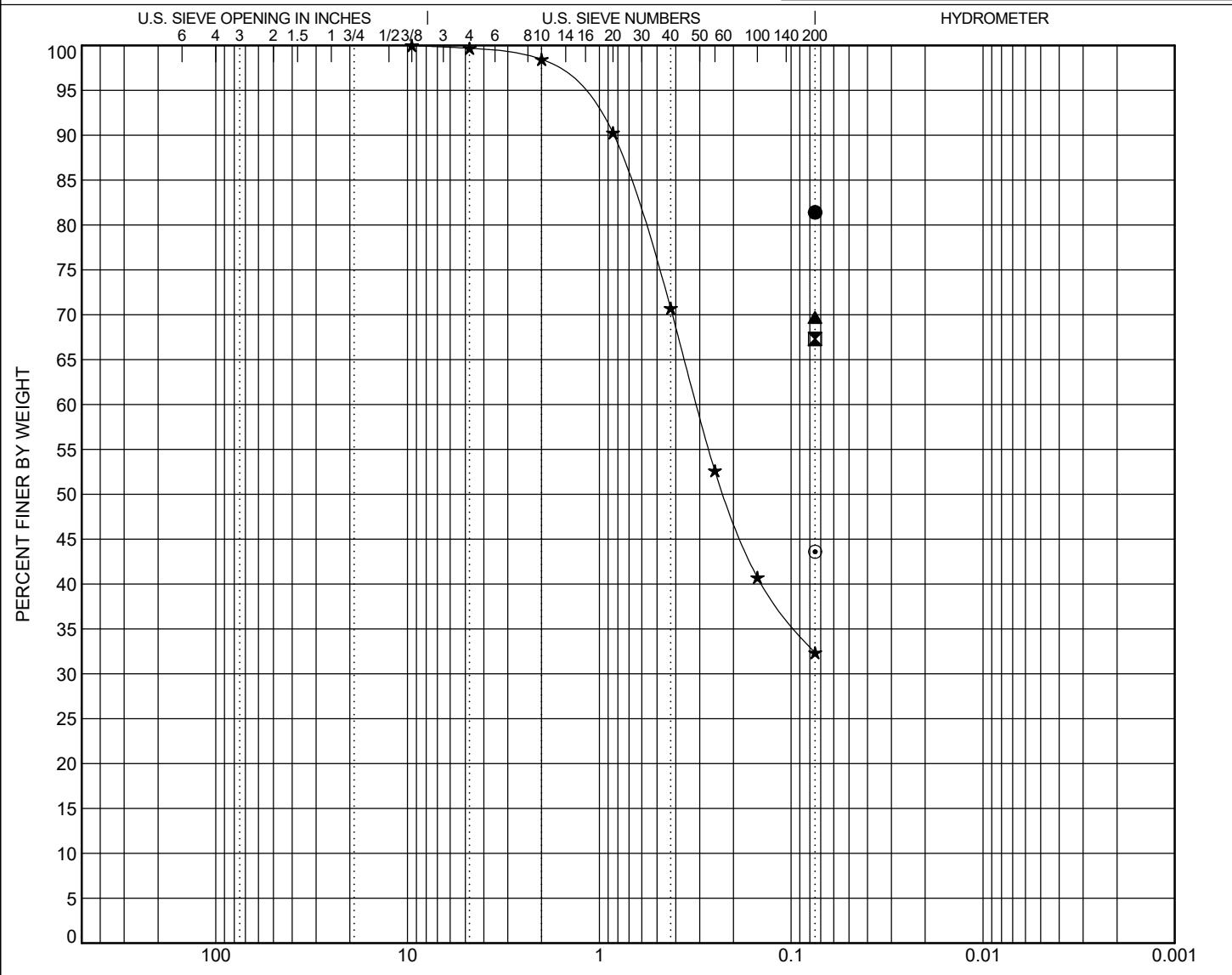


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

BOREHOLE	DEPTH	Classification					LL	PL	PI	Cc	Cu
● EB-3C	33.5	SILT with Sand (ML)					35	29	6		
☒ EB-3C	78.5	Sandy SILT (ML)					35	31	4		
▲ EB-3C	93.5	Sandy SILT (ML)					38	28	10		
★ EB-4C	0.0	Silty SAND (SM)									
○ EB-4C	6.0	Silty SAND (SM)					37	26	11		
BOREHOLE	DEPTH	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay		
● EB-3C	33.5	0.075								81.4	
☒ EB-3C	78.5	0.075								67.3	
▲ EB-3C	93.5	0.075								69.7	
★ EB-4C	0.0	9.5	0.31			0.3	67.3			32.4	
○ EB-4C	6.0	0.075								43.6	

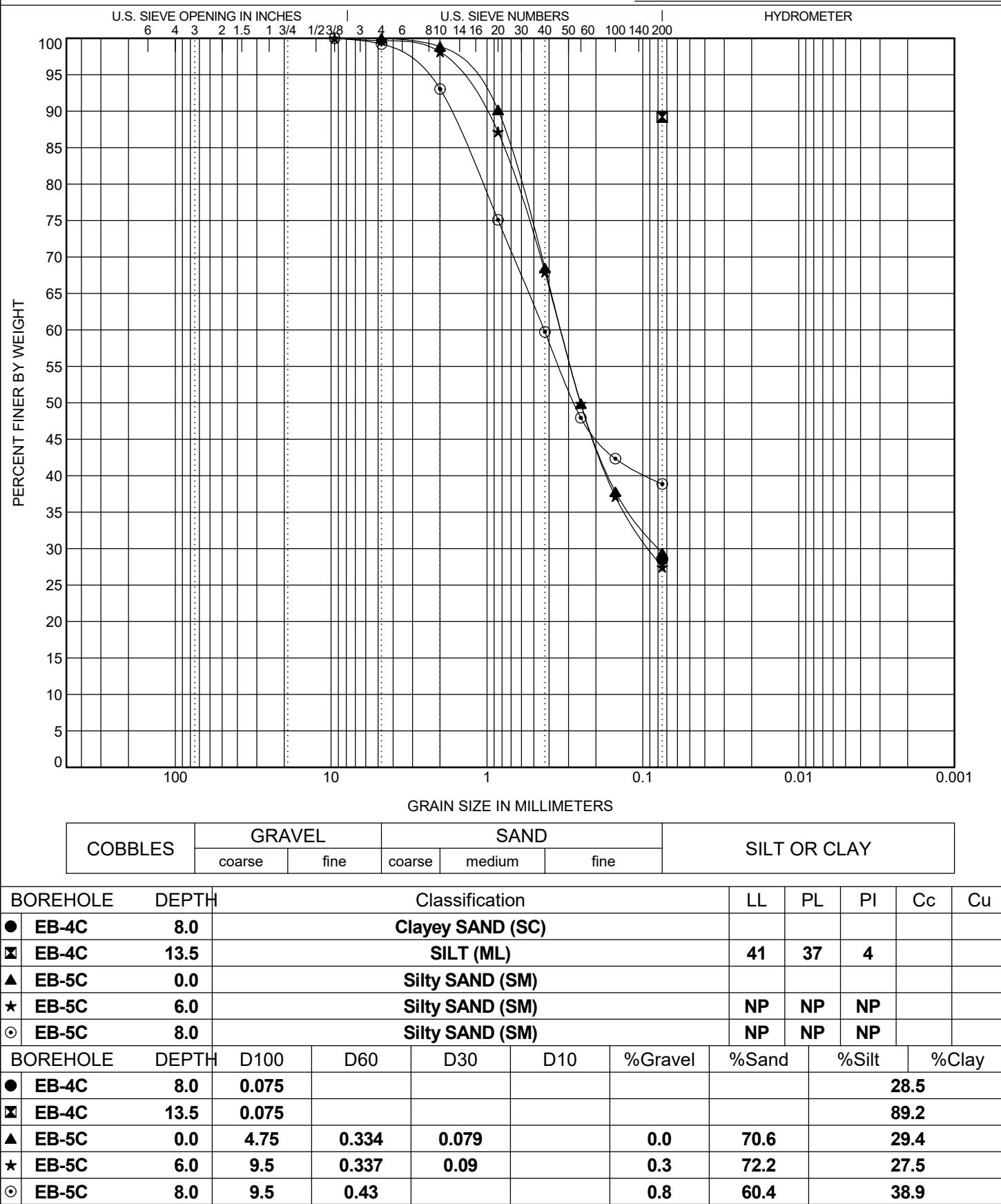


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



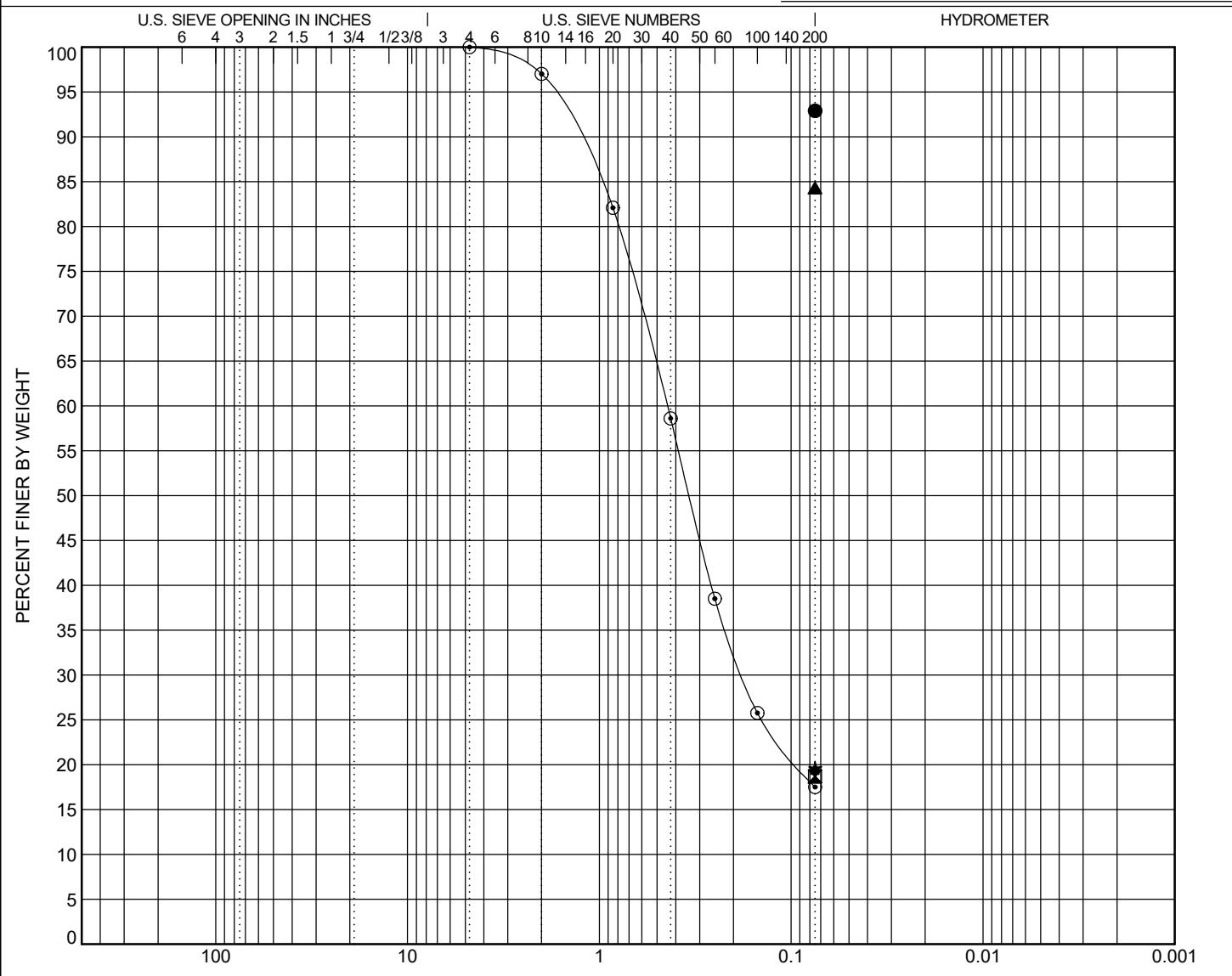


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



BOREHOLE	DEPTH	Classification					LL	PL	PI	Cc	Cu
● EB-5C	23.5	SILT (ML)					49	41	8		
☒ EB-6C	0.0	Silty SAND (SM)					NP	NP	NP		
▲ EB-6C	4.0	Lean CLAY with Sand (CL)					42	23	19		
★ EB-6C	13.5	Silty, Clayey SAND (SC-SM)					24	18	6		
○ EM-1	0.0	Silty SAND (SM)									
BOREHOLE	DEPTH	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay		
● EB-5C	23.5	0.075								92.9	
☒ EB-6C	0.0	0.075								18.7	
▲ EB-6C	4.0	0.075								84.3	
★ EB-6C	13.5	0.075								19.6	
○ EM-1	0.0	4.75	0.443	0.178		0.0	82.5			17.5	

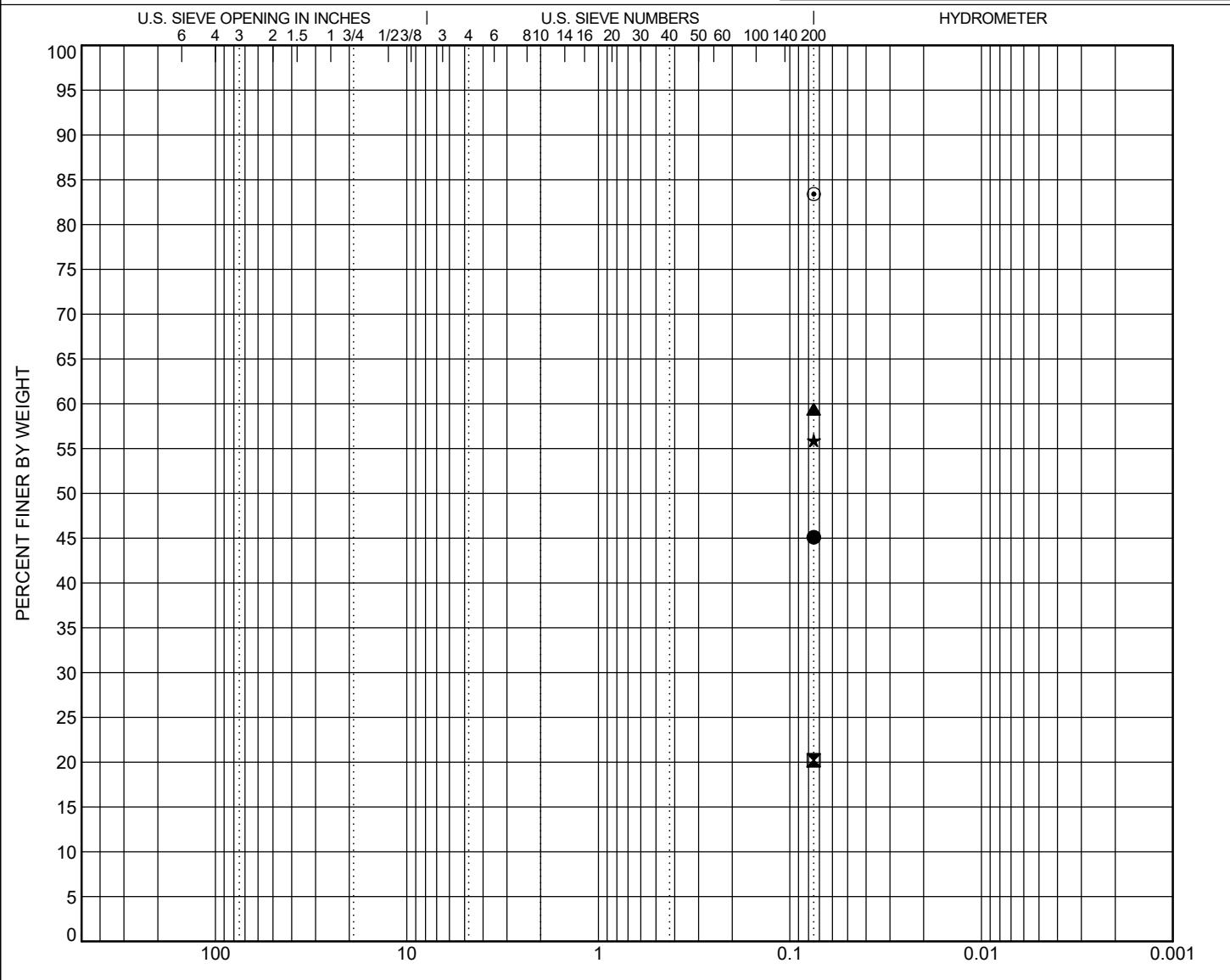


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

BOREHOLE	DEPTH	Classification					LL	PL	PI	Cc	Cu
● IB- 1C	0.0	Clayey SAND (SC)					34	16	18		
■ IB- 1C	6.0	Clayey SAND (SC)					36	18	18		
▲ IB- 1C	18.5	Sandy Elastic SILT (MH)					58	38	20		
★ IB- 2C	2.0	Sandy Lean CLAY (CL)					38	18	20		
◎ IB- 2C	13.5	SILT with Sand (ML)					46	30	16		
BOREHOLE	DEPTH	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay		
● IB- 1C	0.0	0.075								45.1	
■ IB- 1C	6.0	0.075								20.2	
▲ IB- 1C	18.5	0.075								59.4	
★ IB- 2C	2.0	0.075								55.9	
◎ IB- 2C	13.5	0.075								83.4	

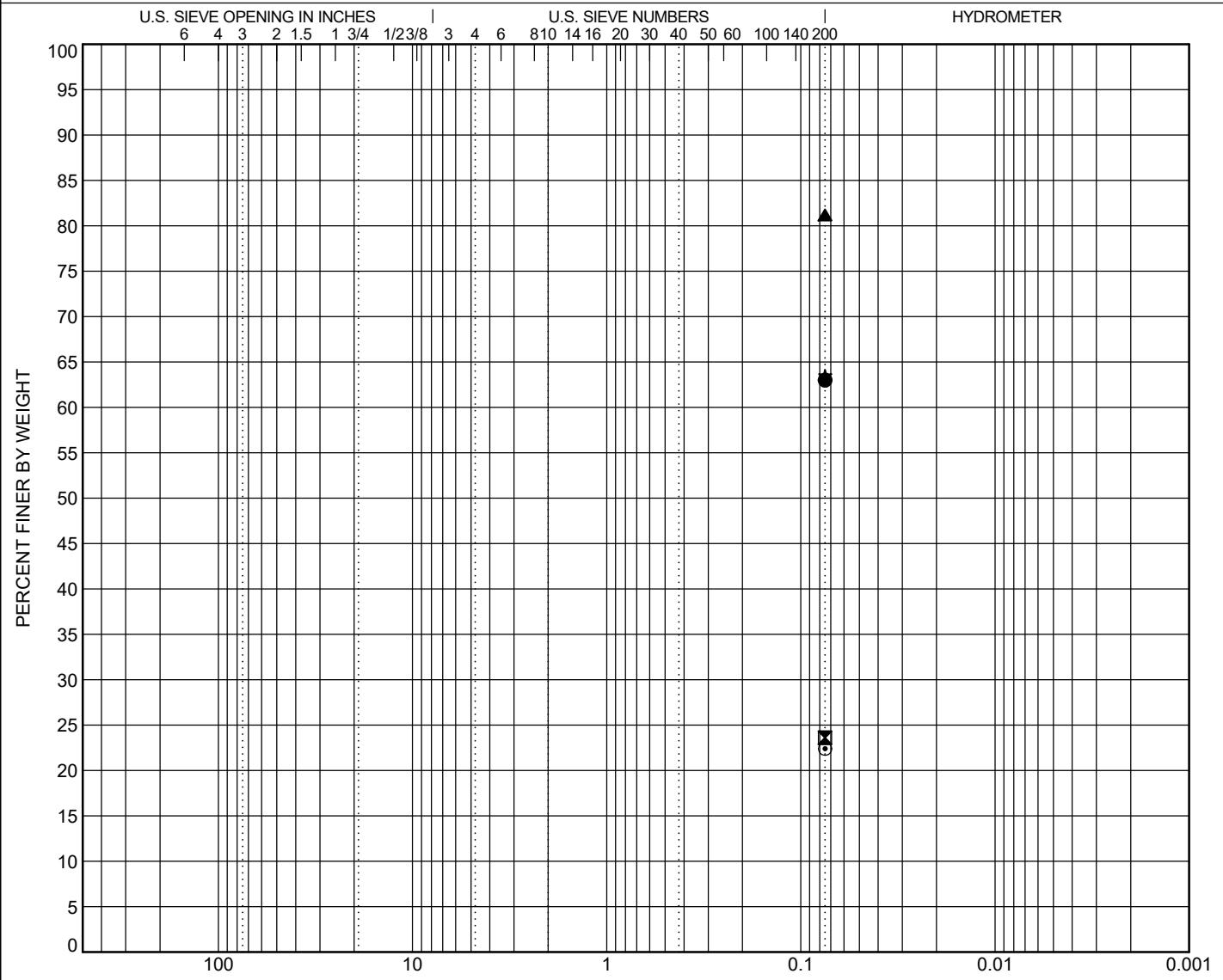


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



GRAIN SIZE IN MILLIMETERS						
COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

BOREHOLE	DEPTH	Classification					LL	PL	PI	Cc	Cu
● IB- 3C	0.0	Sandy Lean CLAY (CL)					32	18	14		
■ IB- 3C	8.0	Silty SAND (SM)					NP	NP	NP		
▲ IB- 3C	13.5	SILT with Sand (ML)					46	36	10		
★ IB- 4C	2.0	Sandy Lean CLAY (CL)					37	19	18		
◎ IB- 4C	8.0	Silty SAND (SM)					NP	NP	NP		
BOREHOLE	DEPTH	D100	D60	D30	D10	%Gravel	%Sand	%Silt		%Clay	
● IB- 3C	0.0	0.075								63.0	
■ IB- 3C	8.0	0.075								23.6	
▲ IB- 3C	13.5	0.075								81.2	
★ IB- 4C	2.0	0.075								63.5	
◎ IB- 4C	8.0	0.075								22.4	

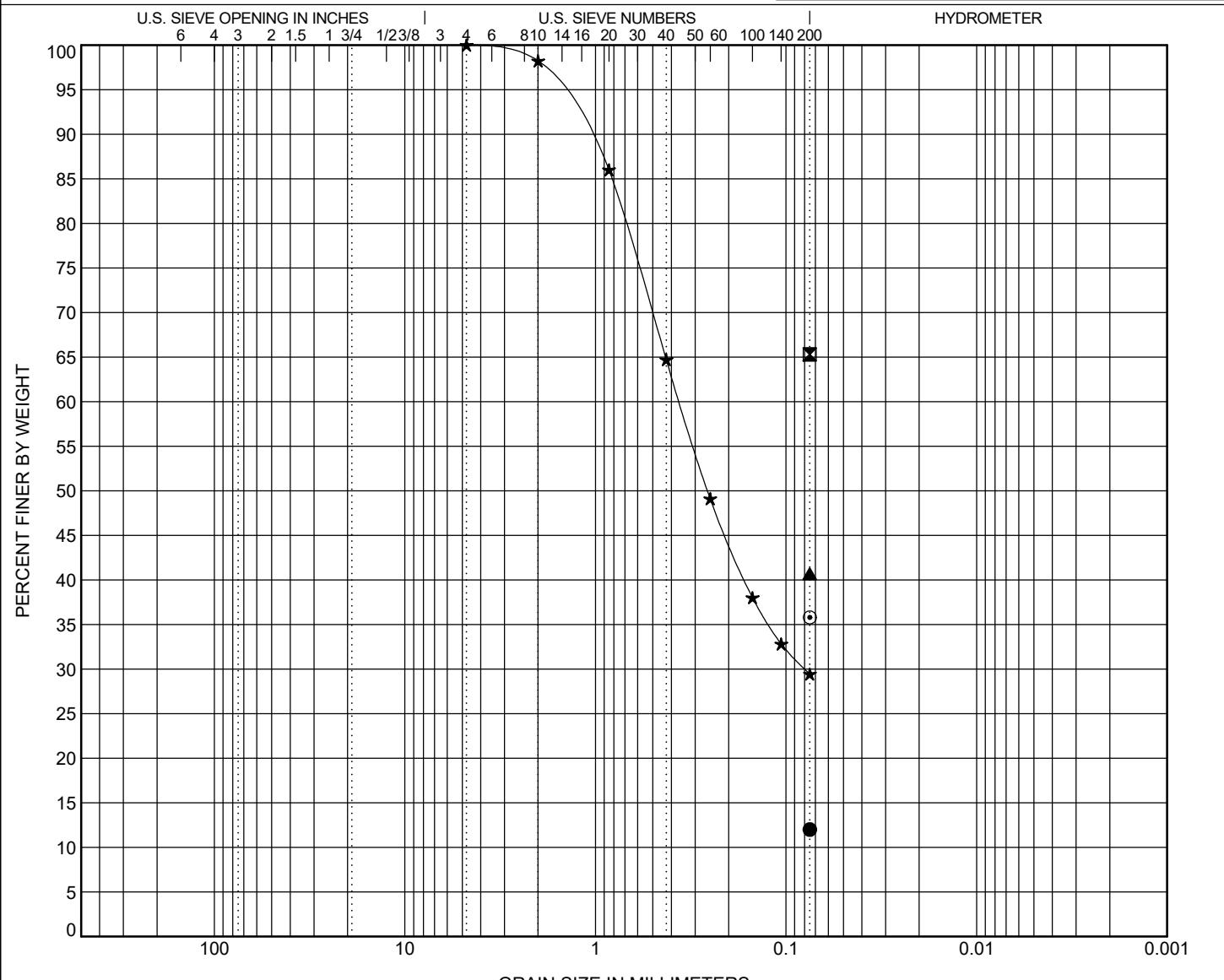


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



BOREHOLE	DEPTH	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
● IB- 6C	0.0	0.075							12.0
☒ IB- 6C	2.0	0.075							65.3
▲ IB- 6C	6.0	0.075							40.7
★ IB- 7C	0.0	4.75	0.362	0.079		0.0	70.6		29.4
○ IB- 7C	4.0	0.075							35.8

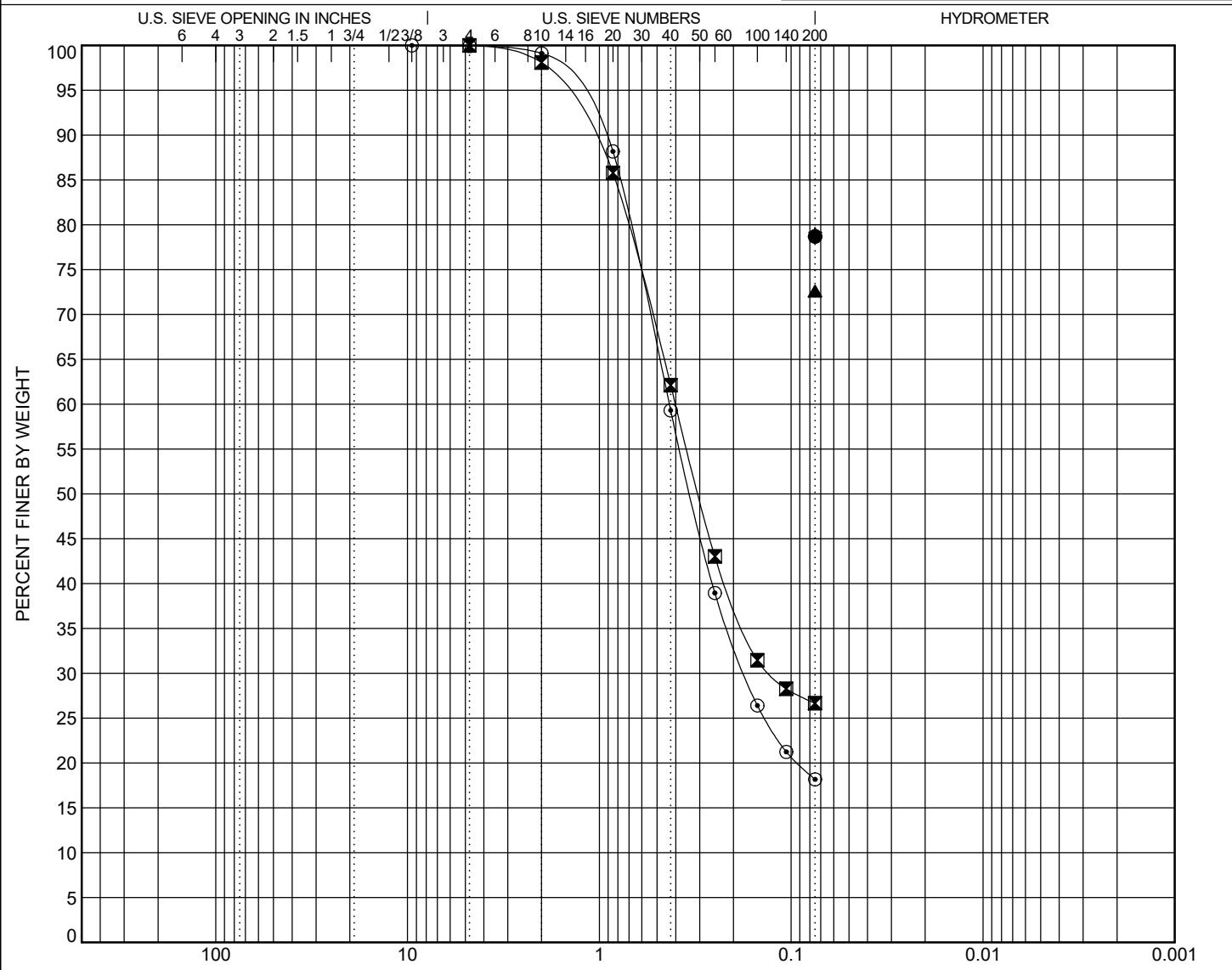


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			
● IB- 7C 8.0			Classification			LL	PL	PI

BOREHOLE	DEPTH	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
● IB- 7C	8.0	0.075							78.7
■ IB- 7C	13.5	4.75	0.401	0.128		0.0	73.3		26.7
▲ IB- 7C	28.5	0.075							72.6
★ IB- 7C	63.5	0.075							79.0
○ IB- 8C	0.0	9.5	0.432	0.174		0.1	81.8		18.2

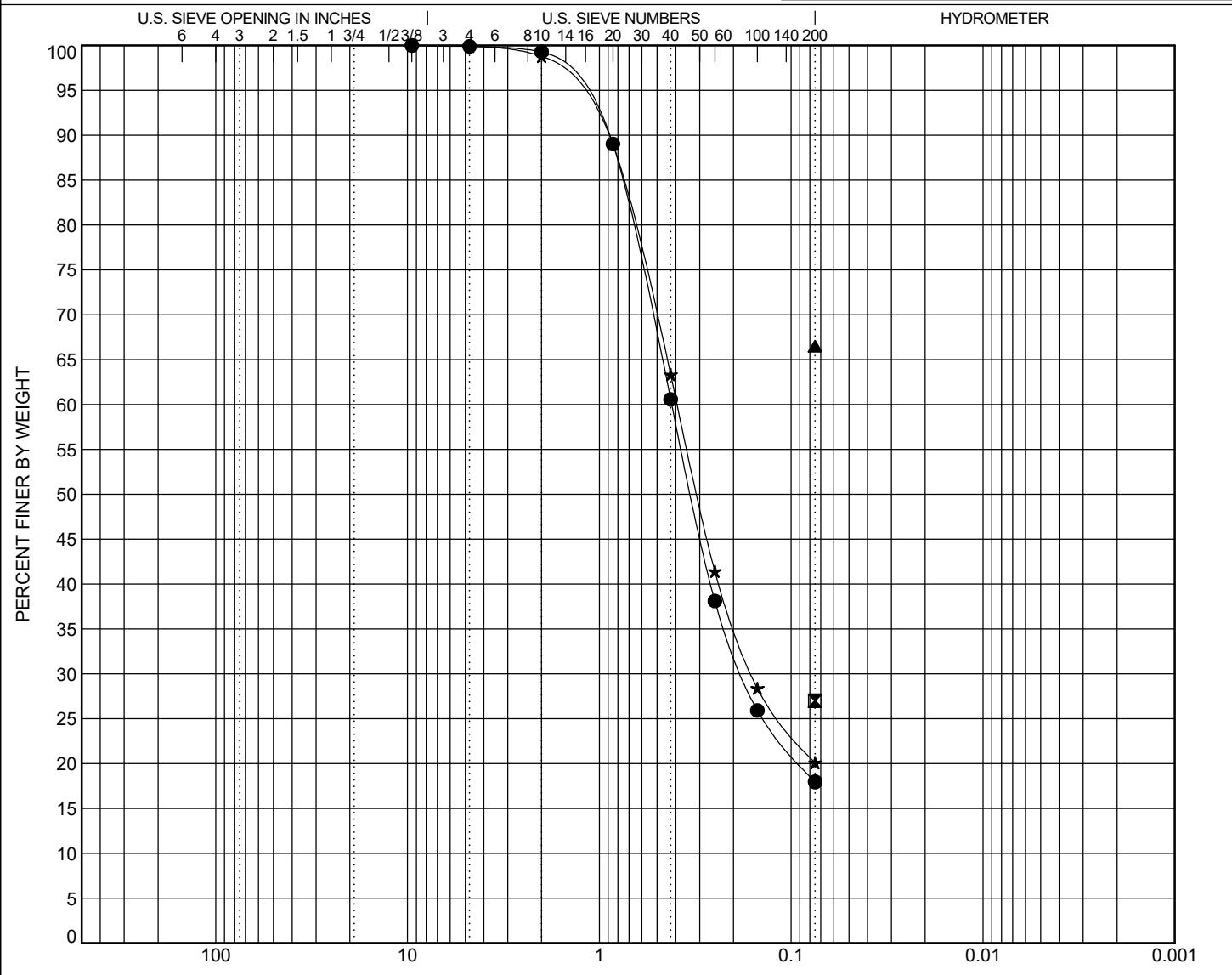


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



BOREHOLE	DEPTH	Classification					LL	PL	PI	Cc	Cu
●	IB-9C 0.0	Silty SAND (SM)					NP	NP	NP		
☒	IB-9C 8.0	Clayey SAND (SC)									
▲	IB-9C 13.5	Sandy Lean CLAY (CL)					30	17	13		
★	IB-10C 0.0	Silty SAND (SM)					NP	NP	NP		
○	IB-10C 2.0	Silty SAND (SM)									
BOREHOLE	DEPTH	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay		
●	IB-9C 0.0	9.5	0.419	0.178		0.1	81.9		18.0		
☒	IB-9C 8.0	0.075							27.0		
▲	IB-9C 13.5	0.075							66.5		
★	IB-10C 0.0	9.5	0.392	0.16		0.1	79.8		20.1		
○	IB-10C 2.0	0.075							17.9		

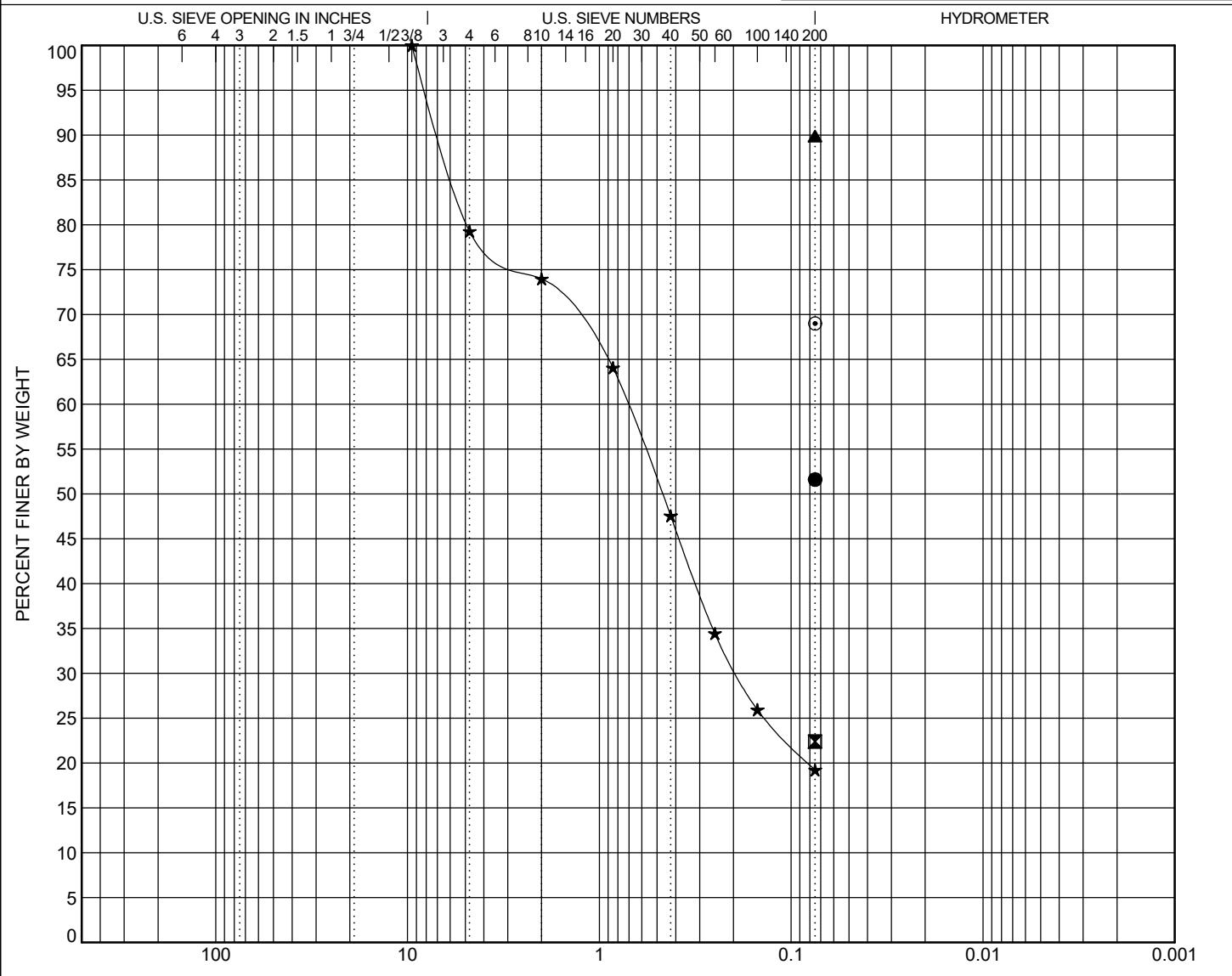


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



GRAIN SIZE 23610178A CONNECTOR BRIDGE OVER I-77 GPJ SCDOT DATA TEMPLATE 01 30 2015 GDT 1/12/24

COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

BOREHOLE	DEPTH	Classification					LL	PL	PI	Cc	Cu
● IB-10C	8.0	Sandy Fat CLAY (CH)					50	27	23		
☒ IB-10C	18.5	Silty SAND (SM)									
▲ IB-10C	28.5	Elastic SILT (MH)					62	45	17		
★ IB-11C	0.0	Silty SAND (SM)					NP	NP	NP		
○ IB-11C	2.0	Sandy SILT (ML)					42	28	14		

BOREHOLE	DEPTH	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
● IB-10C	8.0	0.075							51.6
☒ IB-10C	18.5	0.075							22.4
▲ IB-10C	28.5	0.075							89.9
★ IB-11C	0.0	9.5	0.716	0.191		20.7	60.0		19.2
○ IB-11C	2.0	0.075							69.0

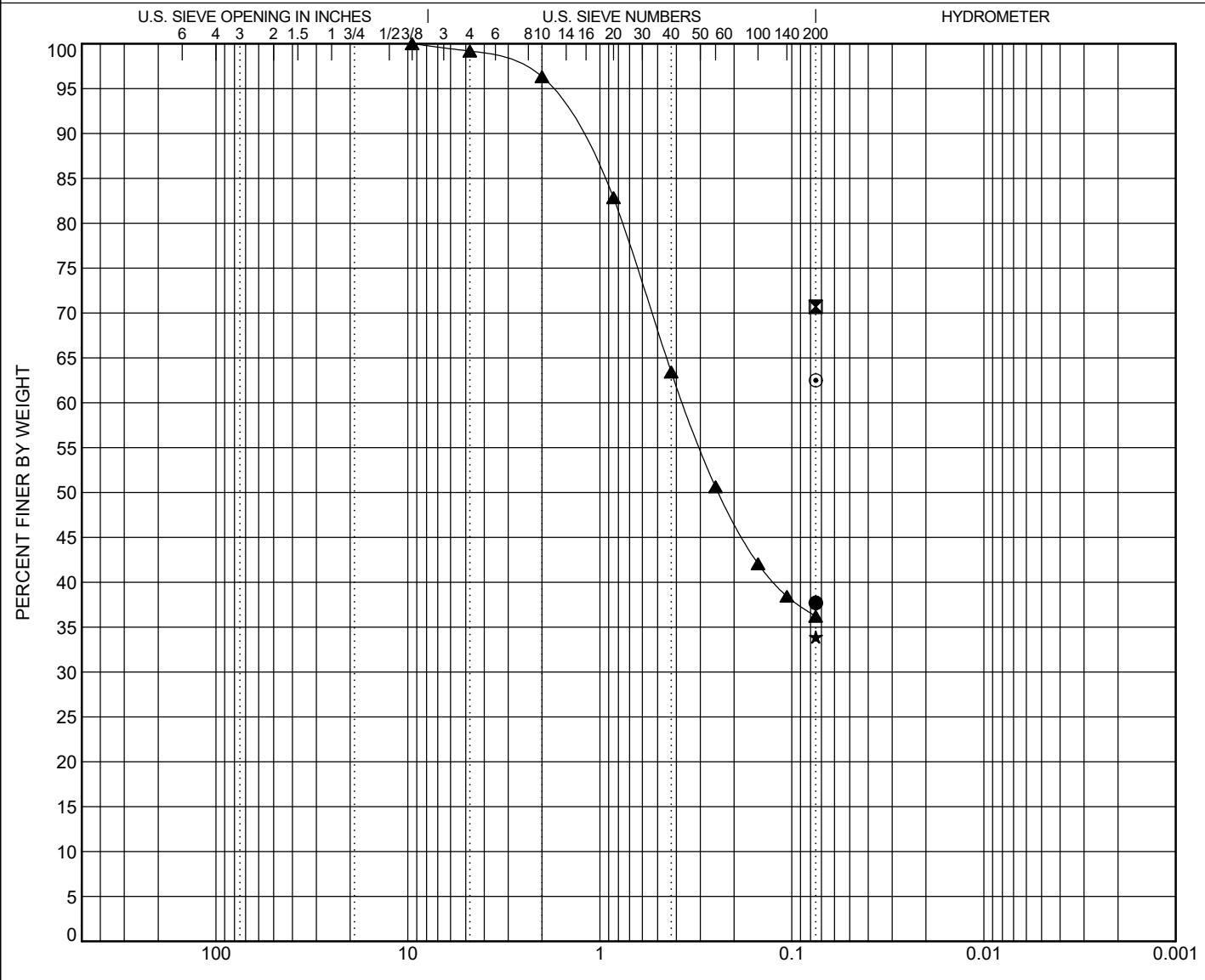


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



GRAIN SIZE IN MILLIMETERS						SILT OR CLAY	
COBBLES	GRAVEL		SAND				
	coarse	fine	coarse	medium	fine		

BOREHOLE	DEPTH	Classification					LL	PL	PI	Cc	Cu
● IB-11C	6.0	Clayey SAND (SC)					29	18	11		
☒ IB-11C	33.5	Elastic SILT with Sand (MH)					67	46	21		
▲ W- 1	0.0	Silty SAND (SM)									
★ W- 1	4.0	Clayey SAND (SC)					31	15	16		
◎ W- 1	23.5	Sandy SILT (ML)					38	28	10		
BOREHOLE	DEPTH	D100	D60	D30	D10	%Gravel	%Sand	%Silt		%Clay	
● IB-11C	6.0	0.075								37.7	
☒ IB-11C	33.5	0.075								70.7	
▲ W- 1	0.0	9.5	0.369			0.8	63.0			36.2	
★ W- 1	4.0	0.075								33.9	
◎ W- 1	23.5	0.075								62.5	

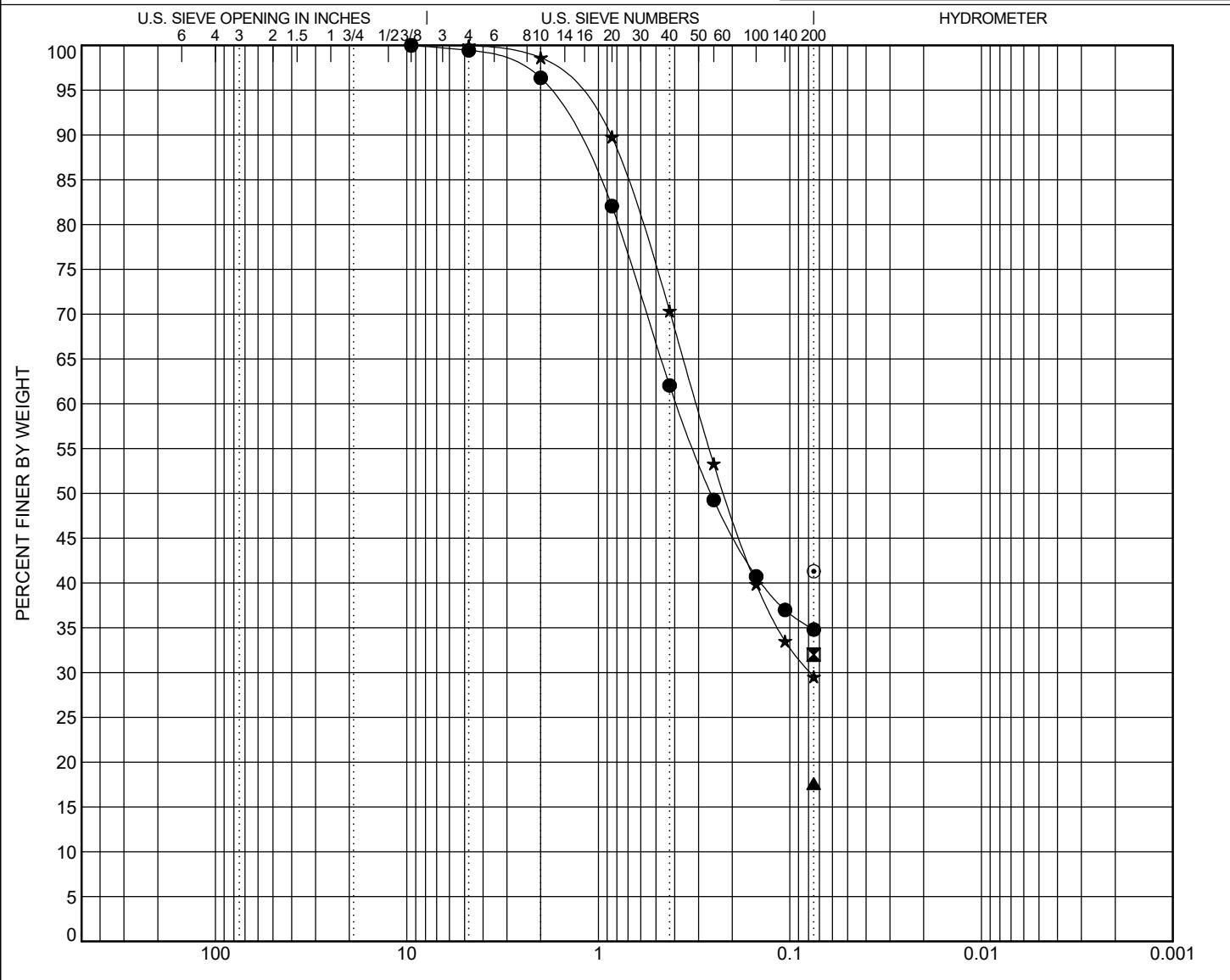


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

BOREHOLE	DEPTH	Classification					LL	PL	PI	Cc	Cu
● W-2	0.0	Silty SAND (SM)									
☒ W-2	4.0	Clayey SAND (SC)					32	16	16		
▲ W-2	8.0	Clayey SAND (SC)					32	14	18		
★ W-3	0.0	Silty SAND (SM)									
○ W-3	4.0	Clayey SAND (SC)					33	18	15		
BOREHOLE	DEPTH	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay		
● W-2	0.0	9.5	0.39			0.6	64.7		34.8		
☒ W-2	4.0	0.075							32.0		
▲ W-2	8.0	0.075							17.6		
★ W-3	0.0	9.5	0.308	0.078		0.0	70.4		29.5		
○ W-3	4.0	0.075							41.3		

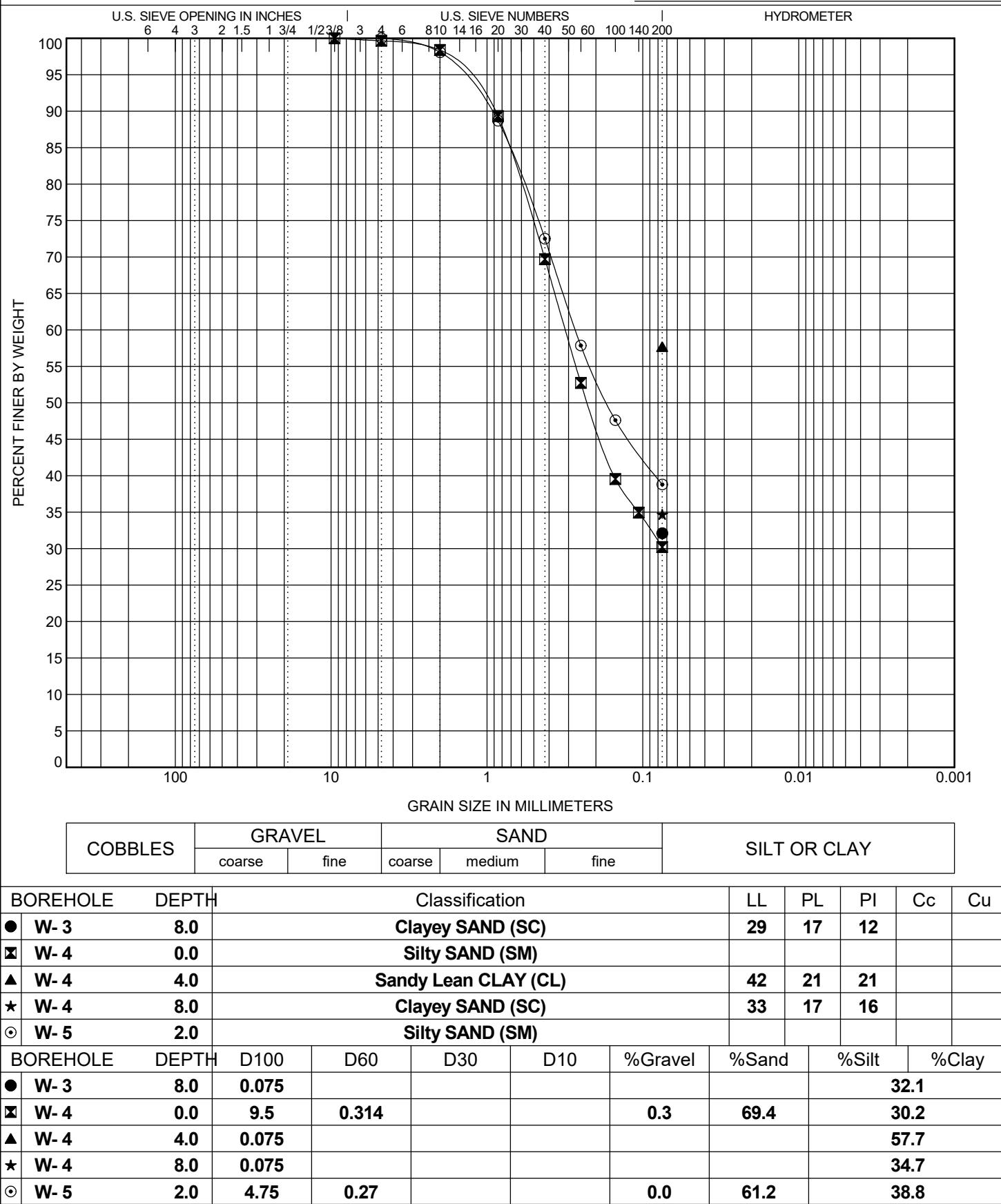


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



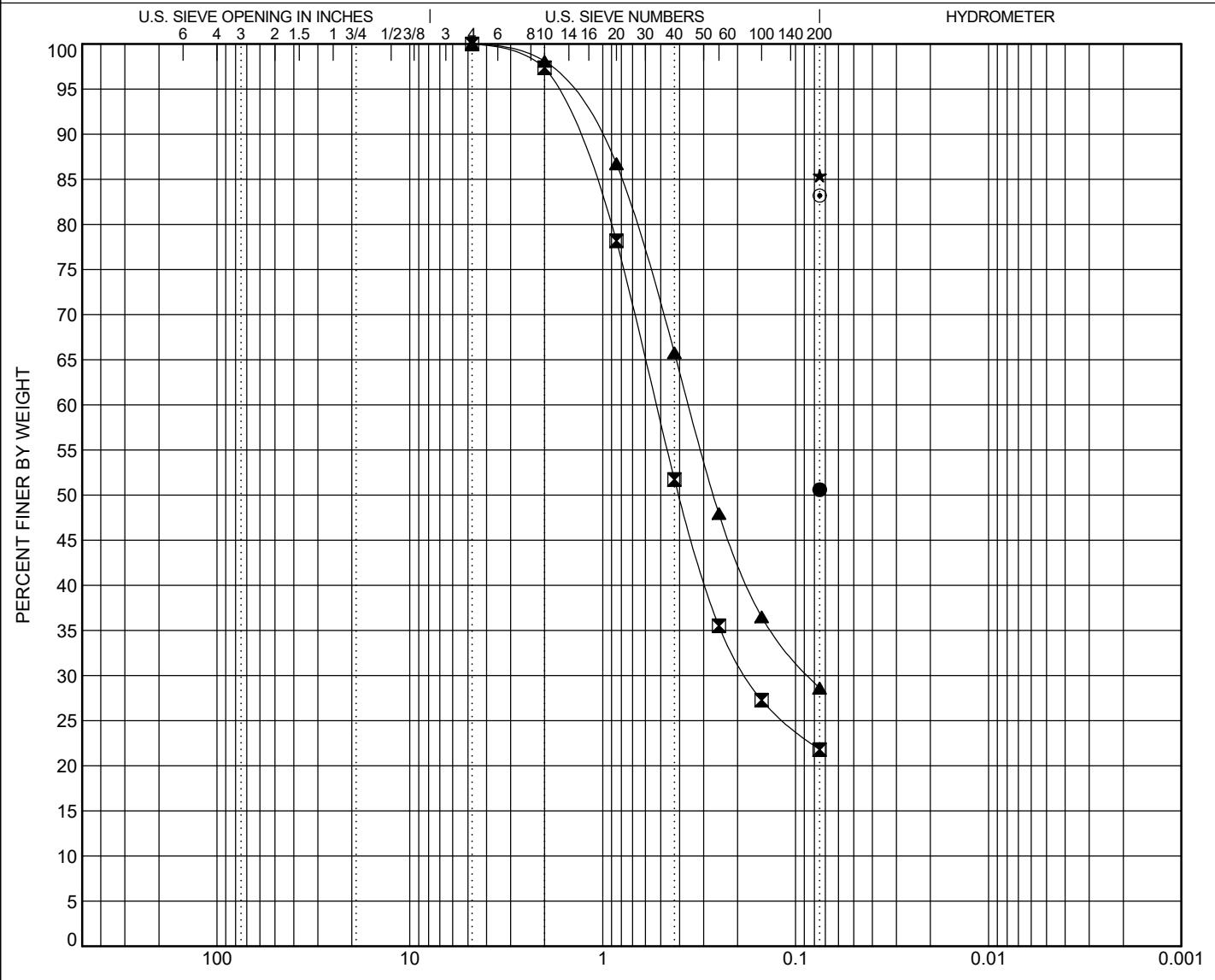


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



GRAIN SIZE IN MILLIMETERS						SILT OR CLAY	
COBBLES	GRAVEL		SAND				
	coarse	fine	coarse	medium	fine		

BOREHOLE DEPTH		Classification	LL	PL	PI	Cc	Cu
● W-5	4.0	Sandy Lean CLAY (CL)	44	23	21		
☒ W-5	13.5	Silty SAND (SM)	NP	NP	NP		
▲ W-6	0.0	Silty SAND (SM)	NP	NP	NP		
★ W-6	6.0	Lean CLAY with Sand (CL)	34	18	16		
◎ W-6	8.0	Lean CLAY with Sand (CL)	29	18	11		

BOREHOLE		DEPTH	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
●	W-5	4.0	0.075						50.6	
☒	W-5	13.5	4.75	0.528	0.178		0.0	78.2	21.8	
▲	W-6	0.0	4.75	0.358	0.085		0.0	71.4	28.6	
★	W-6	6.0	0.075						85.4	
◎	W-6	8.0	0.075						83.2	

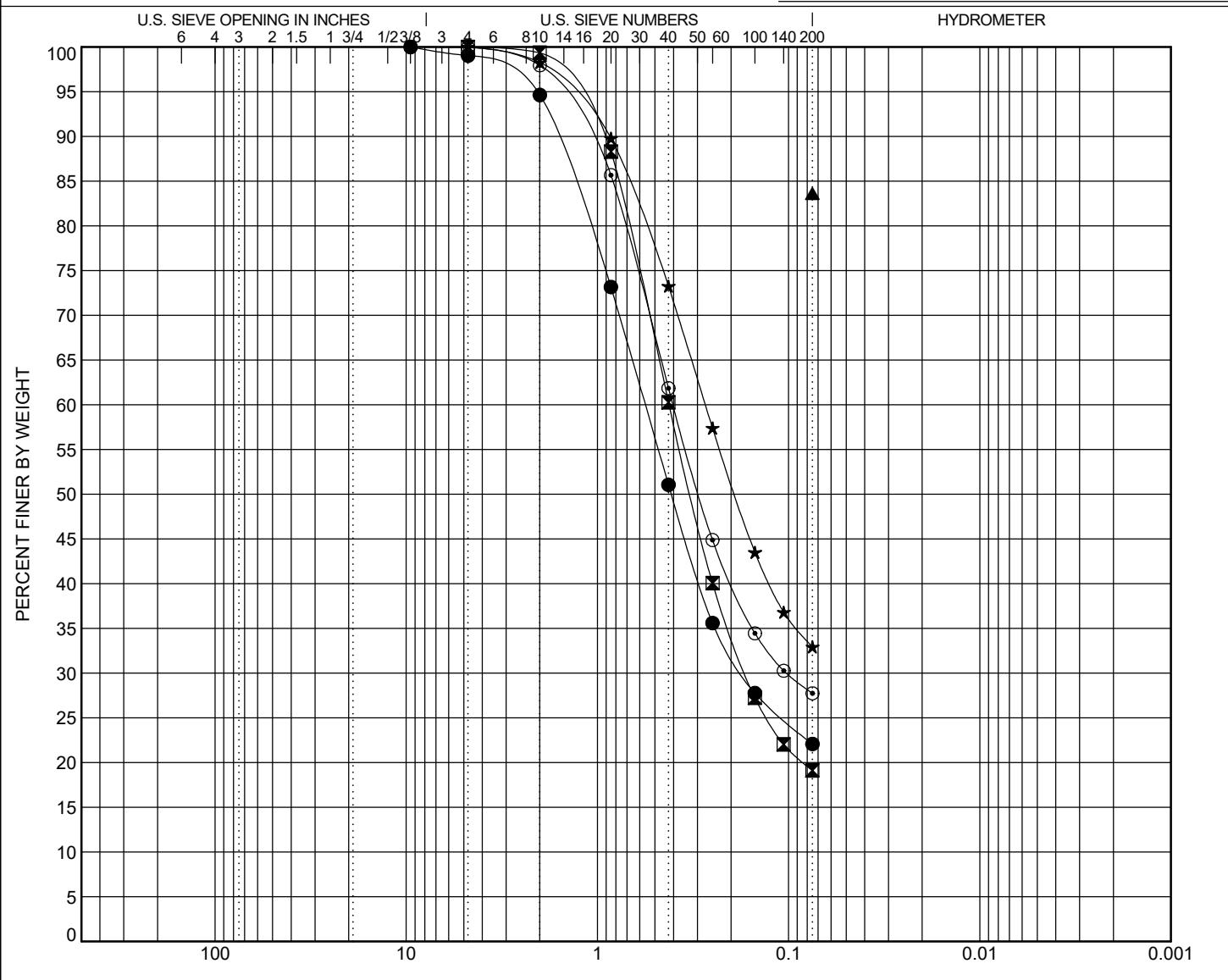


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



BOREHOLE	DEPTH	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
● W-6	13.5	9.5	0.563	0.174		1.0	77.0		22.1
☒ W-7	0.0	4.75	0.422	0.167		0.0	80.9		19.1
▲ W-7	6.0	0.075							83.6
★ W-7	13.5	4.75	0.273			0.0	67.1		32.9
○ W-8	0.0	9.5	0.401	0.102		0.1	72.2		27.7

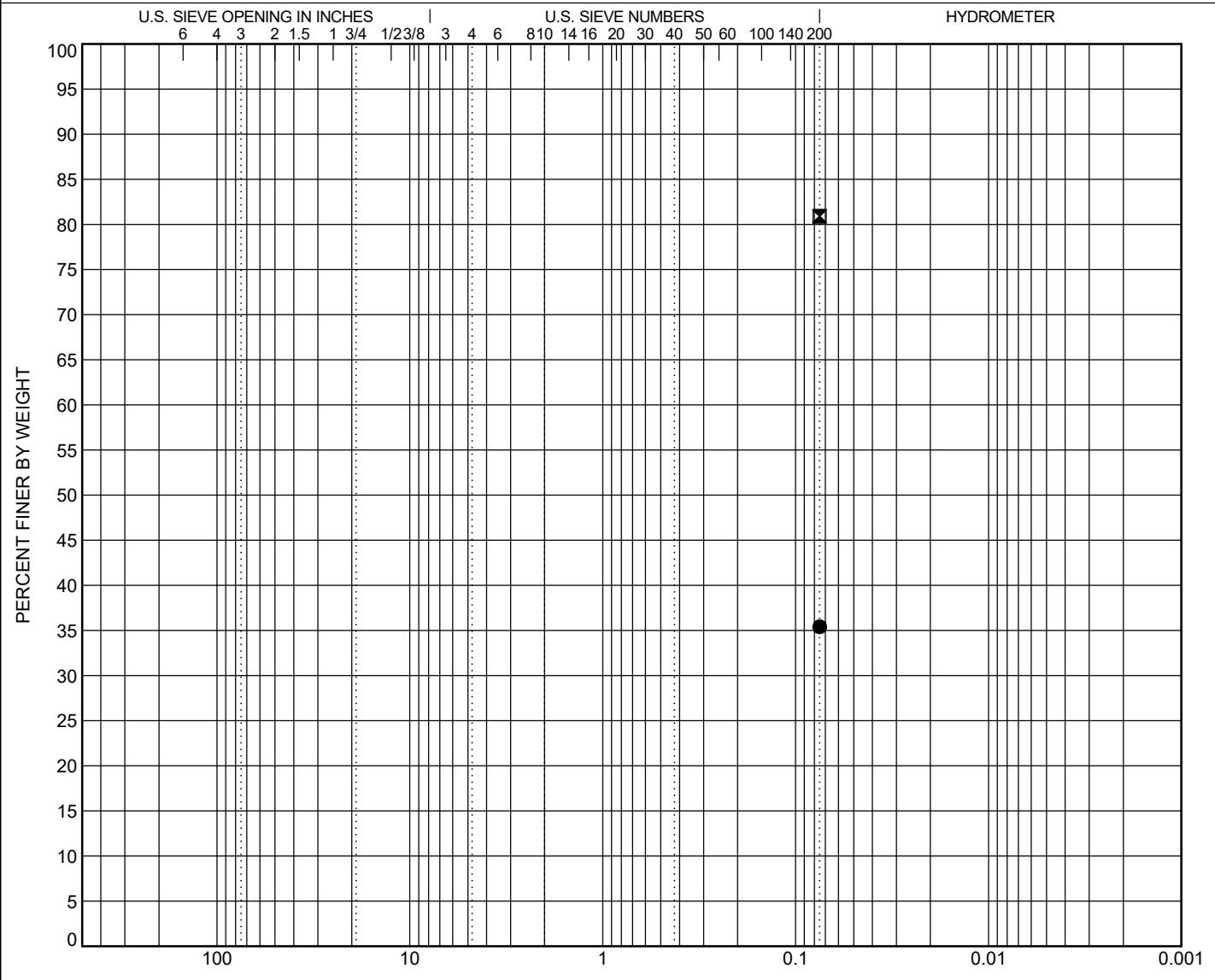


GRAIN SIZE DISTRIBUTION

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



GRAIN SIZE IN MILLIMETERS						
COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

BOREHOLE	DEPTH	Classification	LL	PL	PI	Cc	Cu
● W- 8	5.0	Clayey SAND (SC)	45	22	23		
☒ W- 8	6.0	Lean CLAY with Sand (CL)	33	19	14		

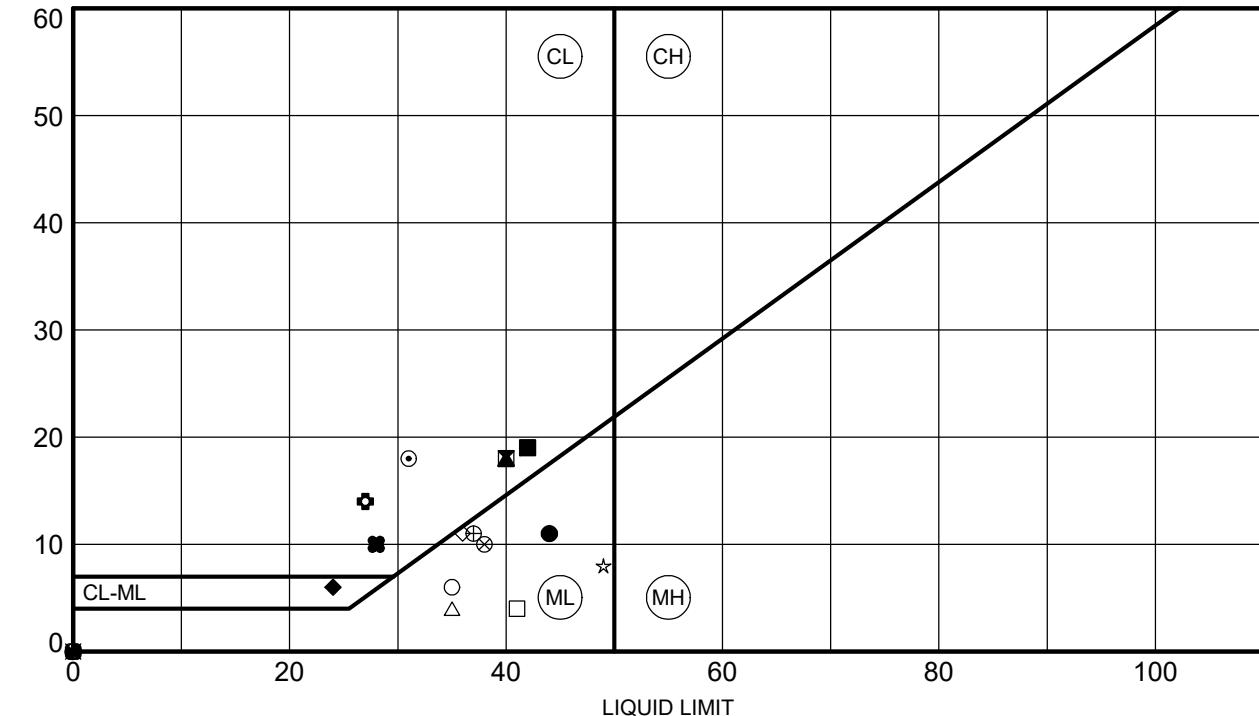


ATTERBERG LIMITS' RESULTS

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



ATTERBERG LIMITS 23610178A CONNECTOR BRIDGE OVER I-77 GPJ SCDOT DATA TEMPLATE_01 30 2015.GDT 1/12/24

BOREHOLE	DEPTH	LL	PL	PI	Fines	Classification
● EB-1C	23.5	44	33	11	87	SILT with Sand (ML)
■ EB-2C	4.0	40	22	18	34	Clayey SAND (SC)
▲ EB-2C	6.0	40	22	18	79	Lean CLAY with Sand (CL)
★ EB-2C	18.5	NP	NP	NP	20	Silty SAND (SM)
○ EB-3C	4.0	31	13	18	40	Clayey SAND (SC)
◆ EB-3C	8.0	27	13	14	21	Clayey SAND (SC)
○ EB-3C	33.5	35	29	6	81	SILT with Sand (ML)
△ EB-3C	78.5	35	31	4	67	Sandy SILT (ML)
⊗ EB-3C	93.5	38	28	10	70	Sandy SILT (ML)
⊕ EB-4C	6.0	37	26	11	44	Silty SAND (SM)
□ EB-4C	13.5	41	37	4	89	SILT (ML)
● EB-5C	6.0	NP	NP	NP	27	Silty SAND (SM)
● EB-5C	8.0	NP	NP	NP	39	Silty SAND (SM)
★ EB-5C	23.5	49	41	8	93	SILT (ML)
⊗ EB-6C	0.0	NP	NP	NP	19	Silty SAND (SM)
■ EB-6C	4.0	42	23	19	84	Lean CLAY with Sand (CL)
◆ EB-6C	13.5	24	18	6	20	Silty, Clayey SAND (SC-SM)
◇ EM-1	8.0	36	25	11	88	SILT with Sand (ML)
× EM-2	0.0	NP	NP	NP	39	Silty SAND (SM)
● EM-2	6.0	28	18	10	24	Clayey SAND (SC)

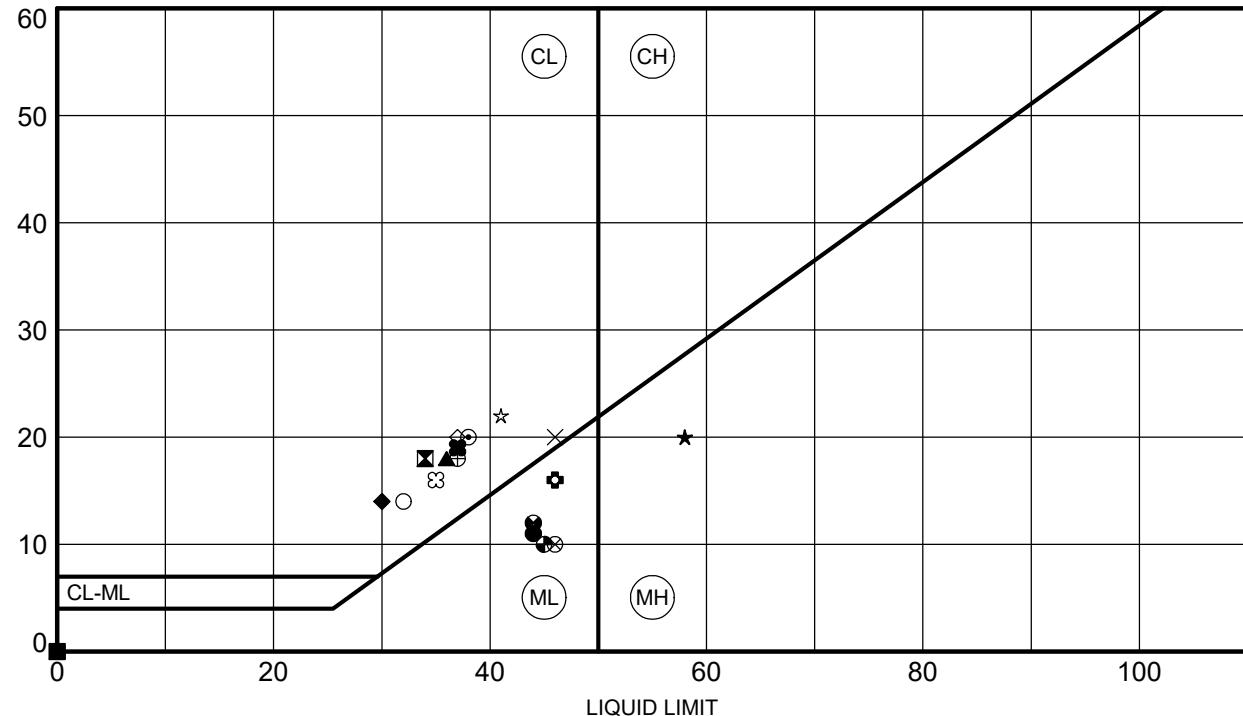


ATTERBERG LIMITS' RESULTS

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



ATTERBERG LIMITS 23610178A CONNECTOR BRIDGE OVER I-77 GPJ SCDOT DATA TEMPLATE_01 30 2015.GDT 1/12/24

BOREHOLE	DEPTH	LL	PL	PI	Fines	Classification
● EM- 2	13.5	44	33	11	86	SILT with Sand (ML)
■ IB- 1C	0.0	34	16	18	45	Clayey SAND (SC)
▲ IB- 1C	6.0	36	18	18	20	Clayey SAND (SC)
★ IB- 1C	18.5	58	38	20	59	Sandy Elastic SILT (MH)
○ IB- 2C	2.0	38	18	20	56	Sandy Lean CLAY (CL)
◆ IB- 2C	13.5	46	30	16	83	SILT with Sand (ML)
○ IB- 3C	0.0	32	18	14	63	Sandy Lean CLAY (CL)
△ IB- 3C	8.0	NP	NP	NP	24	Silty SAND (SM)
⊗ IB- 3C	13.5	46	36	10	81	SILT with Sand (ML)
⊕ IB- 4C	2.0	37	19	18	64	Sandy Lean CLAY (CL)
□ IB- 4C	8.0	NP	NP	NP	22	Silty SAND (SM)
● IB- 4C	18.5	44	32	12	66	Sandy SILT (ML)
● IB- 4C	88.5	45	35	10	76	SILT with Sand (ML)
★ IB- 5C	2.0	41	19	22	65	Sandy Lean CLAY (CL)
⊗ IB- 5C	4.0	35	19	16	79	Lean CLAY with Sand (CL)
■ IB- 6C	0.0	NP	NP	NP	12	Silty SAND (SM)
◆ IB- 6C	2.0	30	16	14	65	Sandy Lean CLAY (CL)
△ IB- 6C	6.0	37	17	20	41	Clayey SAND (SC)
× IB- 7C	4.0	46	26	20	36	Clayey SAND (SC)
● IB- 7C	8.0	37	18	19	79	Lean CLAY with Sand (CL)

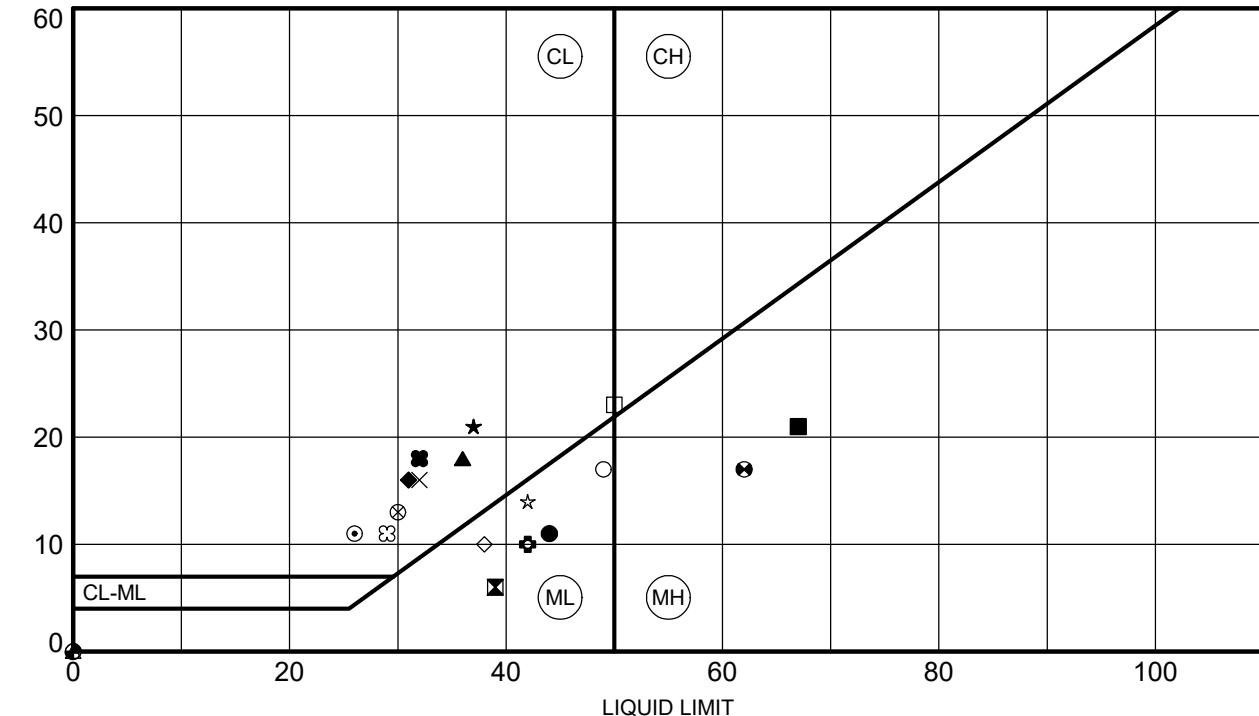


ATTERBERG LIMITS' RESULTS

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



ATTERBERG LIMITS 23610178A CONNECTOR BRIDGE OVER I-77 GPJ SCDOT DATA TEMPLATE_01 30 2015.GDT 1/12/24

BOREHOLE	DEPTH	LL	PL	PI	Fines	Classification
● IB- 7C	28.5	44	33	11	73	SILT with Sand (ML)
■ IB- 7C	63.5	39	33	6	79	SILT with Sand (ML)
▲ IB- 8C	6.0	36	18	18	47	Clayey SAND (SC)
★ IB- 8C	8.0	37	16	21	76	Lean CLAY with Sand (CL)
○ IB- 8C	13.5	26	15	11	48	Clayey SAND (SC)
◆ IB- 8C	23.5	42	32	10	80	SILT with Sand (ML)
○ IB- 8C	48.5	49	32	17	69	Sandy SILT (ML)
△ IB- 9C	0.0	NP	NP	NP	18	Silty SAND (SM)
⊗ IB- 9C	13.5	30	17	13	67	Sandy Lean CLAY (CL)
⊕ IB-10C	0.0	NP	NP	NP	20	Silty SAND (SM)
□ IB-10C	8.0	50	27	23	52	Sandy Fat CLAY (CH)
● IB-10C	28.5	62	45	17	90	Elastic SILT (MH)
● IB-11C	0.0	NP	NP	NP	19	Silty SAND (SM)
★ IB-11C	2.0	42	28	14	69	Sandy SILT (ML)
⊗ IB-11C	6.0	29	18	11	38	Clayey SAND (SC)
■ IB-11C	33.5	67	46	21	71	Elastic SILT with Sand (MH)
◆ W- 1	4.0	31	15	16	34	Clayey SAND (SC)
◇ W- 1	23.5	38	28	10	63	Sandy SILT (ML)
× W- 2	4.0	32	16	16	32	Clayey SAND (SC)
⊗ W- 2	8.0	32	14	18	18	Clayey SAND (SC)

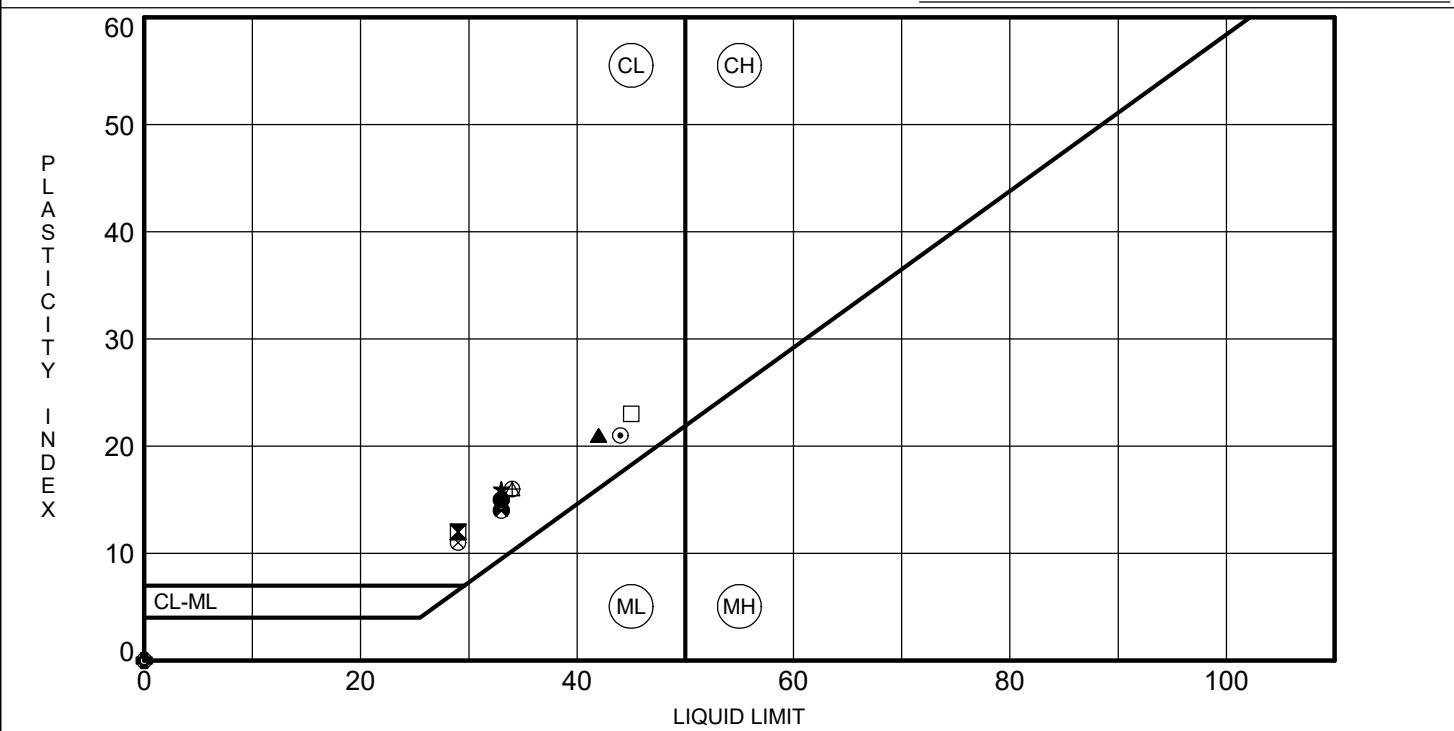


ATTERBERG LIMITS' RESULTS

PROJECT ID P042443 (S&ME 23610178A)

PROJECT NAME I-77 Exit 26 Phase I

PROJECT COUNTY Richland



BOREHOLE	DEPTH	LL	PL	PI	Fines	Classification
● W-3	4.0	33	18	15	41	Clayey SAND (SC)
✖ W-3	8.0	29	17	12	32	Clayey SAND (SC)
▲ W-4	4.0	42	21	21	58	Sandy Lean CLAY (CL)
★ W-4	8.0	33	17	16	35	Clayey SAND (SC)
○ W-5	4.0	44	23	21	51	Sandy Lean CLAY (CL)
✖ W-5	13.5	NP	NP	NP	22	Silty SAND (SM)
○ W-6	0.0	NP	NP	NP	29	Silty SAND (SM)
△ W-6	6.0	34	18	16	85	Lean CLAY with Sand (CL)
✖ W-6	8.0	29	18	11	83	Lean CLAY with Sand (CL)
⊕ W-7	6.0	34	18	16	84	Lean CLAY with Sand (CL)
□ W-8	5.0	45	22	23	35	Clayey SAND (SC)
✖ W-8	6.0	33	19	14	81	Lean CLAY with Sand (CL)

**Appendix VII – Laboratory Test Data Sheets – Corrosion Series
Testing**



Project X

Corrosion Engineering

Corrosion Control – Soil, Water, Metallurgy Testing Lab

REPORT S231204F

Page 1

Results Only Soil Testing for I-77 Exit 26 Interchange - Connector Bridge over I-77

December 5, 2023

Prepared for:

Matt Cooke
S&ME, Inc.
134 Suber Road
Columbia, SC 29210
mcooke@smeinc.com

**Project X Job#: S231204F
Client Job or PO#: 23610178A**

Respectfully Submitted,



Eduardo Hernandez, M.Sc., P.E.
Sr. Corrosion Consultant
NACE Corrosion Technologist #16592
Professional Engineer
California No. M37102
ehernandez@projectxcorrosion.com





Project X

Corrosion Engineering

Corrosion Control – Soil, Water, Metallurgy Testing Lab

REPORT S231204F

Page 2

Soil Analysis Lab Results

Client: S&ME, Inc.

Job Name: I-77 Exit 26 Interchange - Connector Bridge over I-77

Client Job Number: 23610178A

Project X Job Number: S231204F

December 5, 2023

	Method	AASHTO T290		AASHTO T291		AASHTO T288		AASHTO T289
Bore# / Description	Depth	Sulfates SO ₄ ²⁻		Chlorides Cl ⁻		Resistivity As Rec'd Minimum		pH
	(ft)	(mg/kg)	(wt%)	(mg/kg)	(wt%)	(Ohm-cm)	(Ohm-cm)	
EB-2C SS-8	23.5-25	21.7	0.0022	49.3	0.0049	93,800	56,950	6.9
EB-3C SS-6	13.5-15	30.6	0.0031	77.1	0.0077	42,880	34,840	6.0
IB-7C SS-7	18.5-20	25.4	0.0025	75.7	0.0076	73,700	67,000	5.6
IB-1C SS-6	13.5-15	43.1	0.0043	105.7	0.0106	45,560	40,200	5.7
IB-11C SS-7	18.5-20	26.5	0.0026	59.9	0.0060	67,000	58,290	6.8
EB-5C SS-10	33.5-35	27.2	0.0027	62.9	0.0063	93,800	67,000	7.0

Cations and Anions, except Sulfide and Bicarbonate, tested with Ion Chromatography

mg/kg = milligrams per kilogram (parts per million) of dry soil weight

ND = 0 = Not Detected | NT = Not Tested | Unk = Unknown

Chemical Analysis performed on 1:3 Soil-To-Water extract

PPM = mg/kg (soil) = mg/L (Liquid)

Note: Sometimes a bad sulfate hit is a contaminated spot. Typical fertilizers are Potassium chloride, ammonium sulfate or ammonium sulfate nitrate (ASN). So this is another reason why testing full corrosion series is good because we then have the data to see if those other ingredients are present meaning the soil sample is just fertilizer-contaminated soil. This can happen often when the soil samples collected are simply surface scoops which is why it's best to dig in a foot, throw away the top and test the deeper stuff. Dairy farms are also notorious for these items.



* Lab Tech notes

Lab Request Sheet Chain of Custody

Phone (213) 928-7213 • Fax (951) 226-1720 • www.projectxcorrosion.com

Ship Samples To: 29990 Technology Dr, Suite 13, Murrieta, CA 92563

Appendix VIII – Laboratory Test Data Sheets – Undisturbed Samples

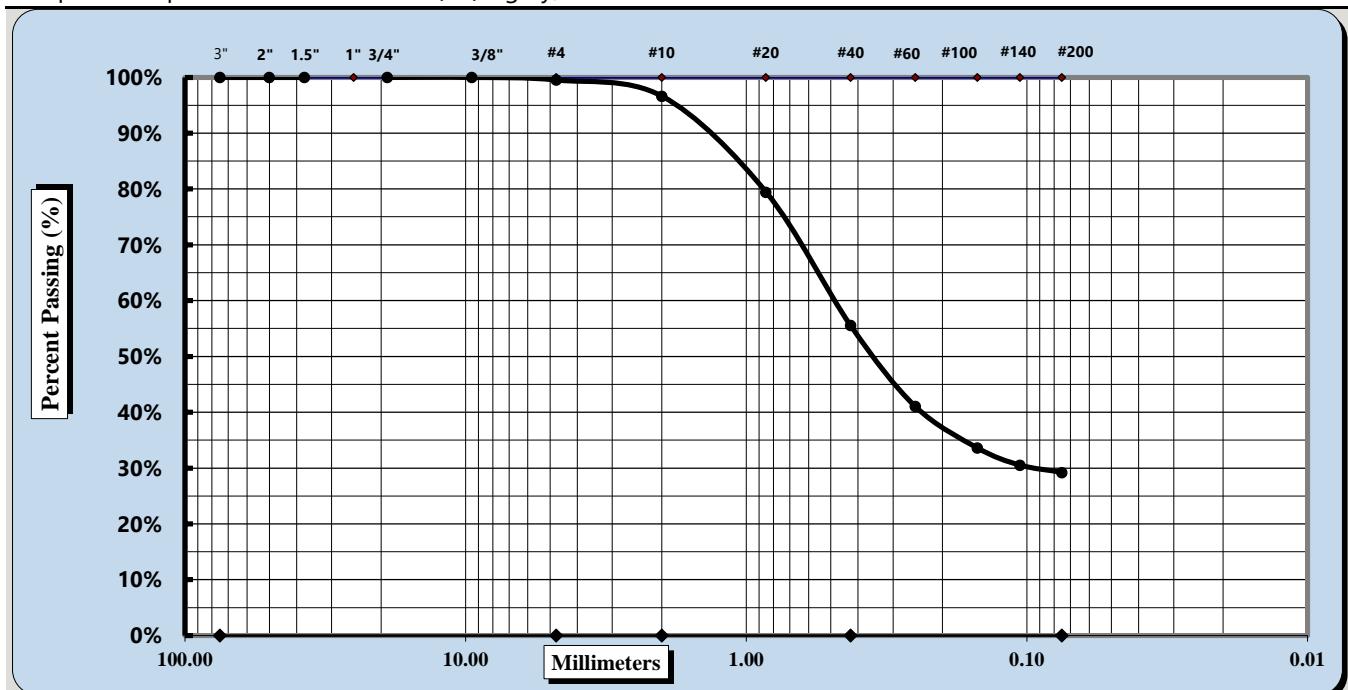
SIEVE ANALYSIS OF SOIL

Single sieve set

ASTM D 6913

S&ME, Inc. - Greenville: 48 Brookfield Oaks Dr., Suite F Greenville, SC 29607

Project #:	23610178A	Report Date:	1/3/24
Project Name:	I-77 Exit 26 Interchange	Test Date:	12/18-1/03/24
Client Name:	RS&H, Inc.		
Client Address:	1520 South Boulevard Suite 200 Charlotte, NC 28203		
Boring #:	W-2	Log #:	129g
Location:	UD-1	Type:	Undisturbed
Sample Description:	CLAYEY SAND (SC) - gray, fine to medium	Sample Date:	10/25/23



Cobbles	< 300 mm (12") and > 75 mm (3")	Fine Sand	< 0.425 mm and > 0.075 mm
Gravel	< 75 mm and > 4.75 mm (#4)	Silt	< 0.075 and > 0.005 mm
Coarse Sand	< 4.75 mm and > 2.00 mm (#10)	Clay	< 0.005 mm
Medium Sand	< 2.00 mm and > 0.425 mm (#40)	Colloids	< 0.001 mm

Method:	B	Procedure for obtaining Specimen:	Moist	Dispersion Process:	Dispersant
Maximum Particle Size	4.75 mm	Coarse Sand	2.9%	Fine Sand	26.3%
Gravel	0.5%	Medium Sand	41.1%	Silt & Clay	29.2%
Liquid Limit	25	Plastic Limit	13	Plastic Index	12

Natural Moisture

*

Notes / Deviations / References:

*See CU Triaxial Test Report

Brian Vaughan, P.E.
Technical Responsibility

Brian Vaughan
Signature

QA Supervisor
Position

1/3/24
Date

This report shall not be reproduced, except in full, without the written approval of S&ME, Inc.

**LIQUID LIMIT, PLASTIC LIMIT,
 & PLASTIC INDEX**



ASTM D 4318 AASHTO T 89 AASHTO T 90

S&ME, Inc. - Greenville 48 Brookfield Oaks Dr., Suite F Greenville, SC 29607

Project #: 23610178A Report Date: 1/03/24

Project Name: I-77 Exit 26 Interchange Test Date: 1/02/24

Client Name: RS&H, Inc.

Client Address: 1520 South Boulevard Suite 200 Charlotte, NC 28203

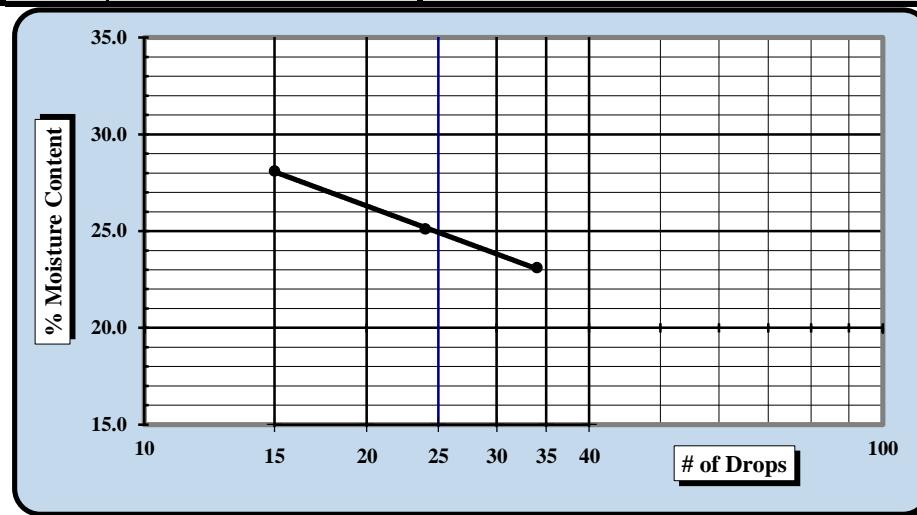
Boring #: W-2 Log #: 129g Sample Date: 10/25/23

Location: UD-1 Type: Undisturbed Depth: 5 - 7'

Sample Description: CLAYEY SAND (SC) - gray, fine to medium

Type and Specification	S&ME ID #	Cal Date:	Type and Specification	S&ME ID #	Cal Date:
Balance (0.01 g)	13942	10/31/2023	Grooving tool	23119	10/15/2023
LL Apparatus	23158	7/18/2023			
Oven	13978	10/1/2023			

Pan #		Tare #:	Liquid Limit					Plastic Limit		
			1	2	3			4	5	
A	Tare Weight	26.70	26.50	26.36				25.91	26.96	
B	Wet Soil Weight + A	42.71	43.77	41.85				36.13	35.57	
C	Dry Soil Weight + A	39.71	40.30	38.45				34.92	34.56	
D	Water Weight (B-C)	3.00	3.47	3.40				1.21	1.01	
E	Dry Soil Weight (C-A)	13.01	13.80	12.09				9.01	7.60	
F	% Moisture (D/E)*100	23.1%	25.1%	28.1%				13.4%	13.3%	
N	# OF DROPS	34	24	15				<i>Moisture Contents determined by ASTM D 2216</i>		
LL	LL = F * FACTOR									
Ave.	Average							13.4%		



One Point Liquid Limit

N	Factor	N	Factor
20	0.974	26	1.005
21	0.979	27	1.009
22	0.985	28	1.014
23	0.99	29	1.018
24	0.995	30	1.022
25	1.000		

NP, Non-Plastic

Liquid Limit **25**

Plastic Limit **13**

Plastic Index **12**

Group Symbol **CL**

Multipoint Method

One-point Method

Wet Preparation Dry Preparation Air Dried % Passing the #200 Sieve: 29.2%

Notes / Deviations / References: Group symbol for minus #40 sieve portion only (see Sample Description for classification of entire sample).

ASTM D 4318: Liquid Limit, Plastic Limit, & Plastic Index of Soils

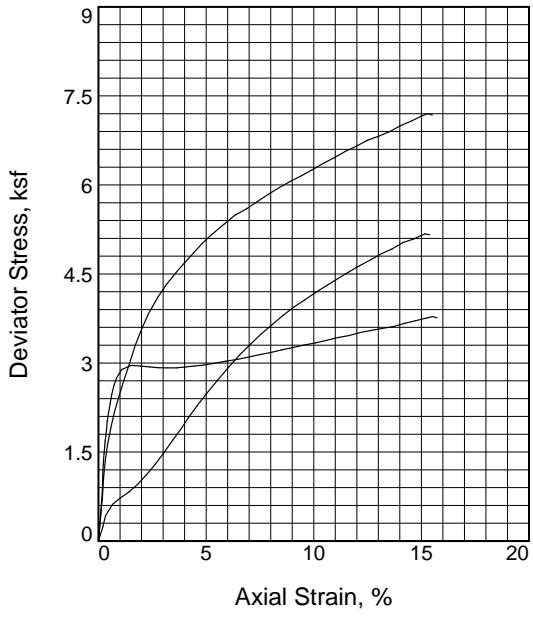
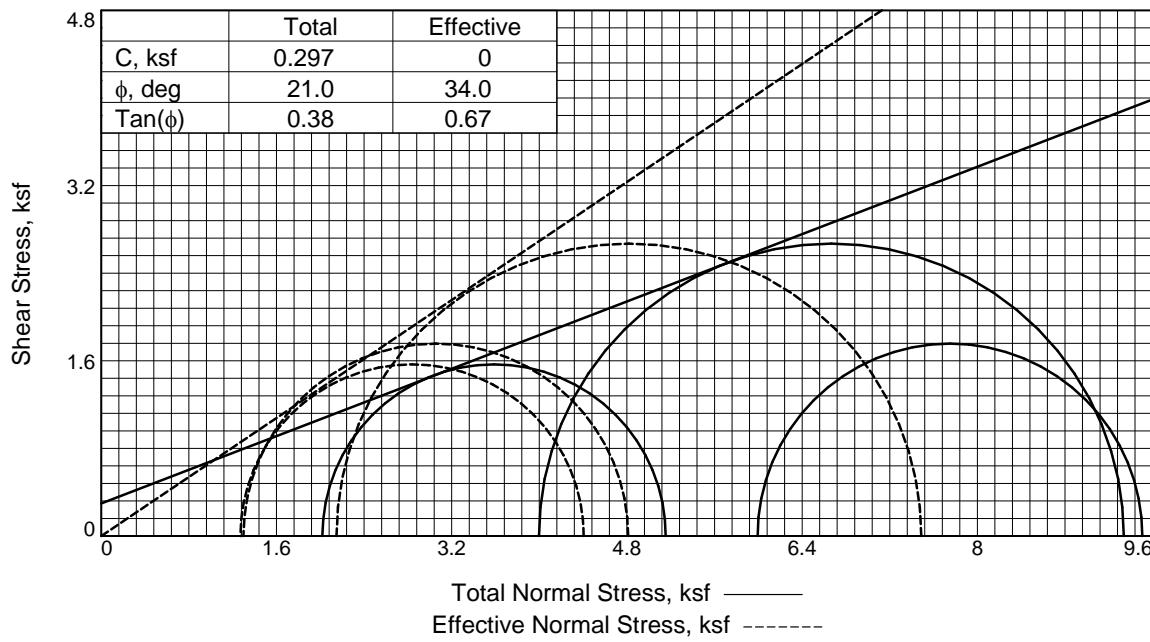
Benjamin J. Kovaleski
 Technician Name

1/03/24
 Date

Brian Vaughan, P.E.
 Technical Responsibility

1/03/24
 Date

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	Specimen No.	1	2	3
Initial	Water Content, %	5.1	6.9	6.5
	Dry Density, pcf	113.7	117.7	109.3
	Saturation, %	29.9	45.3	33.6
	Void Ratio	0.4550	0.4060	0.5132
	Diameter, in.	2.874	2.845	2.853
	Height, in.	5.730	5.710	5.680
At Test	Water Content, %	15.2	12.9	14.2
	Dry Density, pcf	116.7	123.5	119.4
	Saturation, %	96.8	100.8	98.0
	Void Ratio	0.4171	0.3393	0.3851
	Diameter, in.	2.848	2.803	2.774
	Height, in.	5.683	5.603	5.498
Strain rate, %/min.				
Eff. Cell Pressure, ksf				
Fail. Stress, ksf				
Total Pore Pr., ksf				
Strain, %				
Ult. Stress, ksf				
Total Pore Pr., ksf				
Strain, %				
$\bar{\sigma}_1$ Failure, ksf				
$\bar{\sigma}_3$ Failure, ksf				

Type of Test:

CU with Pore Pressures

Sample Type: Undisturbed

Description: CLAYEY SAND (SC) - gray, fine to medium

LL= 25

PL= 13

PI= 12

Assumed Specific Gravity= 2.65

Remarks: The specimens failed with bulging. Failure selected at peak stress ratio. ASTM D4767.

Figure 1

Client: RS&H, Inc.

Project: I-77 Exit 26 Interchange

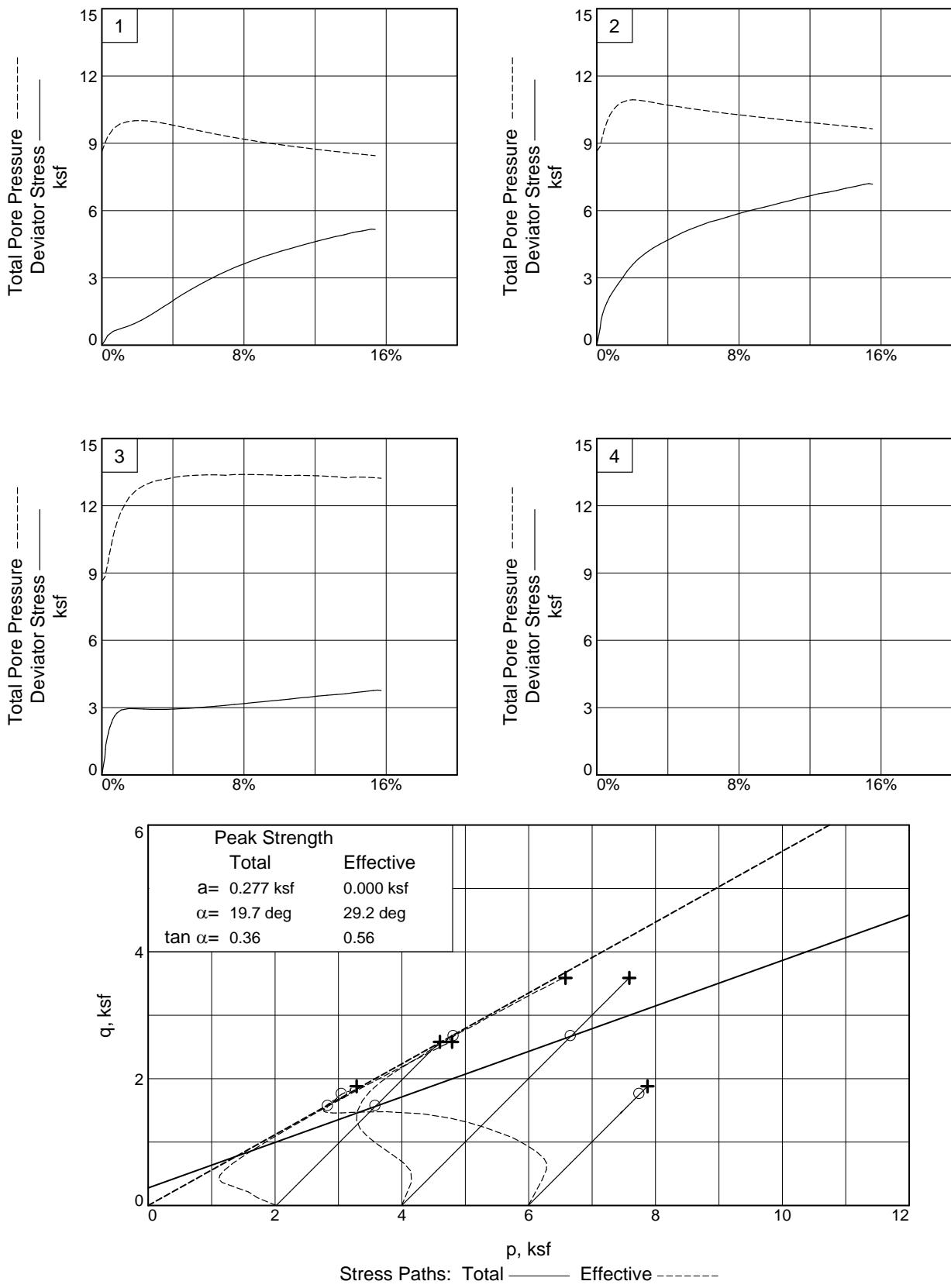
Location: UD-1

Sample Number: W-2 **Depth:** 5 - 7'
Proj. No.: 23610178A **Date Sampled:** 10/25/23

TRIAXIAL SHEAR TEST REPORT

S&ME, Inc.
Greenville, SC

C & phi are not test results but an interpretation of the test results. The designer is responsible for interpreting test data as provided by S&ME.



Client: RS&H, Inc.

Project: I-77 Exit 26 Interchange

Location: UD-1 **Depth:** 5 - 7'

Project No.: 23610178A

Sample Number: W-2
Figure 2

S&ME, Inc.

Tested By: Benjamin Kovaleski - 1/03/24

Checked By: Matthew F. Cooke, P.E.

TRIAXIAL COMPRESSION TEST

CU with Pore Pressures

1/16/2024

9:23 AM

Date: 10/25/23
Client: RS&H, Inc.
Project: I-77 Exit 26 Interchange
Project No.: 23610178A
Location: UD-1
Depth: 5 - 7' **Sample Number:** W-2
Description: CLAYEY SAND (SC) - gray, fine to medium
Remarks: The specimens failed with bulging. Failure selected at peak stress ratio. ASTM D4767.
Type of Sample: Undisturbed
Assumed Specific Gravity=2.65 **LL**=25 **PL**=13 **PI**=12
Test Method: ASTM D 4767 Method A

Parameters for Specimen No. 1

Specimen Parameter	Initial	Saturated	Consolidated	Final
Moisture content: Moist soil+tare, gms.	76.460			1264.640
Moisture content: Dry soil+tare, gms.	72.730			1097.500
Moisture content: Tare, gms.	0.000			0.000
Moisture, %	5.1	16.4	15.2	15.2
Moist specimen weight, gms.	1166.35			
Diameter, in.	2.874	2.870	2.848	
Area, in.²	6.487	6.469	6.371	
Height, in.	5.730	5.722	5.683	
Net decrease in height, in.		0.008	0.039	
Net decrease in water volume, cc.			13.300	
Wet density, pcf	119.5	132.9	134.5	
Dry density, pcf	113.7	114.2	116.7	
Void ratio	0.4550	0.4489	0.4171	
Saturation, %	29.9	97.0	96.8	

Test Readings for Specimen No. 1**Membrane modulus** = 0.14 kN/cm²**Membrane thickness** = 0.03 cm**Consolidation cell pressure** = 74.020 psi (10.659 ksf)**Consolidation back pressure** = 60.000 psi (8.640 ksf)**Consolidation effective confining stress** = 2.019 ksf**Strain rate, %/min.** = 0.48**Fail. Stress** = 3.135 ksf **at reading no.** 17**Ult. Stress** = 5.160 ksf **at reading no.** 35

Test Readings for Specimen No. 1

No.	Def. Dial in.	Load Dial	Load lbs.	Strain %	Deviator Stress ksf	Minor Eff. Stress ksf	Major Eff. Stress ksf	1:3 Ratio	Pore Press. psi	P ksf	Q ksf
0	0.0000	0.000	0.0	0.0	0.000	2.019	2.019	1.00	60.000	2.019	0.000
1	0.0114	10.715	10.7	0.2	0.242	1.605	1.847	1.15	62.874	1.726	0.121
2	0.0187	18.949	18.9	0.3	0.427	1.367	1.794	1.31	64.526	1.581	0.213
3	0.0367	27.554	27.6	0.6	0.619	1.004	1.623	1.62	67.047	1.314	0.309
4	0.0571	32.318	32.3	1.0	0.723	0.806	1.530	1.90	68.420	1.168	0.362
5	0.0805	37.112	37.1	1.4	0.827	0.699	1.526	2.18	69.165	1.113	0.413
6	0.1037	43.139	43.1	1.8	0.957	0.653	1.611	2.46	69.482	1.132	0.479
7	0.1266	50.492	50.5	2.2	1.116	0.646	1.761	2.73	69.537	1.204	0.558
8	0.1502	58.888	58.9	2.6	1.296	0.663	1.959	2.95	69.415	1.311	0.648
9	0.1733	68.258	68.3	3.0	1.496	0.706	2.201	3.12	69.120	1.453	0.748
10	0.1963	77.986	78.0	3.5	1.702	0.761	2.463	3.24	68.732	1.612	0.851
11	0.2198	87.796	87.8	3.9	1.908	0.825	2.733	3.31	68.288	1.779	0.954
12	0.2374	96.003	96.0	4.2	2.079	0.876	2.955	3.37	67.936	1.916	1.040
13	0.2602	105.619	105.6	4.6	2.278	0.946	3.224	3.41	67.448	2.085	1.139
14	0.2834	114.946	114.9	5.0	2.469	1.016	3.484	3.43	66.966	2.250	1.234
15	0.3151	127.186	127.2	5.5	2.715	1.107	3.822	3.45	66.334	2.465	1.358
16	0.3440	138.040	138.0	6.1	2.931	1.192	4.123	3.46	65.742	2.658	1.466
17	0.3729	148.451	148.5	6.6	3.135	1.270	4.406	3.47	65.199	2.838	1.568
18	0.4014	157.842	157.8	7.1	3.316	1.347	4.662	3.46	64.668	3.005	1.658
19	0.4299	167.182	167.2	7.6	3.493	1.417	4.910	3.46	64.177	3.164	1.746
20	0.4589	175.592	175.6	8.1	3.648	1.485	5.133	3.46	63.709	3.309	1.824
21	0.4873	183.948	183.9	8.6	3.801	1.552	5.354	3.45	63.241	3.453	1.901
22	0.5167	192.109	192.1	9.1	3.948	1.616	5.563	3.44	62.799	3.590	1.974
23	0.5453	198.999	199.0	9.6	4.066	1.673	5.739	3.43	62.405	3.706	2.033
24	0.5743	206.462	206.5	10.1	4.195	1.728	5.923	3.43	62.022	3.825	2.098
25	0.6029	213.160	213.2	10.6	4.307	1.783	6.090	3.42	61.641	3.936	2.153
26	0.6318	220.088	220.1	11.1	4.422	1.831	6.253	3.42	61.306	4.042	2.211
27	0.6605	226.880	226.9	11.6	4.532	1.881	6.414	3.41	60.955	4.147	2.266
28	0.6891	233.596	233.6	12.1	4.640	1.931	6.570	3.40	60.614	4.250	2.320
29	0.7179	239.932	239.9	12.6	4.738	1.980	6.718	3.39	60.272	4.349	2.369
30	0.7470	246.564	246.6	13.1	4.841	2.023	6.864	3.39	59.968	4.444	2.420
31	0.7751	252.108	252.1	13.6	4.921	2.066	6.987	3.38	59.674	4.526	2.461
32	0.8039	259.149	259.1	14.1	5.029	2.115	7.144	3.38	59.331	4.630	2.515
33	0.8326	263.871	263.9	14.7	5.091	2.152	7.243	3.37	59.075	4.697	2.545
34	0.8617	269.873	269.9	15.2	5.175	2.193	7.368	3.36	58.794	4.780	2.588
35	0.8743	269.807	269.8	15.4	5.160	2.211	7.372	3.33	58.663	4.792	2.580

Parameters for Specimen No. 2					
Specimen Parameter	Initial	Saturated	Consolidated	Final	
Moisture content: Moist soil+tare, gms.	62.770				1250.510
Moisture content: Dry soil+tare, gms.	58.700				1107.610
Moisture content: Tare, gms.	0.000				0.000
Moisture, %	6.9	14.4	12.9	12.9	
Moist specimen weight, gms.	1198.83				
Diameter, in.	2.845	2.827	2.803		
Area, in.²	6.357	6.276	6.171		
Height, in.	5.710	5.674	5.603		
Net decrease in height, in.		0.036	0.071		
Net decrease in water volume, cc.			17.000		
Wet density, pcf	125.8	137.2	139.5		
Dry density, pcf	117.7	119.9	123.5		
Void ratio	0.4060	0.3794	0.3393		
Saturation, %	45.3	100.7	100.8		

Test Readings for Specimen No. 2

Membrane modulus = 0.14 kN/cm²

Membrane thickness = 0.03 cm

Consolidation cell pressure = 87.760 psi (12.637 ksf)

Consolidation back pressure = 60.000 psi (8.640 ksf)

Consolidation effective confining stress = 3.997 ksf

Strain rate, %/min. = 0.48

Fail. Stress = 5.340 ksf at reading no. 20

Ult. Stress = 7.178 ksf at reading no. 40

No.	Def. Dial in.	Load Dial	Load lbs.	Strain %	Deviator Stress ksf	Minor Eff. Stress ksf	Major Eff. Stress ksf	1:3 Ratio	Pore Press. psi	P ksf	Q ksf
0	0.0000	0.000	0.0	0.0	0.000	3.997	3.997	1.00	60.000	3.997	0.000
1	0.0104	32.085	32.1	0.2	0.747	3.779	4.526	1.20	61.520	4.152	0.374
2	0.0134	46.570	46.6	0.2	1.084	3.600	4.684	1.30	62.760	4.142	0.542
3	0.0176	58.190	58.2	0.3	1.354	3.344	4.697	1.40	64.541	4.020	0.677
4	0.0232	69.148	69.1	0.4	1.607	3.043	4.650	1.53	66.625	3.847	0.803
5	0.0319	81.879	81.9	0.6	1.900	2.685	4.585	1.71	69.115	3.635	0.950
6	0.0411	93.601	93.6	0.7	2.168	2.378	4.546	1.91	71.246	3.462	1.084
7	0.0526	104.829	104.8	0.9	2.423	2.128	4.551	2.14	72.984	3.339	1.212
8	0.0656	116.877	116.9	1.2	2.695	1.938	4.633	2.39	74.302	3.286	1.348
9	0.0789	128.543	128.5	1.4	2.957	1.815	4.773	2.63	75.153	3.294	1.479
10	0.0958	143.904	143.9	1.7	3.301	1.725	5.026	2.91	75.781	3.375	1.650
11	0.1132	156.874	156.9	2.0	3.587	1.698	5.285	3.11	75.969	3.491	1.793
12	0.1303	168.266	168.3	2.3	3.835	1.710	5.546	3.24	75.882	3.628	1.918
13	0.1540	180.763	180.8	2.7	4.102	1.758	5.860	3.33	75.555	3.809	2.051
14	0.1768	191.353	191.4	3.2	4.324	1.818	6.142	3.38	75.137	3.980	2.162
15	0.2004	200.557	200.6	3.6	4.513	1.878	6.391	3.40	74.719	4.134	2.256
16	0.2235	209.036	209.0	4.0	4.683	1.936	6.620	3.42	74.313	4.278	2.342
17	0.2468	217.517	217.5	4.4	4.852	1.982	6.835	3.45	73.993	4.409	2.426
18	0.2694	225.575	225.6	4.8	5.011	2.032	7.043	3.47	73.651	4.537	2.505
19	0.2927	232.975	233.0	5.2	5.153	2.080	7.233	3.48	73.317	4.656	2.576
20	0.3270	243.000	243.0	5.8	5.340	2.148	7.488	3.49	72.843	4.818	2.670
21	0.3558	251.328	251.3	6.4	5.493	2.203	7.696	3.49	72.460	4.949	2.746
22	0.3849	257.456	257.5	6.9	5.595	2.258	7.853	3.48	72.082	5.055	2.798

Test Readings for Specimen No. 2

No.	Def. Dial in.	Load Dial	Load lbs.	Strain %	Deviator Stress ksf	Minor Eff. Stress ksf	Major Eff. Stress ksf	1:3 Ratio	Pore Press. psi	P ksf	Q ksf
23	0.4128	264.503	264.5	7.4	5.718	2.312	8.029	3.47	71.708	5.170	2.859
24	0.4416	271.729	271.7	7.9	5.841	2.355	8.197	3.48	71.403	5.276	2.921
25	0.4704	278.543	278.5	8.4	5.954	2.401	8.356	3.48	71.083	5.379	2.977
26	0.4990	285.009	285.0	8.9	6.059	2.449	8.508	3.47	70.752	5.478	3.029
27	0.5282	291.225	291.2	9.4	6.155	2.493	8.649	3.47	70.445	5.571	3.078
28	0.5565	297.681	297.7	9.9	6.257	2.540	8.796	3.46	70.122	5.668	3.128
29	0.5847	304.398	304.4	10.4	6.362	2.584	8.946	3.46	69.818	5.765	3.181
30	0.6136	310.745	310.7	11.0	6.457	2.624	9.082	3.46	69.537	5.853	3.229
31	0.6424	317.725	317.7	11.5	6.564	2.668	9.232	3.46	69.231	5.950	3.282
32	0.6715	323.916	323.9	12.0	6.653	2.709	9.362	3.46	68.947	6.036	3.326
33	0.7000	330.642	330.6	12.5	6.752	2.750	9.502	3.46	68.663	6.126	3.376
34	0.7290	335.955	336.0	13.0	6.820	2.790	9.610	3.44	68.382	6.200	3.410
35	0.7571	341.656	341.7	13.5	6.896	2.831	9.726	3.44	68.103	6.278	3.448
36	0.7861	348.756	348.8	14.0	6.997	2.874	9.871	3.43	67.803	6.372	3.498
37	0.8147	354.907	354.9	14.5	7.078	2.910	9.988	3.43	67.554	6.449	3.539
38	0.8429	361.475	361.5	15.0	7.166	2.948	10.115	3.43	67.286	6.531	3.583
39	0.8578	364.448	364.4	15.3	7.203	2.970	10.173	3.43	67.136	6.571	3.601
40	0.8691	364.047	364.0	15.5	7.178	2.991	10.169	3.40	66.988	6.580	3.589

Parameters for Specimen No. 3				
Specimen Parameter	Initial	Saturated	Consolidated	Final
Moisture content: Moist soil+tare, gms.	65.130			1172.280
Moisture content: Dry soil+tare, gms.	61.150			1026.110
Moisture content: Tare, gms.	0.000			0.000
Moisture, %	6.5	18.1	14.2	14.2
Moist specimen weight, gms.	1109.91			
Diameter, in.	2.853	2.837	2.774	
Area, in.²	6.393	6.320	6.046	
Height, in.	5.680	5.648	5.498	
Net decrease in height, in.		0.032	0.150	
Net decrease in water volume, cc.			40.300	
Wet density, pcf	116.4	131.4	136.5	
Dry density, pcf	109.3	111.2	119.4	
Void ratio	0.5132	0.4876	0.3851	
Saturation, %	33.6	98.4	98.0	

Test Readings for Specimen No. 3

Membrane modulus = 0.14 kN/cm²

Membrane thickness = 0.03 cm

Consolidation cell pressure = 101.620 psi (14.633 ksf)

Consolidation back pressure = 60.000 psi (8.640 ksf)

Consolidation effective confining stress = 5.993 ksf

Strain rate, %/min. = 0.48

Fail. Stress = 3.513 ksf at reading no. 36

Ult. Stress = 3.760 ksf at reading no. 44

No.	Def. Dial in.	Load Dial	Load lbs.	Strain %	Deviator Stress ksf	Minor Eff. Stress ksf	Major Eff. Stress ksf	1:3 Ratio	Pore Press. psi	P ksf	Q ksf
0	0.0000	0.000	0.0	0.0	0.000	5.993	5.993	1.00	60.000	5.993	0.000
1	0.0095	33.724	33.7	0.2	0.802	5.808	6.610	1.14	61.284	6.209	0.401
2	0.0111	47.566	47.6	0.2	1.131	5.714	6.845	1.20	61.937	6.280	0.565
3	0.0124	56.101	56.1	0.2	1.333	5.615	6.948	1.24	62.630	6.281	0.667
4	0.0143	62.149	62.1	0.3	1.476	5.505	6.981	1.27	63.394	6.243	0.738
5	0.0170	70.899	70.9	0.3	1.684	5.287	6.971	1.32	64.903	6.129	0.842
6	0.0202	78.420	78.4	0.4	1.861	5.068	6.929	1.37	66.424	5.999	0.931
7	0.0221	84.848	84.8	0.4	2.013	4.859	6.872	1.41	67.880	5.865	1.006
8	0.0254	90.669	90.7	0.5	2.150	4.662	6.811	1.46	69.247	5.737	1.075
9	0.0300	97.815	97.8	0.5	2.317	4.345	6.663	1.53	71.444	5.504	1.159
10	0.0335	104.080	104.1	0.6	2.464	4.072	6.536	1.61	73.340	5.304	1.232
11	0.0391	110.604	110.6	0.7	2.616	3.745	6.361	1.70	75.610	5.053	1.308
12	0.0466	116.632	116.6	0.8	2.755	3.387	6.142	1.81	78.098	4.764	1.377
13	0.0596	122.710	122.7	1.1	2.891	2.882	5.773	2.00	81.605	4.328	1.446
14	0.0835	126.099	126.1	1.5	2.958	2.271	5.229	2.30	85.849	3.750	1.479
15	0.1066	126.257	126.3	1.9	2.949	1.936	4.885	2.52	88.172	3.411	1.475
16	0.1299	126.187	126.2	2.4	2.935	1.730	4.665	2.70	89.607	3.197	1.467
17	0.1531	126.093	126.1	2.8	2.920	1.586	4.506	2.84	90.605	3.046	1.460
18	0.1757	126.545	126.5	3.2	2.918	1.494	4.412	2.95	91.246	2.953	1.459
19	0.1995	127.162	127.2	3.6	2.919	1.442	4.361	3.02	91.603	2.902	1.460
20	0.2226	128.403	128.4	4.0	2.935	1.364	4.299	3.15	92.146	2.832	1.467
21	0.2453	129.629	129.6	4.5	2.950	1.319	4.269	3.24	92.463	2.794	1.475
22	0.2685	130.877	130.9	4.9	2.965	1.291	4.257	3.30	92.651	2.774	1.483

Test Readings for Specimen No. 3

No.	Def. Dial in.	Load Dial	Load lbs.	Strain %	Deviator Stress ksf	Minor Eff. Stress ksf	Major Eff. Stress ksf	1:3 Ratio	Pore Press. psi	P ksf	Q ksf
23	0.2911	132.554	132.6	5.3	2.990	1.273	4.263	3.35	92.781	2.768	1.495
24	0.3251	135.214	135.2	5.9	3.030	1.256	4.286	3.41	92.901	2.771	1.515
25	0.3537	137.329	137.3	6.4	3.061	1.253	4.314	3.44	92.917	2.784	1.530
26	0.3821	139.777	139.8	7.0	3.098	1.275	4.373	3.43	92.769	2.824	1.549
27	0.4108	142.481	142.5	7.5	3.140	1.240	4.381	3.53	93.006	2.811	1.570
28	0.4398	144.971	145.0	8.0	3.177	1.237	4.414	3.57	93.030	2.825	1.588
29	0.4683	147.840	147.8	8.5	3.222	1.243	4.464	3.59	92.988	2.854	1.611
30	0.4971	150.550	150.5	9.0	3.262	1.252	4.514	3.61	92.926	2.883	1.631
31	0.5249	153.258	153.3	9.5	3.302	1.260	4.562	3.62	92.868	2.911	1.651
32	0.5538	155.818	155.8	10.1	3.338	1.281	4.618	3.61	92.727	2.949	1.669
33	0.5820	158.708	158.7	10.6	3.380	1.281	4.662	3.64	92.722	2.971	1.690
34	0.6108	161.945	161.9	11.1	3.429	1.274	4.703	3.69	92.773	2.988	1.714
35	0.6395	164.510	164.5	11.6	3.463	1.288	4.751	3.69	92.676	3.019	1.731
36	0.6685	167.893	167.9	12.2	3.513	1.298	4.811	3.71	92.605	3.055	1.756
37	0.6971	170.629	170.6	12.7	3.549	1.318	4.867	3.69	92.468	3.092	1.774
38	0.7252	173.312	173.3	13.2	3.584	1.338	4.921	3.68	92.330	3.130	1.792
39	0.7537	175.868	175.9	13.7	3.615	1.386	5.001	3.61	91.992	3.194	1.807
40	0.7821	179.561	179.6	14.2	3.669	1.351	5.020	3.72	92.238	3.185	1.834
41	0.8104	182.882	182.9	14.7	3.714	1.358	5.072	3.74	92.191	3.215	1.857
42	0.8394	186.346	186.3	15.3	3.761	1.380	5.141	3.72	92.035	3.261	1.881
43	0.8536	187.966	188.0	15.5	3.782	1.391	5.173	3.72	91.960	3.282	1.891
44	0.8645	187.327	187.3	15.7	3.760	1.405	5.166	3.68	91.860	3.286	1.880



Project Name: I-77 Exit 26 Interchange

Project #: 23610178A

Boring #: W-2

Depth: 5.0' – 7.0' (UD-1)

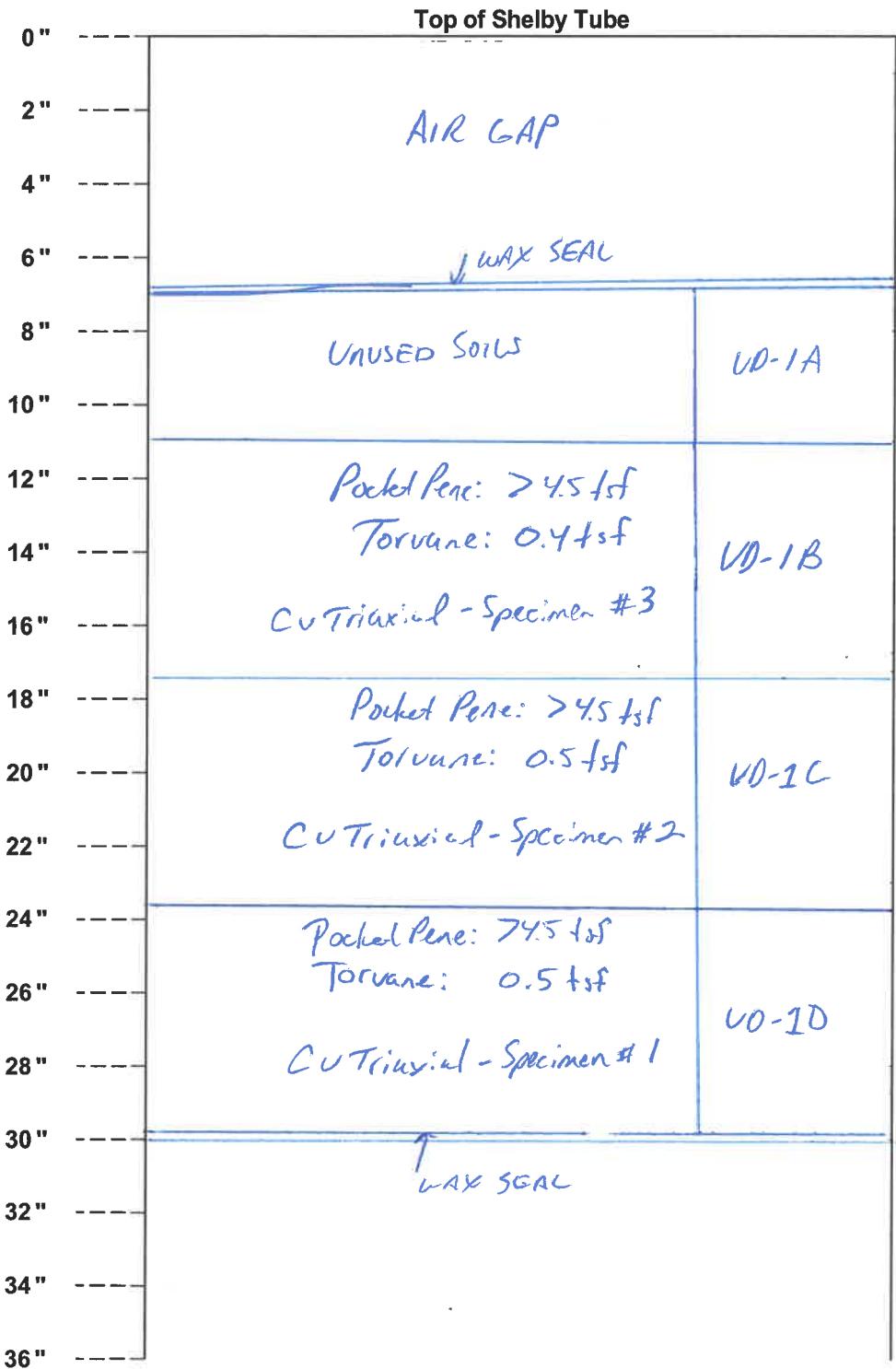
Sample Date: 10/25/23

Test Type: Consolidated Undrained Triaxial Shear (ASTM D4767)



SCDOT Shelby Tube Log

Project ID:	I-77 Ex: f26 Interchange	County:		Boring No.:	w-2
Project Description:	23610178A			Route:	
UD Sample No.:	UD-1	Depth:	5-7'		
Date Sampled:	10/25/23	Date Extracted:	12/13/23		
Extracted By:	B. Kovalevsk	Eng. Firm:	SME, Inc.		



SIEVE ANALYSIS OF SOIL

Revision No. 1

Revision Date: 9/5/17



Single sieve set

ASTM D 6913

S&ME, Inc. - Greenville: 48 Brookfield Oaks Dr., Suite F Greenville, SC 29607

Project #: 23610178A Report Date: 1/11/24
 Project Name: I-77 Exit 26 Interchange Test Date: 1/08 - 1/10/24
 Client Name: RS&H, Inc.
 Client Address: 1520 South Boulevard Suite 200 Charlotte, NC 28203
 Boring #: W-2 Log #: 129g Sample Date: 10/26/23
 Location: UD-2 Type: Undisturbed Depth: 7 - 9'
 Sample Description: SILTY CLAYEY SAND (SC-SM) - gray white, medium to fine



Cobbles	< 300 mm (12") and > 75 mm (3")	Fine Sand	< 0.425 mm and > 0.075 mm
Gravel	< 75 mm and > 4.75 mm (#4)	Silt	< 0.075 and > 0.005 mm
Coarse Sand	< 4.75 mm and > 2.00 mm (#10)	Clay	< 0.005 mm
Medium Sand	< 2.00 mm and > 0.425 mm (#40)	Colloids	< 0.001 mm

Method: B Procedure for obtaining Specimen: Moist Dispersion Process: Dispersant
 Maximum Particle Size 2.00 mm Coarse Sand 0.6% Fine Sand 42.5%
 Gravel 0.0% Medium Sand 14.3% Silt & Clay 42.6%
 Liquid Limit 18 Plastic Limit 14 Plastic Index 4

Natural Moisture 14.0%

Notes / Deviations / References:

Brian Vaughan, P.E.
 Technical Responsibility

Signature

QA Supervisor
 Position

1/11/24
 Date

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**LIQUID LIMIT, PLASTIC LIMIT,
 & PLASTIC INDEX**



ASTM D 4318 AASHTO T 89 AASHTO T 90

S&ME, Inc. - Greenville 48 Brookfield Oaks Dr., Suite F Greenville, SC 29607

Project #: 23610178A Report Date: 1/11/24

Project Name: I-77 Exit 26 Interchange Test Date: 1/10/24

Client Name: RS&H, Inc.

Client Address: 1520 South Boulevard Suite 200 Charlotte, NC 28203

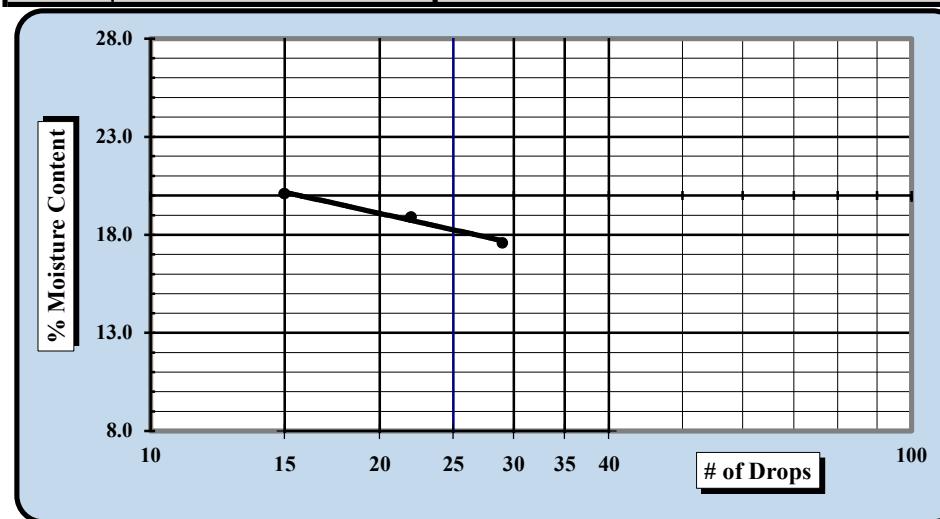
Boring #: W-2 Log #: 129g Sample Date: 10/26/23

Location: UD-2 Type: Undisturbed Depth: 7 - 9'

Sample Description: SILTY CLAYEY SAND (SC-SM) - gray white, medium to white

Type and Specification	S&ME ID #	Cal Date:	Type and Specification	S&ME ID #	Cal Date:
Balance (0.01 g)	13942	10/31/2023	Grooving tool	23119	10/15/2023
LL Apparatus	23158	7/18/2023			
Oven	13978	10/1/2023			

Pan #	Tare #:	Liquid Limit					Plastic Limit	
		6	7	8			9	10
A	Tare Weight	27.77	26.32	27.32			26.83	26.75
B	Wet Soil Weight + A	47.79	43.31	45.78			33.94	34.59
C	Dry Soil Weight + A	44.79	40.61	42.69			33.08	33.65
D	Water Weight (B-C)	3.00	2.70	3.09			0.86	0.94
E	Dry Soil Weight (C-A)	17.02	14.29	15.37			6.25	6.90
F	% Moisture (D/E)*100	17.6%	18.9%	20.1%			13.8%	13.6%
N	# OF DROPS	29	22	15			Moisture Contents determined by ASTM D 2216	
LL	LL = F * FACTOR							
Ave.	Average						13.7%	



One Point Liquid Limit			
N	Factor	N	Factor
20	0.974	26	1.005
21	0.979	27	1.009
22	0.985	28	1.014
23	0.99	29	1.018
24	0.995	30	1.022
25	1.000		

NP, Non-Plastic
 Liquid Limit **18**
 Plastic Limit **14**
 Plastic Index **4**
 Group Symbol **CL-ML**

Multipoint Method
 One-point Method

Wet Preparation Dry Preparation Air Dried % Passing the #200 Sieve: 42.6%

Notes / Deviations / References: Group symbol for minus #40 sieve portion only (see Sample Description for classification of entire sample).

ASTM D 4318: Liquid Limit, Plastic Limit, & Plastic Index of Soils

Benjamin J. Kovaleski
 Technician Name

1/11/24
 Date

Brian Vaughan, P.E.
 Technical Responsibility

1/11/24
 Date

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DENSITY (UNIT WEIGHT) OF SOIL SPECIMENS

ASTM D 7263 - Method B



Project #: 23610178A
Project Name: I-77 Exit 26
Interchange
Sample Description: SILTY CLAYEY SAND (SC-SM) -
gray white, medium to fine
Liquid Limit: 18
Plastic Limit: 14
Plastic Index: 4

Report Date: 1/11/24
Test Date(s): 1/08 - 1/10/24
Sample Date: 10/26/23
Boring #: W-2
Depth: 7 - 9'
Sample Type: UD
% Passing #200: 42.6

TUBE DATA

Weight of Tube and Soil 1814.3 g.
Weight of Tube 435.3 g.
Weight of Soil 1379.0 g.
Length of Tube 6.060 in. 0.5050 ft.
Diameter of Sample 2.898 in. 0.2415 ft.
Volume of Soil 0.0231 ft³

MOISTURE CONTENT DATA

Wet Weight 345.65 g.
Dry Weight 303.13 g.
Weight of Water 42.52 g.
Moisture Content 14.0 %
Pan # D-8

Wet Unit Weight 131.4 pcf

Dry Unit Weight 115.3 pcf

Type and Specification	S&ME ID #	Cal Date:	Type and Specification	S&ME ID #	Cal Date:
Balance (0.01 g)	13945	10/31/2023	Calipers (0.0005")	23286	10/31/2023
Balance (0.002 lb)	13946	10/31/2023	Straightedge	23330	12/9/2023
Oven	22915	10/1/2023			

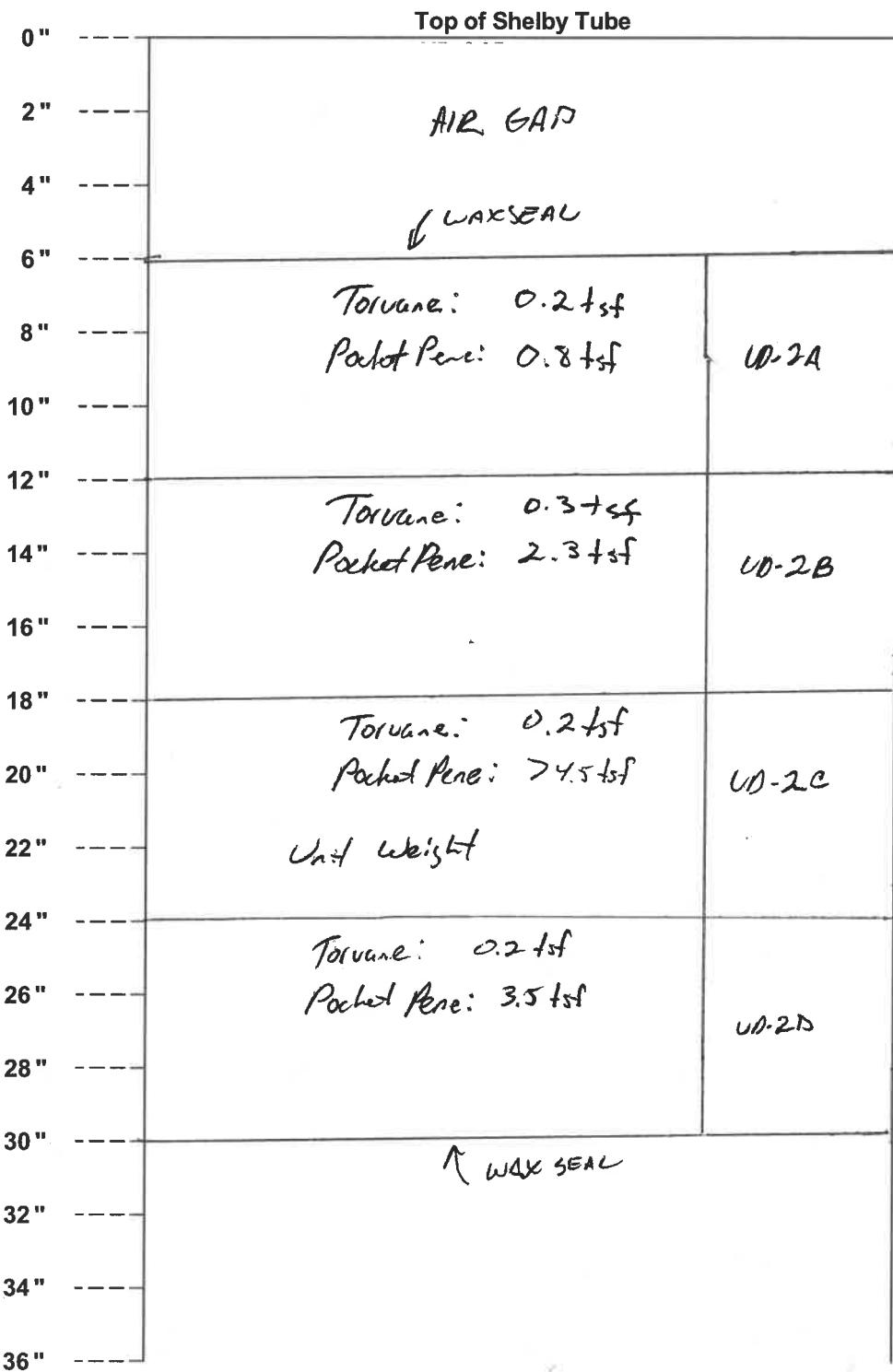
Technician Name: Benjamin Kovaleski NICET Lab Level III 117226 1/11/24
Certification# *Date*

Technical Responsibility: Brian Vaughan, P.E. QA Supervisor
Signature *Position*



Shelby Tube Log

Project ID:	23610178A	County:		Boring No.:	W-2
Project Description:	I-77 Exit 26 Interchange			Route:	
UD Sample No.:	UD-2	Depth:	7-9'		
Date Sampled:	10/26/23	Date Extracted:	1/08/24		
Extracted By:	B. Kovalski	Eng. Firm:	SURE, Inc.		



Appendix IX– 3-Point ADRS Curve

3-Point Acceleration Design Response Spectrum

SCDOT v3.2 - 12/12/2023

Project ID:	P042443	Latitude:	34.1939
Route:	I-77	County:	40 - Richland
Project:	New Exit 26 Interchange	Longitude:	80.9843

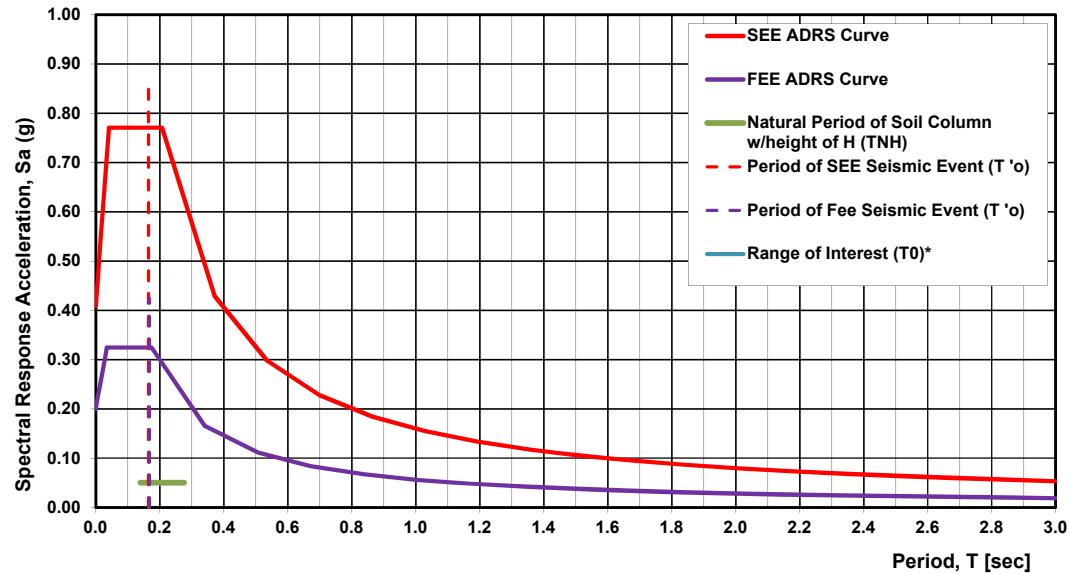
Designer:	N. Harman - Support
Date:	12/12/2023

Design EQ	PGA	S _{DS}	S _{D1}	M _W	R	PGV	D _{a5-95}	T'₀
	g	g	g	-	km	inches/sec	sec	sec
FEE	0.20	0.32	0.06	7.30	126.93	2.14	37.10	0.17
SEE	0.41	0.77	0.16	7.28	125.90	6.06	36.64	0.16

Fundamental Period of Structure, T _₀ *	Range of Interest		V* _{s,H}	H	T _{NH}	
	sec				sec	
	sec	0.5*T _₀	2.0*T _₀	(4*H)/V* _{s,H}	(6*H)/V* _{s,H}	
0.00	0.00	0.00	2101.56	96.70	0.14	0.28
0.00	0.00	0.00				

H = B-C Boundary

SC Seismic ADRS Curve



Damping:	5%
Geologic Condition:	Geologically Realistic (Q = 100)*
ADRS Location within Soil Column:	SCP

South Carolina Piedmont

*Same Geologic Condition as used in SCENARIO_PC (2006)

FEE Data

T	S _a
0.00	0.200
0.01	0.221
0.01	0.241
0.02	0.262
0.02	0.283
0.03	0.304
0.03	0.324
0.05	0.324
0.06	0.324
0.07	0.324
0.08	0.324
0.09	0.324
0.10	0.324
0.12	0.324
0.14	0.324
0.15	0.324
0.17	0.324
0.18	0.324
0.19	0.324
0.21	0.324
0.34	0.166
0.51	0.111
0.67	0.084
0.84	0.067
1.01	0.056
1.17	0.048
1.34	0.042
1.50	0.038
1.67	0.034
1.84	0.031
2.00	0.028
2.17	0.026
2.34	0.024
2.50	0.023
2.67	0.021
2.83	0.020
3.00	0.019

SEE Data

T	S _a
0.00	0.409
0.01	0.469
0.01	0.530
0.02	0.590
0.03	0.650
0.03	0.710
0.04	0.771
0.05	0.771
0.06	0.771
0.07	0.771
0.08	0.771
0.10	0.771
0.11	0.771
0.12	0.771
0.14	0.771
0.15	0.771
0.17	0.771
0.18	0.771
0.19	0.771
0.21	0.771
0.37	0.430
0.54	0.298
0.70	0.228
0.86	0.185
1.03	0.155
1.19	0.134
1.36	0.118
1.52	0.105
1.69	0.095
1.85	0.086
2.01	0.079
2.18	0.073
2.34	0.068
2.51	0.064
2.67	0.060
2.84	0.056
3.00	0.053

Appendix X – Electronic Data Files

gINT® Project Files

Excel® Downhole Seismic Velocity File